

Towards a Methodology to Test UAVs in Hazardous Environments

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ABSTRACT - This paper reports on the early stages of the development of a methodology to analyse and test autonomous systems in hazardous environments, with the aim of verifying both the safe decision-making and resulting actions of the system. The ultimate goal is to generate safety case evidence that a designer can provide to a regulator to show that the system to be used will likely operate safely.

Keywords – UAV; Hazardous Environments; Verification; Simulation.

I. INTRODUCTION

There is currently a drive in the UK toward using autonomous systems, and robotic systems in particular, in extreme or hazardous environments [1]. This paper is concerned with the Verification and Validation (V&V) of autonomous systems operating in hazardous (specifically offshore) environments.

Autonomous systems are systems which decide for themselves what to do [2]. Typically, these decisions are made using computer systems, which control the system in question and perform operations that might otherwise be performed by a person. For example, an autonomous Unmanned Aerial Vehicle (UAV) will need to contain a number of computer systems that can replace a human pilot operating the UAV using remote control [3].

In this paper, an autonomous system means the following:

A system that is given a goal and restrictions and fulfils this goal by planning, making decisions and carrying out actions without direct human interaction

Robotic systems are good for tasks in hazardous environments. Typically, robotic systems are used for Dull, Dirty and/or Dangerous missions, commonly known as the “three D’s”. Recently however, the need to use robots within Demanding, Distant and Distributed missions has also been established. Offshore environments, such as oil platforms and wind farms, are prime examples of these latter “three D’s”.

In all environments, but in particular for hazardous environments, autonomous systems must operate safely and be safe to operate. What is more, this must be demonstrable. Part of the process to demonstrate this safety case means that the decisions being made, by the system, the reasons why

they have been made and the actions that result from these decisions need to be verified for all possible operating conditions. Furthermore, if a system fails, knowledge regarding why it fails is required. Thus, the question asked in this paper is as follows:

How can an autonomous UAV be analysed to determine the conditions under which it fails and to indicate why it failed?

This paper uses an example scenario of an UAV inspecting an offshore asset to demonstrate the development of tools and techniques that will be used to verify its safe operation.

The paper is organised as follows. Section II establishes the challenges of offshore environments for autonomous systems; how V&V can be used to ensure safety; how a system needs to be constructed to be verified; how the V&V outputs can be used to build certification evidence; and how the methodology presented contributes to this. Section III presents the methodology to analyse the UAV and provide explainable failures and Section IV shows the results of its application and interpretation. Finally, conclusions are drawn and future work is detailed in Section V.

II. BACKGROUND

A. Offshore Operations

For the purposes of this paper, ‘the offshore environment’ means the environment around energy generation assets, such as oil rigs and wind turbines.

UAV operations, e.g., remote inspections around oil rigs and wind turbines, pose many engineering challenges. A potentially significant source of operational difficulty for such tasks will be when flying in the disturbed/turbulent air flow near such structures, as shown in Figure 1. Such turbulent flow structures make flying in and around the offshore assets dangerous if the vehicle does not possess sufficient control authority to maintain its desired position, leading to a potential collision with the asset or its associated personnel.

A similar situation exists for ship-borne naval aviation operations. Helicopters are often operated from landing decks located at the ship’s stern. The ship’s motion and wind

conditions create an area of disturbed air flow in the landing area. To determine whether a particular ship and helicopter combination is capable of landing/taking off from the ship under a given wind condition, flight trials are conducted to form a Ship Helicopter Operating Limit (SHOL) [4]. Previous work has investigated the replacement of part of the physical testing required to generate a SHOL with piloted simulations [4]. The method presented in this paper takes a similar simulation-based approach for autonomous UAV system missions.

The scenario considered in this paper is an inspection task for a UAV on an oil rig leg. This is a sufficiently complex task to allow the methodology to be rigorously tested. It will be applied to other, more diverse scenarios at a later date.

B. V&V of Autonomous Systems

Autonomous systems present a significant challenge for V&V. Many non-autonomous systems are designed to use a human operator who has overall responsibility for the safe and reliable operation of the system. Autonomous systems, on the other hand, cannot assume the presence of the responsible human, and therefore must manage safe and reliable operations themselves [5].

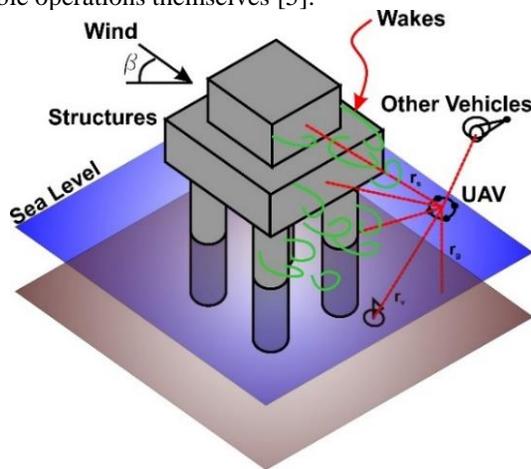


Figure 1. A typical offshore UAV operating environment.

V&V for autonomous systems uses many well-established techniques, as well as some that have been developed with autonomous systems in mind [5]. At the same time, experimentation within controlled environments is a mainstay of engineering best-practice, and is also used for autonomous systems. However, due to the significant challenges and added complexity of autonomous systems, experimentation can be expensive and dangerous. Therefore, high-fidelity simulation is often used as a separate V&V technique [6]. High-fidelity simulation involves incorporating accurate physical models of a system within a realistic synthetic environment. Trials within high-fidelity simulation provide a safer and potentially cheaper means to test than physical experiments. Of course, this comes at the cost of needing to understand the limitations of the models being used. The models of the system and the environment

used within simulation must themselves be verified and validated [7].

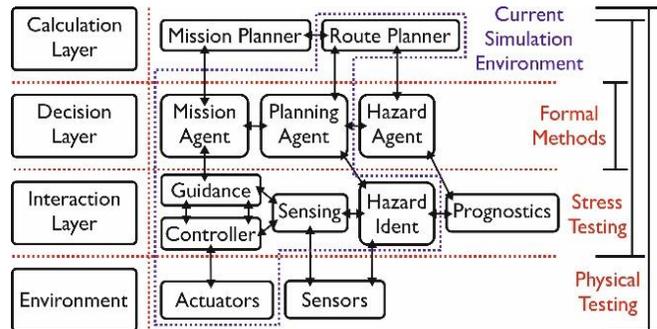


Figure 2. System Architecture of an Autonomous UAV with the separation of the component using layers which then indicates the verification method to be applied to each

A V&V technique commonly used for autonomous systems is formal verification, an application of Formal Methods [8]. Formal verification works by building abstract mathematical models of the system in question, and then exhaustively analysing the models using software to determine whether or not particular requirements hold. Formal verification is particularly useful for finite state systems, and has therefore found a natural application in the verification and validation of autonomous software.

There are, of course, many other V&V techniques not listed above, including hardware-in-loop testing [9], real-world operations and end-user validation [10], that are also used for V&V of autonomous systems.

C. Systems Architecture for V&V

To be able to apply V&V to a whole system, it needs to be constructed in a certain way. This is mostly due to the models used to describe a sub-system. In Figure 2, the systems architecture of an autonomous system that is to fly UAVs around oil rigs is shown. There are two important features in this architecture: the layers and the intra-layer separation of subsystems.

The layering is to group sub-systems, similar in construction rather than role or output. The calculation layer can be thought of as any task that reasons about the world in a non-abstract way, such as a route or mission planner. The decision layer is for those systems that make decisions based on information provided by the interaction and calculation layers. The interaction layer is the low level autonomous tasks that translates plans and decisions into actions. The environment layer is the actual hardware that physically carries out the desired actions.

On the right of Figure 2, the verification methods are aligned with the components that they are best suited to testing. Formal methods are well suited to analysing and verifying decision making, but the abstraction required to apply them to planners or continuous controllers makes them less so for these elements. Simulation-based testing allows

many permutations of the systems goals, initial conditions and even internal parameters, to be tested; thus allowing the actions of the systems to be rigorously tested. The physical testing of the system then checks the results of the formal methods and simulations against reality and will determine the validity of the abstractions and assumptions required to build them.

In short, with the system constructed in such a way, the following questions can be answered:

- Formal Methods* - Has the safe decision been made?
- Simulation Based Testing* - Did it result in safe actions?
- Physical Testing* - How well do these answers match reality?

D. Evidence for Safe Operations

For an autonomous system to be used in a real-world environment, its safe operation needs to be agreed with the regulator. In the UK, there is no standard method for assessing whether or not autonomous UAV operations are safe. Each request for operation is reviewed on a case-by-case basis using a submitted safety case/risk assessment for the planned operation.

V&V techniques can be used to generate evidence to prove that a system will operate safely and reliably. This paper proposes that formal methods and simulation based stress testing can be included to add strength to the safety case.

For the scenario considered in this paper, the operating envelope of the system, when being used in certain conditions is the addition to the safety case. An example of this is shown in Figure 3. This example is intentionally similar to that of a SHOL. The aim of simulation-based verification is to generate this operating envelope. The dotted lines represent the boundary between safe and unsafe operations.

As an example, for a UAV doing inspections of the legs of an oil rig, there will exist a set of wind speeds and directions under which the UAV is no longer able to operate. The operator of the UAV, oil rig and regulators will need to know the safe wind speed and direction operating envelope before any task can proceed.

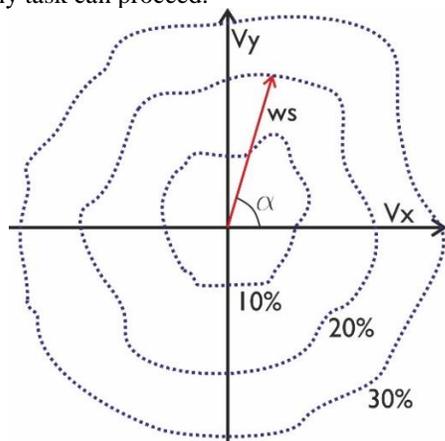


Figure 3. Illustration of the safety case evidence aimed for when using the methodology.

In addition, for this situation the variables that affect the safe operation of the UAV are not restricted to just the wind speed and direction. They could include, but are not limited to, the following:

- Initial position and goal
- Geometry of environment
- UAV performance capability
- Actuator/sensor performance/degradation
- Other environmental conditions e.g. ambient light, sea state etc.

This means that the real operating envelope will be a multi-dimensional surface.

It is important to note here that such a surface can not only be used as safety-case evidence, but also as a run-time safety monitor. The analogy is that the boundary is the equivalent of the prior experience of the human pilot, where they intuitively know what actions and decisions are a good idea or not. This can then be used, while the system is in operation, to inform the autonomous system of when it is feasible to carry out a plan or not; or as a monitor to tell the system that, as the environment changes, planned actions or current states (such as where it is) are no longer safe.

E. Understanding the System's Failure

If a system is tested under one set of conditions and is found to successfully complete the task assigned to it safely, this is good. If under slightly different conditions, the system fails to complete it safely, this is also good. This now informs both the user and the system itself, when it should and should not carry out particular actions. This is the essence of the operating envelope shown in Figure 3. However, this does not inform the user, or regulator, why the system failed.

It is far more useful to be able to say under what conditions a system can or cannot work and to also to be able to say why. This both directs any effort to redesign or improve the system, as the designer now knows which system to focus on; and it provides the regulator with a more concrete answer as to why it behaves in the way it does.

As an example, suppose there are measures of failure for an actuator, controller, guidance, and navigation of a UAV (more on this in Section III). After a simulation of a task, at a number of wind speeds and directions, these failure measures are then applied to the response, a possible result could be as shown in Figure 4 (a). Outside of this boundary, the system failed its task, while inside it succeeded. The aggregate of these failure results in Figure 4 (b).

This boundary is now the operating envelope of the system. However, by splitting the failure of the system into separate components, the colours shown can be added. This then indicates that the actuator, at least in this example, was the most likely cause of the system to fail its task.

III. METHODS

This section describes the cost functions and methodology used to apply V&V ideas to an autonomous systems.

A. Cost functions for each component

Four continuous autonomy components are considered. The responsibility of each component, what its job is, determines the definition of the cost function. The responsibilities of each component are as follows:

Actuator: To create the required output while leaving a margin of error as a contingency.

Controller: To force the current states to follow the commanded states as closely as possible, while maintaining system stability.

Guidance: To cause the system to follow the desired path to within a desired separation distance.

Navigation: To generate a path between the start and goal, while avoiding collisions with objects.

The cost function defining the actuator's performance is shown in (1) and illustrated in Figure 5.

$$A_f = \frac{1}{n_a} \sum_{i=1}^{i=n_a} \frac{1}{t_m} \int_0^{t_m} \frac{\sqrt{(A_i - .5)^2}}{.5 - Mar} dt \quad (1)$$

Where n_a is the number of actuators, t_m is the maximum simulation time, A_i the actuator output at time t , Mar the specified margin of error, and dt the time step of the simulation.

Here, the zero point for the actuator is 50%. The function is, in essence, a time average of the deviation from the neutral point normalised by the margin of error. The performance of all the actuators is averaged over time and over the number of actuators.

This function aims to create a single measure for all the actuators over the time period of operation between 0 and 1. The cost function gives a gradual increase in the failure. If an actuator reaches either 100% or 0%, this results in the failure of the system being set to 1. This can be considered a critical failure, as would a collision, since the system would very likely become unsafe.

The controller's performance is defined in (2) and shown in Figure 6.

$$C_f = \frac{1}{n_s} \sum_{i=0}^{i=n_s} \frac{1}{t_m} \int_0^{t_m} \frac{\sqrt{(R_i - u_i)^2}}{Dif_i} dt \quad (2)$$

Where n_s is the number of controlled states, R_i is the command reference, u_i the measured state of the system, and Dif_i the specified max difference between the actual and reference values.

It is essentially the same as the cost function used in Linear Quadratic Regulator controllers. The difference between the reference and controlled state is normalised by a desired maximum distance. It is then averaged over both time and the number of controlled states. A discontinuity exists when the system becomes unstable.

The guidance performance is defined by both in (3) and Figure 7.

$$G_f = \frac{1}{t_m} \int_0^{t_m} \frac{\sqrt{(\delta_x + \delta_y + \delta_z)^2}}{Div} dt \quad (3)$$

Where δ_x , δ_y , and δ_z are the orthogonal difference between the actual position and the desired path and Div is the specified maximum deviation from the path.

It is the length of the vector perpendicular to the nearest point on the desired path from the system's current location. It is then normalised by the desired maximum deviation from the path. A discontinuity does not explicitly exist with this function, however the discontinuities are handled by the mission manager's performance, see Criteria Analysis section later.

The navigation's performance is defined by (4) and by Figure 8.

$$N_f = \frac{1}{t_m} \int_0^{t_m} \frac{Prox}{P} dt \quad (4)$$

Where P_n is the planned proximity at the point on the path perpendicular to the current position, P the proximity to the nearest object, and $Prox$ is the specified maximum proximity to an object.

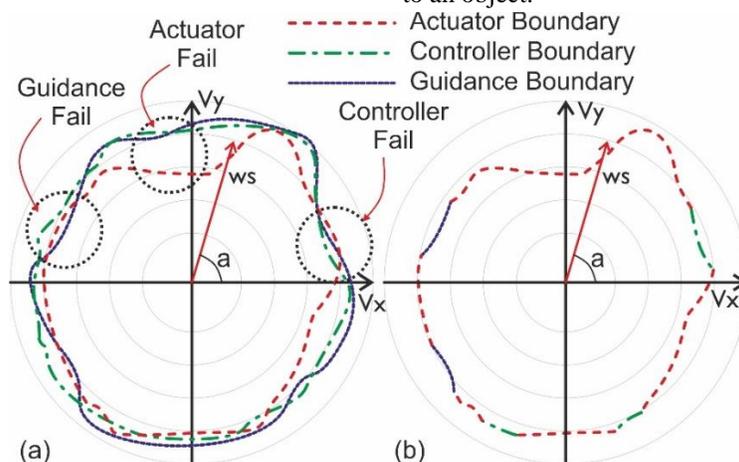


Figure 4. Illustration of how the subsystems can be combined and therefore allow the explanation of why a system failed to operate safely

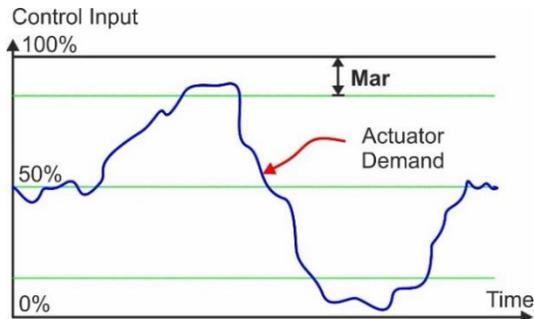


Figure 5. Definition of cost function for the analysis of the actuator's performance

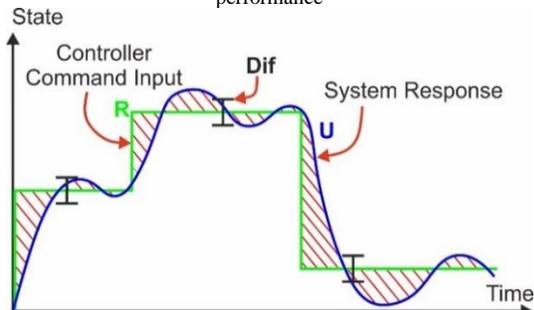


Figure 6. Definition of cost function for the analysis of the controller's performance

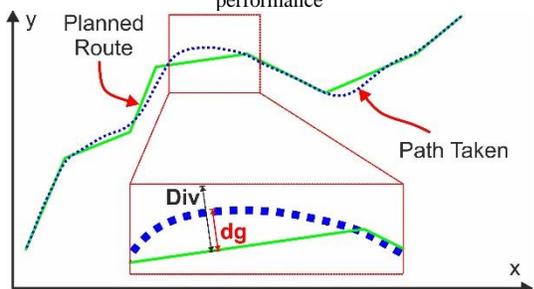


Figure 7. Definition of the cost function for the analysis of the guidance performance

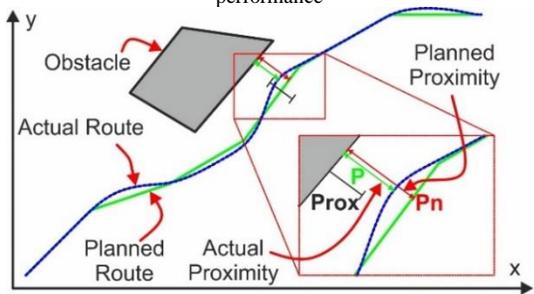


Figure 8. Definition of the cost function for the analysis of the navigation performance

B. Simulation Environment

A simple simulation environment of a helicopter moving around the legs of an oil rig is used to generate the data required to test the above cost functions, see Figure 9.

It consists of a series of linearized state space flight dynamics models identified from a non-linear simulation model. The models are then scheduled based on the forward

flight speed of the UAV, to account for the changing dynamics.

To control the helicopter a PI controller [11] is gain scheduled and a waypoint following with cross tracking error is used as the guidance method [12]. A simple A* route finding algorithms is used for the navigation [13], where a simple hazard model is used to allow the planner to plan a route around the wakes of the oil rig legs.

A sample data set is taken from the simulation environment and presented in the next section. The cost functions are then applied to the output of the simulator.

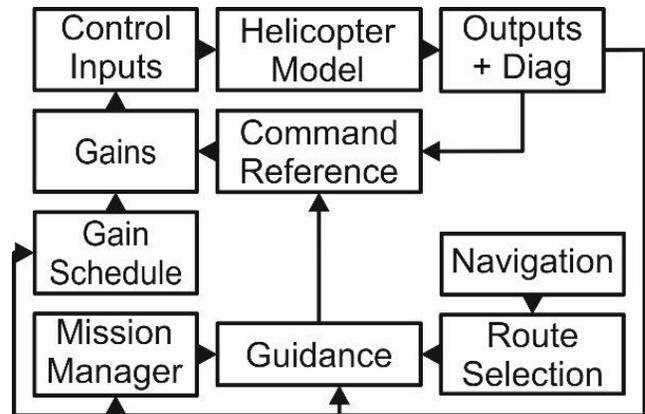


Figure 9. Systems diagram for the simulator

IV. RESULTS

When testing and analysing an autonomous system's performance, a designer may be presented with the output shown in Figure 10 to Figure 12. From this the designer would be able to determine whether the UAV was able to carry out the task assigned to it. In this case, simply move from bottom left to the right of the top right leg.

However, some of the routes come very close to the legs, to the point where a collision is very likely. This is also for only a single set of conditions, but can only be interpreted visually. If the conditions change, will the UAV be able to still carry out the task? How does this compare to other UAVs or settings/weightings within the autonomous components of the UAV?

A closer inspection of the least risky plan's response of the UAV can be seen in Figure 13, Figure 14, and Figure 15. From this, it can be determined that the control input is not exceeded, the body velocities follow the reference values and the UAV follows the desired path reasonably well. However, again this does not allow an easy comparison to other UAVs or settings. The interpretation is also abstract and not quantified.

Further detail can be determined from Figure 16 and Figure 17, where how well the UAV followed the planned path and how well the plan enabled the UAV to avoid collisions with its surroundings is shown. The actuator cost function can be applied to the results in Figure 13, the controller function to Figure 14, the guidance function to Figure 16 and the navigation function to Figure 17.

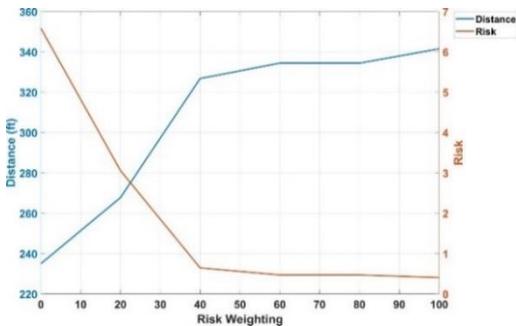


Figure 10. Balance between a route's total distance and the risk associated with it

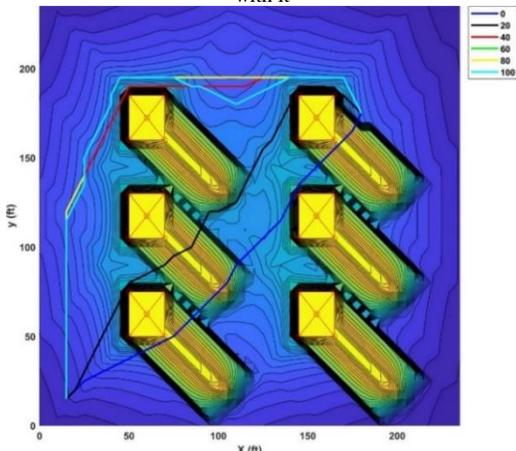


Figure 11. Planned routes for a range of risk weightings

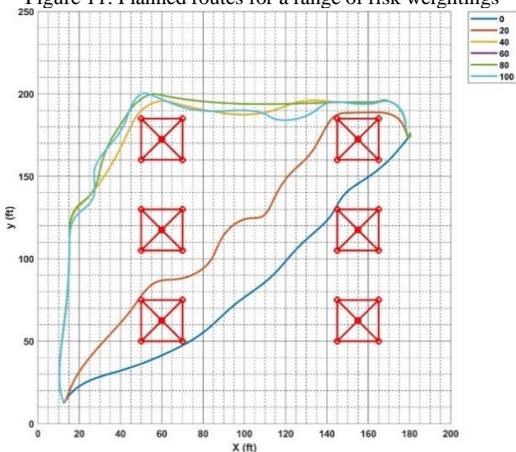


Figure 12. Plan view of the response of the UAV as the guidance, controller and model tries to follow the planned route

This allows a simple metric to be applied to the UAV's response, reducing the interpretation of the performance down to a single number, thus allowing easier comparisons and optimisations of the UAV's settings to be made.

Figure 18 to Figure 21 show the cost functions of the UAV response for a range of different performance specifications.

Figure 18 shows that, as the specification is made more demanding, the cost increases, as would be expected. It also illustrates the control that is closest to failure, in this case the collective.

Figure 19 shows the performance of the flight controller. It can be seen that the u and v velocities are by far the most difficult for the controller to follow; also that unless very strict limits on the deviation of the actual from the command reference values are imposed, the performance is good. A similar story can be seen in Figure 20, where only very small allowed deviations from the desired direction will result in the system's failure.

Figure 20 shows that, on average, the guidance system allows the UAV to follow the desired path well. Only when the allowable deviation from the desired path is below 4 ft will the system fail. Therefore, showing that the guidance is able to perform correctly, unless under tight restrictions.

The navigation performance is shown in Figure 21, where the performance decreases as the closest allowable proximity of the UAV to an object is increased. It can be seen that only small allowable proximities result in the system being safe.

Taking Figure 18 to Figure 21 together, it can be seen that the actuators and controller are performing well, even under tight requirements. Guidance performs well, but the navigation component is the likely cause of the systems to be unable to carry out its assigned task. This is in contrast to the interpretation of Figure 10 to Figure 12, where such conclusions are harder to draw, as the performance of the system is not quantified.

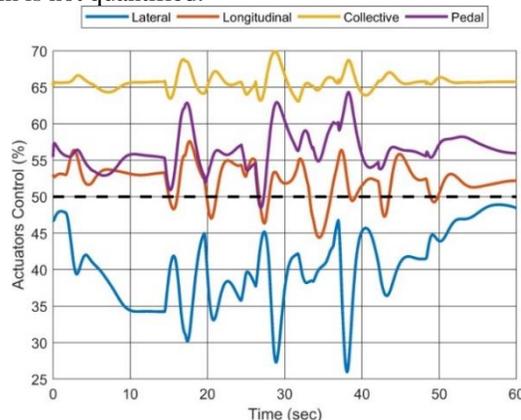


Figure 13. Control inputs for the UAV

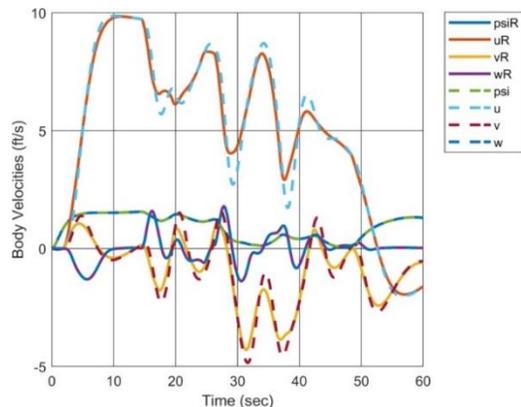


Figure 14. Body velocities (u,v,w)/heading (psi) and controller reference velocities (uR, vR, wR, psiR)

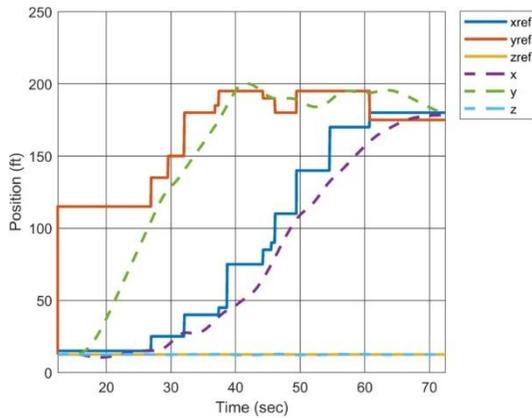


Figure 15. UAV (x, y, z) and reference (xref, yref, zref) positions

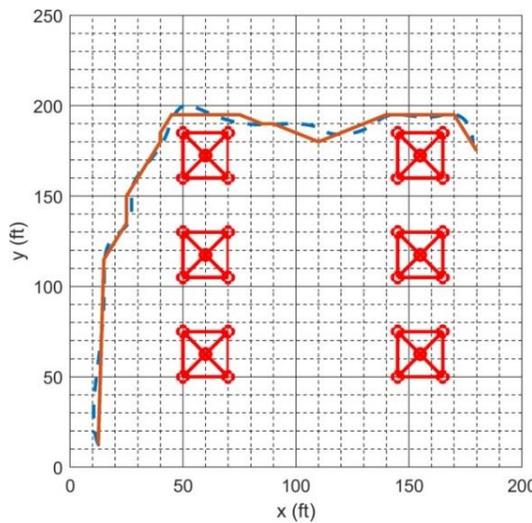


Figure 16. Plan view of the UAV's response when following the least risky planned route. Solid line = planned route. Dashed line = path taken

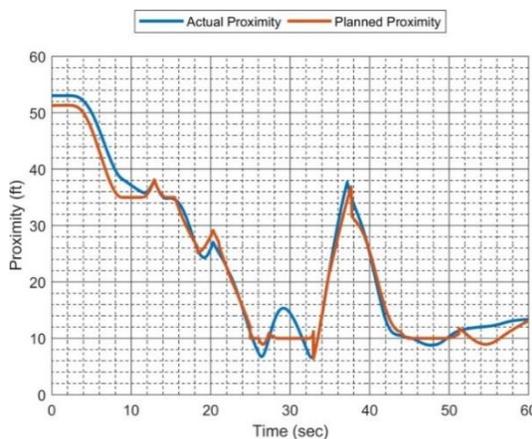


Figure 17. Actual and planned proximity to the nearest object at a point in time in the UAV's response

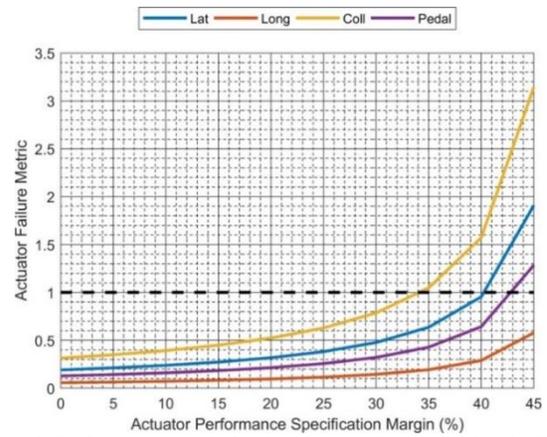


Figure 18. Performance metric for the actuator when applied to the UAV's response for a range of specifications

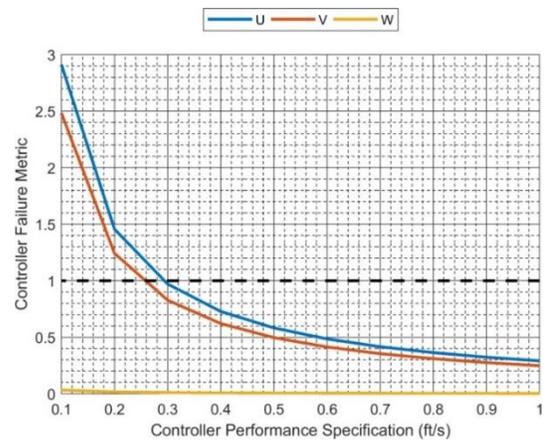


Figure 19. Controller performance for the body velocities for a range of specifications

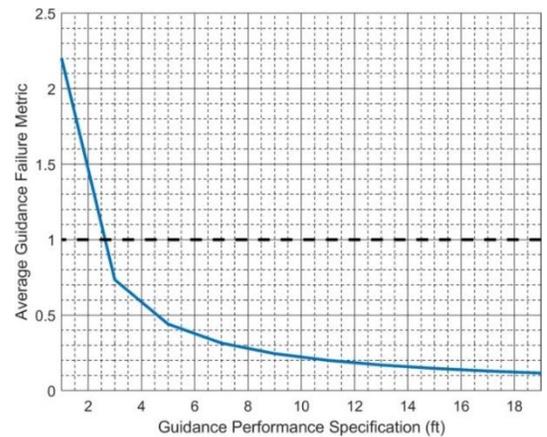


Figure 20. Controller performance for the direction command reference

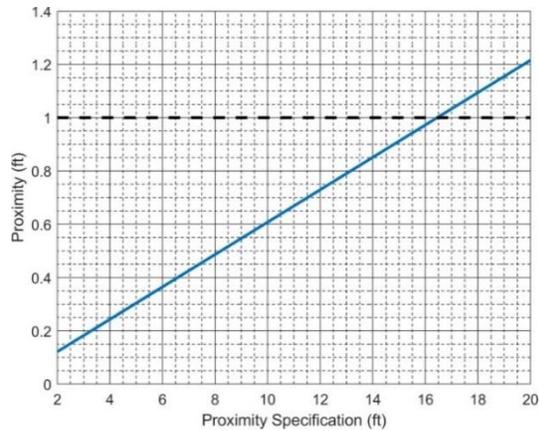


Figure 21. Navigation performance for a range of specified proximity specifications

V. CONCLUSION AND FUTURE WORK

A. Conclusion

A method for the analysis of the continuous autonomous components of a system has been reported. Results from a scenario where a UAV moves around an oil rig’s legs have been presented.

The need to certify an autonomous systems operating in hazardous environments by V&V methods was discussed and the need to separate the failure of subsystems outlined.

It was found that by applying the presented methodology, the performance of the system can be quantified; also, that the component that is likely to cause the system to fail can be found, and therefore focused on by the system’s designer. Thus, the first stages of a method to analyse a system to determine when a system fails and why was successfully demonstrated.

B. Future Work

Having a quantifiable metric of a systems performance allows two follow up pieces of work. First, it allows the generation of operating envelopes, which can then be used by a systems user or by the system itself as safety run time errors. Second, it allows the performance of the system to be optimised by wrapping the simulation and analyse method in an optimiser, where the bias, weightings and settings of the system are the independent variables and the outputs of the presented cost functions can be used to form a cost function of an optimiser.

To achieve both of these, a third and final follow up task is required, where an algorithm to search all the variables that can influence the system’s performance is needed. The algorithm will be required to move through both continuous and discrete parameter space. A hybrid evolutionary/genetic algorithm or a modified Particle Swarm Optimisation method is a likely solution to meet this requirement.

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