Quantification of the uncertainty in coastal storm hazard predictions due to wave-current interaction and wind forcing

Charlotte E. Lyddon1,2, Jennifer M. Brown2, Nicoletta Leonardi1, Andrew Saulter3, Andrew J. Plater1

1University of Liverpool, School of Environmental Sciences, Liverpool, L69 7ZT, United Kingdom.

2National Oceanography Centre Liverpool, Joseph Proudman Building, 6 Brownlow Street, Liverpool, Merseyside L3 5DA, United Kingdom.

3Met Office, Exeter, EX1 3PB, United Kingdom.

Corresponding author: Charlotte Lyddon ([c.e.lyddon@liverpool.ac.uk)](mailto:c.e.lyddon@liverpool.ac.uk))

Key Points:

* Delft3D-FLOW-WAVE is used to quantify uncertainty in water level and waves in a hyper-tidal estuary due to coupling and forcing processes.
* Exclusion of locally generated winds underestimates significant wave height at high water by up to 90.1% in the outer estuary.
* Local atmospheric forcing is vital in coastal hazard predictions for timely flood warnings and to avoid under-designing protection schemes.

Abstract

Coastal flood warning and design of coastal protection schemes rely on accurate estimations of water level and waves during hurricanes and violent storms. These estimations frequently use numerical models which, for computational reasons, neglect the interaction between the hydrodynamic and wave fields. Here, we show that neglecting such interactions, or local effects of atmospheric forcing, causes large uncertainties, which could have financial and operational consequences because flood warnings are potentially missed or protection schemes under-designed. Using the Severn Estuary, SW England we show that exclusion of locally generated winds underestimates high water significant wave height by up to 90.1%, high water level by 1.5% and hazard proxy (water level + ½ significant wave height) by 9.1%. The uncertainty in water level and waves is quantified using a system to model tide-surge-wave conditions, Delft3D-FLOW-WAVE in a series of eight model simulations for four historic storm events.

**Plain Language Summary**

Coastal zones worldwide are subject to combined effects of astronomical tides, meteorological storms surges, waves and wind during storms and hurricanes, which can lead to flooding, property damage, and casualties. Coastal communities and critical infrastructure rely on accurate water level and wave forecasts to mitigate these combined hazards. Forecasts utilize hydrodynamic numerical models which need to accurately represent these hazards and how they interact with, and feedback to, each other. This study uses a model, Delft3D-FLOW-WAVE, to calculate how tides and waves from four historic storm events combine to contribute to water level, wave height and hazard proxy (water level + ½ wave height) in the Severn Estuary, southwest England. Additional simulations are run to show how local winds can further contribute to the hazard. Results show that including locally generating winds in simulations of water level, wave height and hazard proxy is most important for accurate representation of physical processes that contribute to coastal hazards. Excluding locally generated winds from numerical model predictions could mean that flood alerts, warnings and evacuation orders are missed, or coastal protection schemes are under-designed, potentially leading to more flooding.

1 Introduction

Concurrence of astronomical high tides, meteorological storm surge due to hurricanes, cyclones or mid-latitude storms, energetic waves, and strong winds can cause coastal flooding, and subsequent damage to property and loss of life to some of the 600 million people estimated to live in low-lying coastal (<10 m) regions worldwide (Barnard et al., 2019; Wolf, 2009). The devastating effects of concurrent coastal hazards are well documented in hyper-tidal regions, where tidal range exceeds 6 m, in the Severn Estuary, UK (Sibley et al., 2015), Bay of Fundy (Greenberg et al., 2012) and Yangtze Estuary (Yin et al., 2017), as combined storm parameters can enhance high water level (HWL) and high water significant wave height (HWHs), defined as significant wave height at the time of high water, to increase the likelihood of overtopping and subsequent inundation. Increasing coastal population and urbanization, potential future changes in storm tracks and sea-level rise means there is a need to plan for the negative consequences of coastal hazards.

Operational storm surge and wave forecasts are important components of coastal storm hazard mitigation strategies (Tunstall et al., 2004). If operational forecasts exceed pre-defined threshold levels, corresponding to the minimum wave and total water level that represent a potential flood hazard (Del Río et al., 2012), alerts and flood warnings will be issued to detail scale, timing and location of a hazard (Lawless et al., 2016). To prevent negative consequences of forecast extreme storm events, flood warnings issued by local agencies must be accurate and timely. Operational forecasts can make use of measured and modeled meteorological and oceanic data (e.g. O’Neill et al., 2016) and outputs can be used to estimate likelihood of coastal flooding, and the effect of wind, waves and total water level on overtopping and breaching for specific flood events (Quinn et al., 2014). However error can be introduced into operational forecasts due to model, knowledge and data uncertainty (Stephens et al., 2017). Uncertainty due to a model’s ability to accurately represent physical processes or replicate interactions (e.g. Bolaños et al., 2014), lack of knowledge of interactions in a physical system and inaccurate input parameters (e.g. temporally or spatially limited) can be introduced, and propagated through the modelling chain to inundation assessments and flood warnings (Sayers et al., 2003). There is a need to understand and reduce uncertainty in operational forecasts of HWL and HWHs that contribute to hazard assessments. Uncertainty in operational forecasts could mean flood events are underestimated or missed, which may increase the risk to coastal communities and critical infrastructure.

The accurate definition of HWL and HWHs is also important for critical storm threshold identification for the design of cost-effective coastal protection strategies. Implementation of hard structures or nature-based solutions, which aim to mitigate the effects of HWL and HWHs, rely on a thorough understanding of the physical processes and interactions in a region (Conger & Chang, 2019). The type and costs of new schemes largely depend on the physical conditions at the site, and sensitivity of the scheme to natural processes and their interaction (Temmerman et al., 2013). Uncertainty in HWL and HWHs may lead to incorrect hazard thresholds, as defense exceedance is most likely to occur close to the time of high water, or implementation of strategies which are not able to protect hinterlands against normal winter conditions as well as extreme storm tide conditions. Commitment to upgrading engineered structures, such as Canada’s recent US$114 million pledge to upgrade 64 km of dikes and sluices in Nova Scotia (Fairclough, 2019), or implementing new strategies, e.g. the new £63 million seawall at Rossall, Lancashire (Environment Agency, 2018) are based on multi-disciplinary, cost-benefit analysis in areas with highest potential for protection benefits. Representative, site-specific information of HWL and HWHs are needed to support decisions to ensure crest level and defense heights are appropriate, for effective storm hazard mitigation and resilience to future change.

1.1 Case Study

This research focuses on the Severn Estuary (Figure 1a), SW England, as an example of hyper-tidal and funnel shaped estuaries worldwide. The estuary has the third largest mean spring tidal range in the world, up to 12.2 m at Avonmouth due to the funneling effect (Dyer, 1995), which is also known to modulate the local wave climate (Pye & Blott, 2010). The orientation of the mouth of the estuary to the Atlantic Ocean means it is exposed to prevailing swell waves, and the large fetch (up to 6000 km) amplifies wave driven hazards in the outer estuary. The south coastline of the estuary is dominated by energy and port infrastructure and large areas of low-lyingagricultural land, highlighting the need for accurate operational forecasts in this region.

1.2 Outline of the paper

This research quantifies the sensitivity of HWL, HWHs and high water hazard proxies (HWHP) to model coupling along the Severn Estuary coastline. Hazard proxy (HP) is defined as the WL+½ Hs and is used to understand the severity of a condition. 32 model simulations are run in total; a series of eight model simulations are run for four events which represent a potential hazard in Delft3D-FLOW-WAVE. The model is applied to consider waves and circulation in isolation (standalone), the influence of circulation on waves (one-way coupled) and the influence of the circulation on the waves and waves on the circulation (two-way coupled). Wind and atmospheric pressure are included on four of the eight model simulations to investigate wind influence on HWL and HWHs during storms. Water level (WL), significant wave height (Hs) and HP are simulated to explore the sensitivity of each parameter to model coupling (Section 2), and the results (Section 3) quantify uncertainty introduced into the model due to the coupling and forcing processes. Before concluding in Section 5, Section 4 discusses the importance of locally generated winds and coupling processes in simulating Hs and HP in hyper-tidal estuaries, and the implications that uncertainty in storm parameters have on flood warnings and management activities.

2 Method

2.1 Delft3D hindcast of select historic events

The Delft3D modelling system (Lesser et al., 2004) was used to simulate tide-surge-wave propagation across the Severn Estuary for four historic storm events. Delft3D-FLOW simulates hydrodynamic flow under the shallow water assumption, and Delft3D-WAVE simulates the generation and propagation of waves, based on the third-generation spectral wave model Simulating WAves Nearshore (SWAN), which solves the spectral action balance (Booij et al. , 1999). A 2D-horizontal, curvilinear grid of the Severn Estuary extends from Woolacombe, Devon and Rhossili, South Wales in the west, with a maximum resolution of 5 km, to Gloucester in the east with a minimum resolution of 25 m at the coast, to resolve fine-scale processes in shallow water (Figure 1a), and has been validated in Lyddon et al., 2018a, 2018b, 2019. Gridded bathymetry data at 50 m resolution (SeaZone Solutions Ltd. 2013) was interpolated over the 2DH curvilinear grid. Delft3D-FLOW has two open boundaries forced by time-varying, spatially uniform water level, representing the Atlantic Ocean to the west and the River Severn to the east. Delft3D-WAVE was forced with five, space- and time-varying boundary points to the west. Delft3D-WAVE explicitly represents the dissipation of wave energy due to white-capping, bottom friction and depth-induced breaking, and wave generation by wind, and non-linear wave-wave interactions (Deltares, 2014).



Fig 1 a) Delft3D-FLOW-WAVE model domain. Bathymetry relative to CD. Average bias and RMSE (m) of WL and Hs model results for four events to tide gauge and wave buoy observations are shown in brackets; (b) six year Hs record from Scarweather wave buoy; (c) Long-term tide gauge record taken from Ilfracombe, with HWHP grouped based on wind direction at the time of the event. HWL, HWHs, and wind speed (WS) at the time of the events are shown. Horizontal black lines indicate maximum, 90th, 50th and 10th percentile HP thresholds.

Six years of Hs data from the Scarweather Directional Waverider buoy (Figure 1b) (Cefas, 2019) and tide gauge data at Ilfracombe (NTSLF, 2019) were used to identify historical coastal flood and wave hazard events. Hs was isolated when the tide is at or above 5.91 m (the level of lowest high water level in the record), to leave only wave events when overtopping is most likely to have occurred (see Figure 1c). This was used to calculate HP for concurrent water level and wave conditions exceeding this threshold (see colored dots in Figure 1c). Each HP event represents a real event with hazard potential, and was grouped according to the concurrent wind direction, using data from the Met Office weather station at Pembrey Sands (CEDA, 2018). Winds from a southwest and west direction have been shown to generate maximum Hs and contribute to greatest wave hazard in the estuary (Lyddon et al., 2019). Four events with a southwest and west wind direction were selected, which represent the maximum (3 January 2014, 07:00), 90th (16 December 2012, 19:00), 50th (26 January 2014, 01:00) and 10th percentile (30 June 2012, 12:00) HP thresholds (Figure 1c).

The open sea boundary to the west was forced with a time-varying, spatially uniform water level at a 15 minute interval using observation data from Ilfracombe tide gauge (NTSLF, 2018). For WAVE standalone simulations, a constant WL was applied at the open sea boundary, at the level of HWL during the selected event, to eliminate the effect of tidal currents on Hs and variability in WL. Time- and space-varying wave conditions (Hs, wave direction, mean period and directional spread) from the Met Office WAVEWATCH III hindcast (Saulter et al., 2016; Siddorn et al., 2016) were used at five equidistant points along the open sea boundary (see Figure 1a), and were linearly interpolated along the boundary to force the model at 15-minute intervals. A time- and space-varying wind and atmospheric pressure field forced the model domain at hourly intervals, using data originating from the Met Office global unified model (Walters et al., 2014) and extracted from the Extended Area Continental Shelf Model CS3X (Williams & Horsburgh, 2013). All simulations were forced with 15-minute river gauge data from Sandhurst (Environment Agency, 2016) at an up-estuary open boundary (see Figure 1a).

2.2 Model validation and scenario test

Model outputs from two-way coupling of Delft3D-FLOW-WAVE, which represents a complete five-way multi-hazard simulation (tide-surge-wind-wave-river), for the four events were validated at five tide gauge locations (Hinkley Point, Newport, Severn Bridge, Oldbury, Sharpness) and four wave buoy locations (Scarweather, Minehead, Weston-super-Mare, Severn Bridge). Average bias and root mean squared error (RMSE) of WL and Hs were calculated at validation locations (see Figure 1a). The bias is defined as:

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| --- | --- | --- |
|  |  | (1) |

where M represents the model values, O the observed values and the overbar denotes the mean value of the simulated storm event. A value of 0 indicates an unbiased estimate; a positive value indicates the model is over-predicting; a negative value is under-prediction. The RMSE is defined as:

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| --- | --- | --- |
|  |  | (2) |

where a value closer to zero indicates better model performance.

There is good agreement for WL in outer estuary. Hinkley Point has a bias value of 0.08 m and RMSE of 0.34 m, which represents 2.75% of the observed tidal range during the maximum event. Positive bias and larger RMSE values up-estuary indicate the model overestimates WL at Oldbury and Sharpness. Hs is well reproduced, as bias and RMSE values remain close to zero. Wave data used for validation are available along the southern estuarine coastline, where areas of critical energy infrastructure are located highlighting the importance of accurately representing Hs in this region.

The validated Delft3D-FLOW and WAVE model was run from 48 hours before the event to 12 hours after, in a series of eight standalone, one-way or two-way coupled simulations. Delft3D-FLOW and WAVE can run in ‘standalone’ mode with user-defined properties (Delft Hydraulics, 2014). Delft3D-WAVE is used in one-way coupled simulations where the FLOW simulation is completed and then input (offline) into the wave simulation, to account for the effect of flow on waves. Two-way coupled simulations allow dynamic (online) interaction of Delft3D-WAVE with FLOW to account for the effect of waves on current, and the effect of current on waves. The FLOW and WAVE modules exchange information at 15-minute intervals, such as wave radiation stresses and water level conditions needed for wave transformation, to represent two-way wave-current interaction, refraction and depth-induced breaking. The influence of wind is considered in both FLOW and WAVE when included, to represent changing forcing processes. Eight model runs were completed for each of the four historical HP events (32 in total) to explore how model coupling and forcing processes contribute to uncertainty in HWL, HWHs, and HWHP:

1. FLOW
2. FLOW + wind
3. WAVE
4. WAVE + wind
5. FLOW 🡪 WAVE (1-way, FLOW output from 1)
6. FLOW 🡪 WAVE+ wind (1-way, FLOW output from 2)
7. FLOW 🡨 🡪 WAVE (2-way)
8. FLOW 🡨 🡪 WAVE + wind (2-way)

The maximum, mean and median percentage difference in HWL, HWHs, and HWHP were calculated between each model run and model run 8 as:

|  |  |  |
| --- | --- | --- |
|  |  | (3) |

Run 8 is used as the baseline run as it includes all boundary forcing, and has been successfully validated to observational tide and wave data in the estuary. Model results are presented as the % difference between each run and the validated run 8 for the north and south coastline to i) identify which coupling HWL, HWHs and HWHP are most sensitive to and ii) quantify uncertainty introduced into the model due to omitting coupling and forcing processes.

3 Results

HWL and HWHs were extracted from model results every 5 km, from the second row of grid cells in, along the estuary coastline, and HWHP calculated, for each event. Results of the maximum event (3 January 2014) are seen in Figure 2a-c. HWL (Figure 2a) is amplified to a maximum of 11.7 m up-estuary, beyond Newport and Oldbury, due to the funneling effect (Uncles, 1984). HWHs (Figure 2b) is greatest in the outer estuary near Swansea and Porthcawl. HWHs dissipates up-estuary but shows greater sensitivity to coupling and forcing processes. HWHP (Figure 2c) is greatest up-estuary, and shows greatest sensitivity to model coupling and forcing in the outer estuary.

The cumulative effect of wave dissipation as energy propagates up-estuary, i.e. increased white capping as waves steepen and depth-induced breaking and up-estuary cross-section friction, dampens the hazard, therefore analyses are focused in areas where water level and waves are largest, in the lower- and mid-estuary. Maximum, mean and median percentage difference in HWL, HWHs and HWHP between each run with run 8 (solid black line in Figure 2a-c) is calculated for sections of the estuary coastline up to the point where Hs < 10 cm in all simulations, termed the wave limit, to focus on the impact on non-negligible wave conditions (Figure 2d-f). Absolute differences in HWL, HWHs and HWHP between each run with run 8 along the coastline are shown in Figure S1a-c.





Figure 2: Simulated a) HWL; b) HWHs; c) HWHP along the coastline of Severn Estuary starting at Swansea to Gloucester and thence down-estuary towards Woolacombe for maximum event (3 January 2014 07:00); d-f) % difference between each run and run 8. The divide between north and south coastlines (dashed black vertical line) and wave limit where Hs < 10 cm (dashed grey vertical line) is shown. Solid black vertical lines indicate locations of critical infrastructure and coastal towns.

Alongshore maximum, mean and median % difference relative to run 8 for HWL, HWHs and HWHP are presented for the north (Figure 3a, left panels) and south (Figure 3b, right panels) coastline for each event up to the wave limit (Hs < 10 cm), to identify the model’s response to coupling processes. Absolute differences in HWL, HWHs and HWHP are shown in Figure S2.



Figure 3: For the a) north (left panels) and b) south (right panels) coastlines the alongshore maximum, mean and median percentage difference in i) HWL; ii) HWHs; iii) HWHP between model simulations is calculated for the four events with hazard potential calculated using the HP parameter.

3.1 Uncertainty in High Water Level (HWL)

Run 3 and 4 are simulated with a constant water level at MHWST throughout the model domain, and no funneling of the tidal wave to amplify tidal range up-estuary occurs (Figure 2a). Up-estuary % difference exceeds 50%, therefore these are excluded to avoid masking other results. Run 5 and 6 use the model outputs from Run 1 and 2, and are excluded to avoid repetition.

The model shows that runs 1 and 7 generate maximum % difference in HWL along the north and south coastline for all events up to the wave limit, regardless of event severity. . Maximum % difference in HWL is 1.5% between run 8 and 1 for the 50 percentile event, which also represents maximum absolute difference of 0.046 m (Figure S2a). This absolute difference is < 1% of the maximum tidal range. The 90th percentile event shows the least sensitivity to model coupling, where the range in maximum % difference is 0.42% on the north coastline and 0.38% on the south coastline. Run 2generates the smallest percentage difference in HWL along the north and south coastline for all events, indicating locally generated winds are more important than coupling processes when simulating water level, however the differences remain small.

3.2 Uncertainty in High Water Significant Wave Height (HWHs)

Increasing HP threshold increases the % and absolute difference in HWHs on the north coastline, but this trend is less clear on the south coastline. The model highlights up to 90.1% maximum difference in HWHs 150 km up-estuary, near Cardiff, which represents 1.13 m, between run 5 and 8. Figure S3a highlights the substantial % differences in HWHs up-estuary of the wave limit, and the contribution of local atmospheric forcing to wave generation up-estuary.

The maximum absolute difference in HWHs is 1.45 m between runs 5 and 8, which occurs just 20 km up-estuary west of Swansea, and represents a 34.4% difference. The geometry of the north coastline means some stretches of coastline have a more exposed west facing aspect as waves are generated and propagate towards the coast contributing to increased sensitivity to incoming storms with a west-southwest wind direction.

Runs 4 (standalone) and 6 (one-way) include local atmospheric forcing and generate a closer representation of HWHs compared to run 8, with a 39.9% maximum difference. Run 4 and 6 generate a range of –9.2 to 17% mean difference for all events. -51.2% % difference occurs between run 8 and 6, which represents 0.48 m, in shallow, sheltered regions (e.g. Swansea Bay and Cardiff Bay) on the north coastline (Figure S1b) where the one-way simulation generates larger HWHs than two-way simulation. Figure S3b shows one-way simulations underestimate depth-averaged velocities compared to run 8. HWHs is overestimated in one-way simulations as slower wave driven currents in shallow areas may mean waves are not refracted around the coastline, but instead build in height.

3.3 Uncertainty in High Water Hazard Proxy (HWHP)

Runs 1 and 2 are not included in these comparisons as HP is underestimated in the outer estuary when waves are not included as a physical forcing condition (Figure 2f), highlighting the importance of coupling here. Runs 3 and 4are forced with a constant water level and are not included in these comparisons, as HP is greatly underestimated when tide is not included as a physical forcing condition (Figure 2f).

As with HWHs, increasing HP threshold increases the % and absolute difference in HWHP on the north coastline. Run 5 generates maximum % difference in HWHP of 9.02%, representing 0.71 m, with run 8 at 20 km up-estuary on the north coastline. The difference between runs 5 and 8 generates 8.43% difference, 100 km up-estuary on the south coastline, however this represents just 0.27 m. The south coastline is sheltered from approaching storms simulated here from the southwest, as waves do not propagate directly towards the coastline. Therefore hazard is lower than the north coastline.

3.4 Spatial variability of hazard

Each metric is further analyzed up to the wave limit and the entire estuary, indicating the large impact of model coupling and forcing processes on the upper estuary (Table S1). A greater maximum, mean and median % difference for HWL and HWHs occurs when considering the entire estuary coastline. Locally generated winds blow waves into the upper estuary, generating a larger response up-estuary. Conversely, mean and median % difference for HWHP is smaller when including the upper estuary, and maximum % difference in HWHP occurs in the lower estuary shows no difference.

4 Discussion

The model highlights that HWL shows least sensitivity to forcing and coupling processes. The 90 percentile event, which showed smallest range of % and absolute difference, has a wind speed of 9.8 m/s from 232 – 247°, representing the most southerly direction of all HP events. This event may be fetch limited, so wind speed is reduced as it approaches from a more southerly direction to reduce setup (Brown et al., 2012), indicating estuary orientation is important when considering uncertainty in simulated HWL at the coastline.

Accurate prediction of HWHs and HWHP in the outer estuary is important for prediction of wave run-up and wave overtopping, and used to design crest levels of flood defense structures (Sayers et al., 2003; EurOtop, 2018). This is particularly important at the time of high tide, when defense exceedance is most likely (Quinn et al., 2014). Largest absolute changes in HWHs and HWHP occur on sections of the north coastline in the outer estuary with a southwesterly aspect indicating uncertainty, from model and coupling processes, may be sensitive to estuary orientation and coastline geometry in relation to the direction of incoming storm conditions. Accurate model setup for land use planning is critical to avoid under-design, particularly for infrastructure and communities facing the direction of prevailing storms. Defenses could be built too low if the contribution of local winds to sea generated wave hazard is not considered, leading to more regular, low level ‘nuisance flooding’ (Moftakhari et al., 2018). Future flood damages to coastal cities is estimated at over US$1 trillion damage by the middle of the 21st century (Hallegatte et al., 2013), and this could increase if implementation of new grey or green adaptation strategies are built to inaccurate crest levels and are not able to withstand local storm conditions (Temmerman et al., 2013). At £700-5400 / linear meter for seawalls in the UK (Hudson et al, 2015) and US$500 million spent annually in the USA on pre-hazard mitigation (Reguero et al., 2018), over design could be a costly use of funding and resources. Further, a high degree of error in forecasts can propagate through the model cascade (Hewston et al., 2010) when used to then force the boundary of shoreline response models. A 1.45 m underestimation of HWHs in the outer estuary could mean overtopping models (e.g. EurOtop) or inundation depth and extents (e.g. LISFLOOD-FP) do not accurately capture the impacts of extreme events. This could be costly in terms of management activity, or result in financial losses or casualties.

Uncertainty in HWHs can directly impact on coastal populations up-estuary. HWHs in run 3,4,5,6 and 7 is consistently smaller than run 8, as wave propagation may have lost momentum up-estuary due to lack of local wind, or be depth limited (Karimpour et al., 2017). Further, one-way and standalone simulations do not account for the effect of waves on current, which may limit wave setup and propagation up-estuary. Increased uncertainty in HWHs up-estuary of Newport and Weston-super-Mare could underestimate the damaging effects of slopping as a source of coastal flooding (Rego & Li, 2010) or simulated critical threshold levels in operational forecasts may not being reached. Flood warnings may be missed and evacuation orders not sent to coastal communities. This is particularly important in low-lying regions near Oldbury Naite, where simulated HWHP of 9.88 m in run 8 for the maximum HP event would breach earthen embankments of 9.0 to 9.5 m OD (Knight et al., 2015). Locally generated winds are an important component of operational forecasts in coastal zones and estuaries to ensure flood warnings are timely and accurate (Marcos et al., 2019),.

The importance of locally generated winds in accurate representation of Hs has been shown in coastal and estuarine regions worldwide. Maximum wind speed and surface wind stress is shown to be important in simulating hurricane storm surge with the Sea, Lake, and Overland Surges from Hurricanes (SLOSH) model in northeastern US, and can underestimate hazard by 22% if excluded (Mayo & Lin, 2019). The geometry of the mouth of the Mersey Estuary, NW England, at high tide makes it wide enough for substantial local wind-wave generation and for wind setup to elevate the water surface, which should be considered when simulating local flood hazards (Flowerdew et al., 2009). The orientation of hyper-tidal estuaries to prevailing conditions and their large geometries, such as the Bay of Fundy, Canada increase the likelihood that strong winds are coincident with extreme total water levels (Desplanque & Mossman, 1999). Simulated Hs during the Patriot's Day storm in the Bay of Fundy show maximum Hs occurs in the outer Gulf of Maine due to long fetch and wind setup (Marsooli & Lin, 2018), indicating the importance of local winds during extreme storm events. Storm surges are often accompanied by large wind-waves in more than half of coastal regions worldwide (Marcos et al., 2019), thus increasing the potential for coastal flooding and highlighting the need for accurate, local boundary conditions when simulating HWHs.

5 Conclusion

Potential future changes in sea level and storm tracks necessitate accurate prediction of HWL and HWHs in hyper-tidal coastal and estuarine areas for operational forecasts, inundation assessments and cost-effective defence strategies. Delft3D-FLOW-WAVE is used in a series of 32 standalone, one-way or two-way coupled simulations for four historic storm events, to quantify the uncertainty in forecasting HWL and HWHs due to coupling and forcing processes in the Severn Estuary, SW England, used here as a test case for hyper-tidal and funnel shaped estuaries worldwide. HWL shows least sensitivity to both coupling and forcing processes, with 1.5% difference (0.046 m) between the two-way coupled and standalone simulation. For a model domain this size, inclusion of local atmospheric forcing is crucial to continue to add momentum to wave generation up-estuary for accurate HWHs and HWHP prediction. The model shows a 34.4% difference (1.45 m) in HWHs and 9.02% (0.71 m) in HWHP on the north shoreline in the outer estuary, and up to 90.1% difference (1.13 m) in the upper estuary when local atmospheric forcing is excluded from simulations. Aspect and geometry of the coastline to prevailing storm conditions is also an important consideration for coastal hazard prediction. Results highlight how coastal and estuarine numerical models can be best setup to ensure outputs can be used in confidence to force shoreline response models (e.g. for overtopping or inundation studies), to inform design of new coastal protection schemes or flood warnings.

Acknowledgments, Samples, and Data

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Data used in this research are available from sources stated in the reference list.

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