

TRIFIC: The TRIUMF Fast Ion Counter

A. Chester^{a,1,*}, J. Smallcombe^{a,b}, J. Henderson^{a,2}, J. Berean-Dutcher^a,
N. Bernier^{a,c}, S. S. Bhattacharjee^a, A. B. Garnsworthy^a, S. Georges^a,
S. A. Gillespie^a, G. Hackman^a, B. Olaizola^a, O. Paetkau^a, C. J. Pearson^a,
B. Undseth^a, D. Yates^{a,c}

^a*TRIUMF, 4004 Wesbrook Mall, Vancouver, British Columbia, Canada, V6T 2A3*

^b*Oliver Lodge Laboratory, University of Liverpool, Liverpool L69 9ZE, United Kingdom*

^c*Department of Physics and Astronomy, University of British Columbia, Vancouver,
B.C., Canada, V6T 1Z1*

Abstract

The TRIUMF Fast Ion Counter (TRIFIC) is a tilted-grid gas counter detector for identifying the impurities in radioactive ion beams (RIBs). Placed at zero degrees downstream of a primary reaction target at the TRIUMF ISAC-II facility, TRIFIC provides accurate Z identification of beam species on an event-by-event basis at a rate of up to 5×10^5 particles per second and functions as a beam composition monitor at rates up to 5×10^7 particles per second. With this additional level of diagnostics, RIB experiments at TRIUMF are able to reach levels of sensitivity not previously possible. Details regarding the construction and instrumentation of TRIFIC as well as results from the commissioning of the detector are presented.

Keywords: Gas Detector, Ionization chamber, Radioactive ion beams,
Particle identification

*Corresponding Author: chester@frib.msu.edu

¹Present Address: National Superconducting Cyclotron Laboratory, Michigan State University, East Lansing, Michigan 48824, USA

²Present Address: Lawrence Livermore National Laboratory, Livermore, CA 94550, USA

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1. Introduction

Radioactive ion beam (RIB) facilities have created many opportunities to study nuclei far from stability, critical to advancing the understanding of nucleosynthesis, nuclear structure, and reactions. RIB production at TRIUMF, Canada's particle accelerator centre, is achieved through the isotope separation on-line (ISOL) technique: a driver beam—in this case protons from the TRIUMF 520 MeV H^- cyclotron—impinges on a heavy target material. Isotopes created by reactions in the target are extracted and ionized, separated by mass-to-charge ratio, and delivered to an experimental station. Along with the isotope of interest, isobars and isotopes with a similar mass-to-charge ratio may all reach an experiment. Some beams delivered to the ISAC-II facility at TRIUMF require charge state breeding, which can introduce additional stable beam contaminants. As such, it is essential to distinguish the RIB isotope of interest from any contaminant species which may also be present in the beam. Many experiments which take advantage of RIBs are run in so-called inverse kinematics, where a heavy beam nucleus undergoes a reaction on a light target, resulting in forward-focused reaction products. In such applications beam identification can be achieved by placing a detector at zero degrees with respect to the beam axis.

Gas ionization chambers are ideal for this purpose due to their sensitivity to the characteristic range and energy loss of ions, radiation hardness, and the relatively fast signal risetimes which allow for the operation of specially-constructed detectors at high beam intensity. Following the development of several successful fast ion counters [1–4], the TRIUMF Fast Ion Counter (TRIFIC) was designed and constructed to couple with experiments using the TIGRESS γ -detector array [5] at TRIUMF's ISAC-II facility [6].

27 TRIFIC is a compact cylindrical gas counter, mounted along the beam
28 axis directly downstream of TIGRESS and used to identify beam-like ion
29 species based on their characteristic energy loss profile. Signals from the
30 detector are read out through custom-built low-noise preamplifiers and fur-
31 ther analyzed using a GRIFFIN-style digital data acquisition system [7].
32 These aspects of the detector, which distinguish it from other recently de-
33 veloped detectors presented in Refs. [1–4], are discussed further in Secs. 2
34 and 3. TRIFIC is designed for operation in two modes. In the “recoil tag-
35 ging” operational mode, beam-like reaction products are identified on an
36 event-by-event basis in coincidence with signals from TIGRESS and ancil-
37 lary charged-particle detection systems such as the SHARC [8] and Bam-
38 bino [9] segmented silicon detector arrays. At high incident beam rates,
39 TRIFIC may be operated in the so-called “beam monitor” mode, where
40 the intense beam is attenuated (see Sec. 2) and contaminant beam species
41 may be quantified in real time. These two modes of operation are discussed
42 in the subsequent sections in the context of typical types of experiments
43 performed at TIGRESS.

44 *1.1. Transfer reaction experiments with TRIFIC*

45 Reactions in which one or two nucleons are added to or removed from a
46 nucleus (so-called “direct” reactions such as (d,p) or (t,p)) provide a pow-
47 erful tool for studying the single particle structure of exotic nuclei at RIB
48 facilities such as TRIUMF (see, e.g. Ref. [10]). Typically performed at 5–10
49 MeV/A, the direct reaction of interest will often be contaminated by other
50 channels, such as compound reactions or other direct reaction channels,
51 even with a contaminant-free primary beam. Due to the reaction kinemat-

52 ics, recoiling nuclei produced in the reactions are forward focused and can
53 be observed by placing a detector at zero degrees relative to the beam axis.
54 Operating TRIFIC in “recoil tagging” mode allows for the separation of
55 the reaction products of interest from background reactions following un-
56 ambiguous identification of the desired transfer reaction products in the
57 TRIFIC detector. Coincident detection of the reaction products using mul-
58 tiple detection systems (e.g. TIGRESS, TRIFIC, and SHARC) provides a
59 clean tag of the reaction.

60 Additionally, the use of TRIFIC as a zero-degree “recoil tagging” detec-
61 tor has a significant advantage over fast scintillator detectors which have
62 been previously employed for this purpose (see Ref. [11]) because cycling gas
63 through TRIFIC ensures that the detector performance is stable over long
64 periods of time. This is in contrast to the significant loss in performance
65 and efficiency of scintillator detectors as they become radiation damaged
66 from exposure to reaction products and un-reacted beam. TRIFIC in the
67 “recoil tagging” mode is designed to operate with beam intensities up to 1
68 Mpps with a resolving power of $Z/\Delta Z \geq 40$.

69 *1.2. Coulomb excitation experiments with TRIFIC*

70 Great progress is being made in understanding the structure of nuclei
71 far from stability by studying Coulomb excitation (Coulex), where nuclear
72 electromagnetic matrix elements are determined directly from sub-barrier
73 collisions [12–15]. An important question of normalization arises during the
74 analysis of such experiments. It is common to normalize to known strengths
75 of transitions in the target nuclei which are excited simultaneously with the
76 beam in the Coulex process [13]. However to perform such a normalization

77 it is important to have an accurate measurement of both the make-up of the
78 target and of the beam. Moreover, the composition of the beam can change
79 during the measurement period. The precision to which one knows the beam
80 composition is often a significant source of systematic uncertainty, which can
81 constitute a serious limitation to the accuracy of the final measurement.

82 With this in mind, TRIFIC can be used to get an accurate synchronous
83 (real-time) measurement of the beam constituents on a run-by-run basis
84 throughout the course of an experiment. This has the advantage over spo-
85 radic asynchronous measurement (i.e. snapshots of the beam composition),
86 in that rapid shifts in the beam composition which are common due to the
87 complex chemical nature of ISOL targets at facilities such as TRIUMF-
88 ISAC, can be correctly accounted for in order to give the most accurate
89 integrated yields over time. When in this “beam monitor” mode of oper-
90 ation TRIFIC requires only a representative sample of the full beam rate.
91 Furthermore, in such experiments the selection of particles being detected
92 is dominated by un-reacted beam particles which suffer significantly less an-
93 gular dispersion than that of reaction products. As such, the tilt of the grids
94 (see Sec. 2) has a smaller effect on the range measurement of the particles
95 and an overall higher $Z/\Delta Z$ resolving power is achieved. One final boon of
96 this operational mode is that different species need not be clearly resolved
97 on an event-by-event basis, as only a ratio measurement is required. This
98 enables the device to be operated closer to the resolving limit.

99 **2. Detector construction**

100 TRIFIC is a tilted-grid gas ionization chamber, consisting of multiple
101 wire grids mounted in a 73 mm radius cylindrical chamber, typically oper-

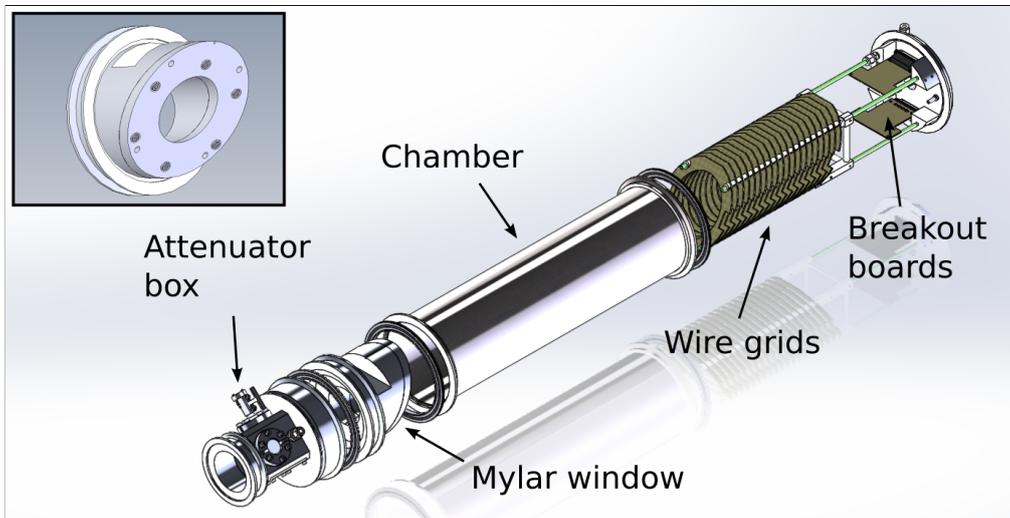


Figure 1: Exploded view of the TRIFIC detector with key components labelled. A description of the components is given in the text. The inset shows the downstream side of the Mylar entrance window. Beam enters the detector from the lower left. (Color online).

102 ated using 50–100 Torr of CF_4 gas. TRIFIC was developed from the design
 103 of a similar detector used at the HRIBF facility at Oak Ridge National
 104 Laboratory [1]. An upstream attenuator box houses two $\times 0.1$ attenuator
 105 foils which can be used together to accommodate beam intensities up to 50
 106 Mpps in the “beam monitor” operational mode along with a Faraday cup
 107 for beam tuning and diagnostics. A schematic drawing of the detector’s
 108 important constituent parts is shown in Fig. 1. A cross-sectional diagram
 109 is shown in Fig. 2, and a photo of the detector components presented in
 110 Fig. 3.

111 The TRIFIC electrode grids are constructed from 2.6 mm thick PCB
 112 boards with an elliptical opening tilted by 30° such that the electrodes
 113 present a circular profile with a 50 mm radius along the beam axis. Tilting

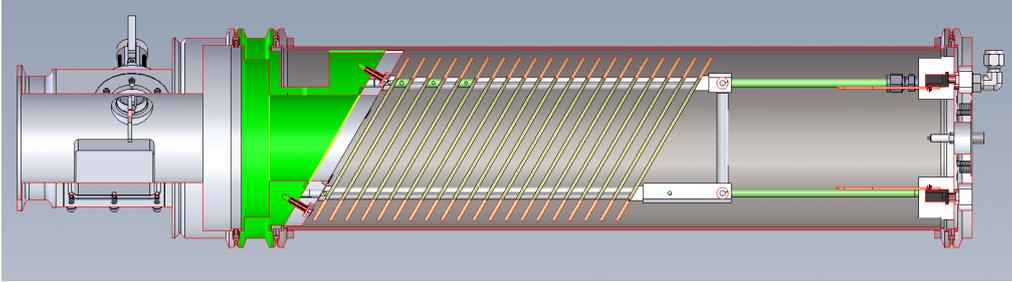


Figure 2: A cross-section of the TRIFIC detector showing the various components described in Sec. 2. The Mylar entrance window mount is highlighted in green. Beam enters from the left. (Color online).

114 the electrodes aligns the electric field such that electrons and ions created
 115 within the gas drift away from the beam axis thereby minimizing recomb-
 116 nation effects. Fifty 20 μm diameter gold-coated tungsten wires are soldered
 117 to the electrodes at a 2 mm pitch giving a total transmission per grid of
 118 99%. TRIFIC is nominally operated with 24 electrodes, which are individ-
 119 ual mounted on G-10 rods and separated by 10 mm PEEK spacers³. The
 120 24 grid setup can accommodate ion ranges up to 30 cm with a total trans-
 121 mission of $\approx 79\%$ from the first to the last grid allowing for good flexibility
 122 in detecting ions in the 5–10 MeV/A range achievable at TIGRESS. For
 123 example, ^{20}Ne at 5.25 MeV/A (105 MeV), ^{40}Ar at 5.75 MeV/A (230 MeV),
 124 and ^{84}Kr at 6.31 MeV/A (530 MeV) all have a range of 30 cm in 95 Torr
 125 of CF_4 gas [16].

126 To create the electric field of TRIFIC different bias is applied to alter-
 127 nating grids, creating 2 groups of electrodes (cathodes and anodes). The
 128 capacitance between adjacent grids was measured to be 15.8(5) pF. High

³Up to 48 grids can be accommodated using 5 mm PEEK spacers that are also available but were not used in the presented work.

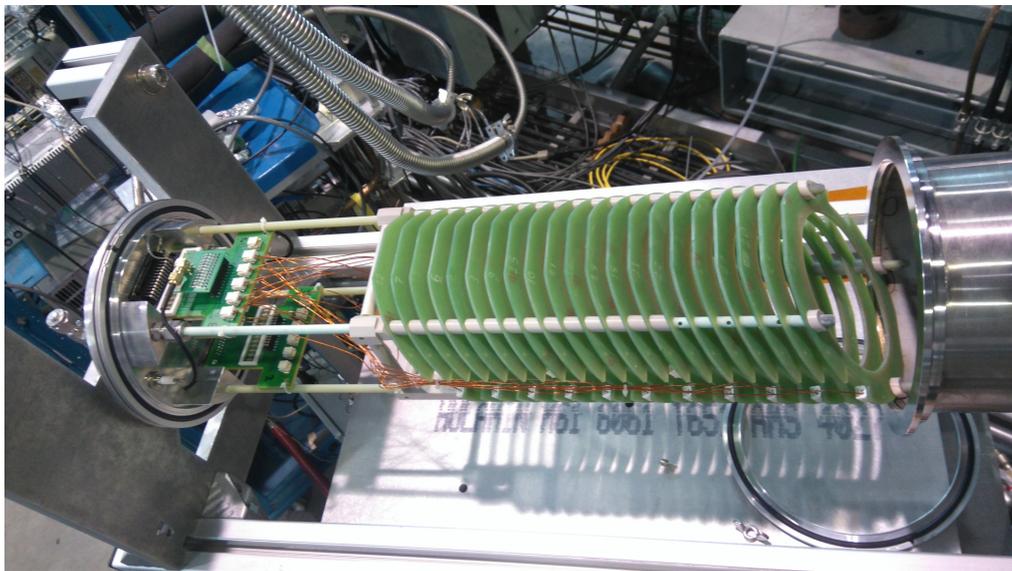


Figure 3: A photo of the interior components of the TRIFIC detector labelled in Fig. 1. The grids are described in detail in Sec. 2. The breakout boards containing the internal RC buffer circuits are visible on the left of the figure. The beam enters the detector from the right in this photograph. (Color online).

129 voltage bias is applied separately to the cathode and anode grids via two
130 RG-59 cables with SHV connectors which are connected to a mesytec MHV-
131 4 power supply [17]. External high-pass filters consisting of a $1\text{ M}\Omega$ resistor
132 (R_{HV}) and $1\text{ }\mu\text{F}$ capacitor (C_{HV}) are used to suppress low-frequency noise
133 from the power supply. Signals from individual electrodes are read out
134 through an internal RC buffer circuit composed of an exchangeable $1\text{ M}\Omega$
135 resistor (R_{B}), through which HV bias is delivered, and a 47 pF capacitor
136 (C_{B}), which isolates the HV from the signal output. These components
137 are highlighted on the block diagram of the detector electronics shown in
138 Fig. 4. The buffer capacitors are vacuum potted with epoxy for isolation
139 and to prevent arcing at low operating pressure. The buffer circuit can ac-
140 commodate up to 4 groups of 12 signals giving a maximum readout capacity
141 of 48 individual channels.

142 TRIFIC is separated from the beamline vacuum by an entrance window
143 with a radius of 35 mm which protrudes inside the chamber and is tilted
144 at 30° similar to that described in Ref. [1]. A schematic of the window is
145 shown on the inset of Fig. 1. The window opening is located 2 cm upstream
146 from the first set of electrode wires and consists of aluminized Mylar which
147 is fixed in place with a bracket machined to match the 30° tilt and is sealed
148 using an O-ring. Windows experience some limited distortion towards the
149 target while under pressure. Six μm thick Mylar windows were tested at
150 pressure differentials up to 300 Torr.

151 *2.1. Biasing scheme*

152 The effect of different biasing schemes on the electron transport in
153 TRIFIC was investigated using the Garfield++ simulation package [18].

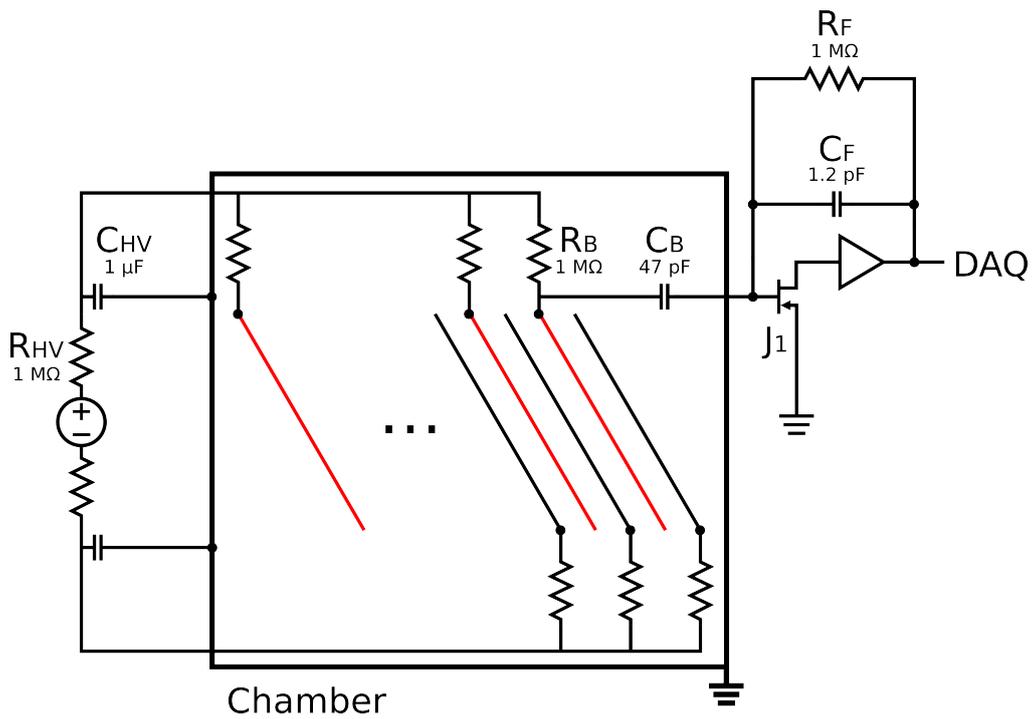


Figure 4: Block diagram of TRIFIC showing the HV filter (R_{HV} and C_{HV}) and buffer circuit (R_B and C_B) described in Sec. 2 as well as a single channel of the preamplifier circuit (J_1 , R_F and C_F) described in Sec. 2.2. Some typical component values are shown. For details on the specific sub-systems, refer to the text. The cathode and anode grids are shown in black and red, respectively. (Color online).

154 Field maps and electron drift lines calculated by Garfield++ for a constant
155 potential difference of 244 V between the electrode grids are shown in Fig.5.
156 During the commissioning tests, it was demonstrated that a negative bias
157 voltage on the first electrode grid (initially at ground) significantly improved
158 the signals recorded on the second. This improvement arises due to the sup-
159 pression of slow charge collection on the second grid from electron-ion pairs
160 created in the region between the Mylar window and the first electrode. As
161 expected, the Garfield++ simulations confirmed that supplying a negative
162 bias to the first electrode group creates an electric field which repels elec-
163 trons created from ionization upstream of the first grid. Calculated drift
164 lines demonstrating this effect are shown in the bottom two panels of Fig. 5.

165 The optimal biasing scheme determined from the simulations was to split
166 the bias evenly across the anodes and cathodes. This scheme minimizes the
167 potential difference between the anodes/cathodes and the detector elements
168 which are kept at ground, such as the chamber and window. As a result,
169 sparking between these elements is minimized and stable running condi-
170 tions with higher electric fields in the active volume of the detector can be
171 achieved. Additionally, the fringe effects at the edges of the grids are also
172 minimized as shown in Fig. 5.

173 *2.2. TRIFIC electronics*

174 A set of 24-channel, low-noise, two-stage gain charge-sensitive preampli-
175 fier modules, instrumented with a JFET for noise reduction, have been de-
176 signed and constructed by the TRIUMF Electronics Development Group for

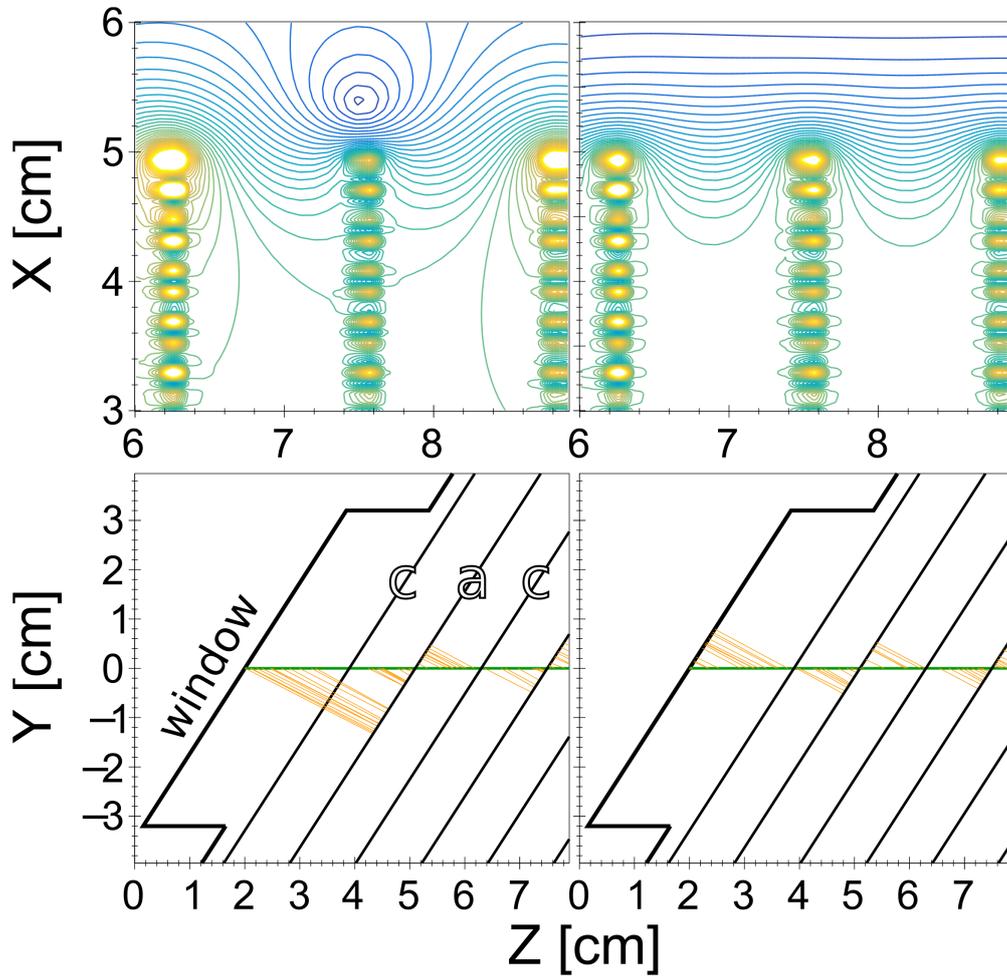


Figure 5: Field map contours (top) and electron drift lines (bottom) calculated by Garfield++ for a constant potential difference of 244 V between the cathode and anode grids. [Left] Cathode voltage = 0 V, anode voltage = +244 V. [Right] Cathode voltage = -122 V, anode voltage = +122 V. Electron drift lines (thin orange lines) from the beam ionization track (thick green lines) are shown in the bottom two panels. The Mylar entrance window, cathode (c) and anode (a) grids are labeled on the bottom left panel. (Color online).

177 use with TRIFIC ⁴. The multiple-channel readout capability of the custom
178 preamplifiers give TRIFIC a higher degree of segmentation than described
179 in Ref. [1].

180 Three versions of the module have been constructed. In each, low-noise
181 amplification is achieved using NXP BF862 JFETs [19] (J_1) with a noise
182 specification of $0.8 \text{ nV}/\sqrt{\text{Hz}}$ at 100 kHz and ADI ADA4897-1 amplifiers [20]
183 with a noise specification of $1 \text{ nV}/\sqrt{\text{Hz}}$ at 1 kHz. A preamplifier circuit is
184 shown on Fig. 4 for a single TRIFIC channel. Different total gain and
185 shaping times are set for each module. The first is a slow-decay ($R_F = 30$
186 $\text{M}\Omega$, $C_F = 1.2 \text{ pF}$, $\tau_{RC} = 36 \text{ }\mu\text{s}$), high-gain ($11\times$) module designed for off-
187 line tests with α -particle sources, while the second and third modules have
188 a fast-decay ($R_F = 1 \text{ M}\Omega$, $C_F = 1.2 \text{ pF}$, $\tau_{RC} = 1.2 \text{ }\mu\text{s}$) with low- ($2\times$) and
189 medium-gain ($5\times$) respectively, for use in high-rate in-beam experiments
190 at TIGRESS. The total power consumption of one 24 channel module is
191 $+6 \text{ V}$ at 384 mA and -6 V at 144 mA. Each preamplifier module is housed
192 in a shielded $60 \times 110 \times 30 \text{ mm}$ ($l \times w \times h$) box. Individual TRIFIC
193 electrodes are read out through a single channel as shown on Fig. 4 and
194 input to a 100 MHz, 14 bit ADC on a GRIF-16 card in the GRIFFIN
195 DAQ architecture [7]. Detector hit information such as time and charge are
196 determined by the standard GRIFFIN digital signal processing algorithms
197 described in Ref. [7], with optimization discussed in Sec. 3.2. Waveform
198 traces can also be written to disk for further analysis.

199 TRIFIC was tested off-line using a Pu-Am-Cm 3α source. TRIFIC
200 was operated with 91.2 Torr of CF_4 gas during these tests. The source

⁴A set of single-channel ORTEC 109a preamplifier modules were used with TRIFIC previously.

201 was mounted 5 mm from the first electrode and collimated through a 2 mm
 202 aperture in order to collimate the emitted α particles along the z -axis of the
 203 detector. A Bragg curve for the emitted particles was measured and is shown
 204 in Fig. 6. The energy resolution of the individual grids is approximately 1.6
 205 MeV which is not sufficient to resolve the three α -particle energies.

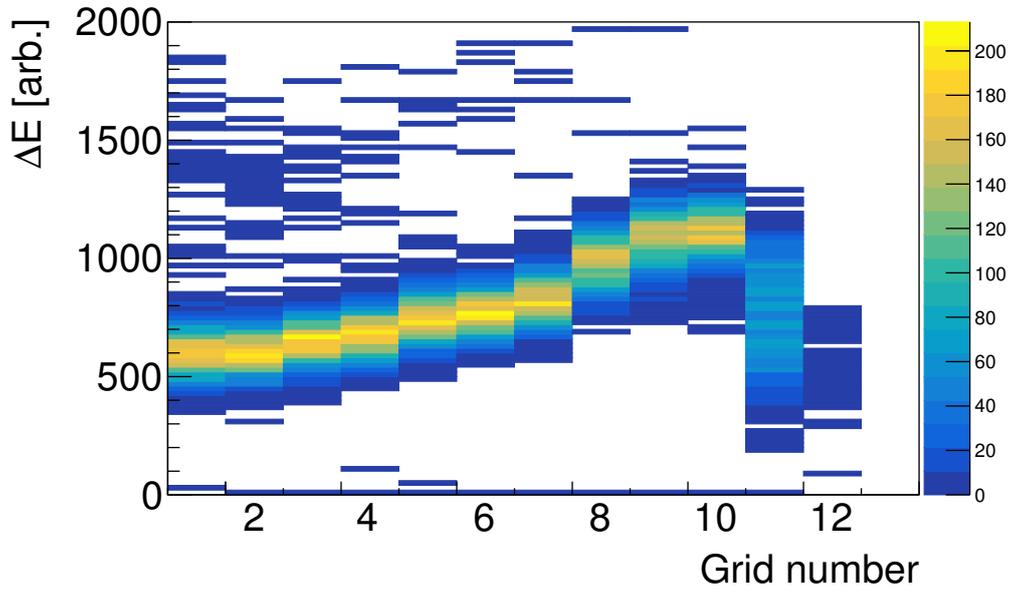


Figure 6: Bragg curve showing the energy deposited in each grid versus the grid number measured for a 3α source. The approximately 1.6 MeV (FWHM/centroid) energy resolution is insufficient to resolve the three α emitters. (Color online).

206 2.3. Reduced field optimization

207 Off-line analysis of waveform traces from the individual grids was per-
 208 formed in order to minimize the charge collection time, which manifests as a
 209 shorter observed signal risetime. The charge collection time was minimized
 210 by minimizing the risetime as a function of the pressure-reduced field E/P
 211 by changing bias voltages applied to the anode and cathode grids while

212 keeping the CF_4 gas pressure constant at 91.2 Torr. A plot of the signal
213 risetime against the reduced field is shown in Fig. 7. A third-order poly-
214 nomial fit to the minimum gave an optimum pressure-reduced field E/P
215 of approximately 2 V/cm/Torr. The behavior of the signal risetime at dif-
216 ferent reduced fields is governed by a complex interplay of many different
217 factors which depend on the gas properties and charge collection process.
218 A reduction in electron drift speed in CF_4 as the reduced field strength ap-
219 proaches 10 V/cm/Torr has been experimentally observed [21], and suggests
220 that a monotonic dependence of the signal rise time as a function of the re-
221 duced field should not be expected. Instead, the detector performance was
222 characterized and optimized. Due to differences in the preamplifier electron-
223 ics, signal risetimes of ≈ 120 ns were observed in-beam using the fast-decay
224 modules.

225 *2.4. Gas handling system*

226 Tetramethylfluoride (CF_4) gas is the standard gas used with TRIFIC.
227 Running the detector at a high count rate requires that the ion and elec-
228 tron transport in the gas is fast: CF_4 satisfies this requirement with respect
229 to other perfluoroalkanes [22], and has been used in other recently com-
230 pleted high-rate gas counters [1–4]. Additionally, the drift velocity does not
231 saturate in the expected operating range ($E/P \approx 1\text{--}5$ V/cm/Torr) of the
232 detector [21]. Gas pressure inside TRIFIC is controlled during operation
233 using a system consisting of an MKS Type 622C Baratron gauge for moni-
234 toring the gas pressure and an Omega CN76000 process controller operated
235 by a MKS 247C mass flow controller power supply unit. Typical gas flow
236 rates are on the order of 10 sccm, giving a total cycle time of approximately

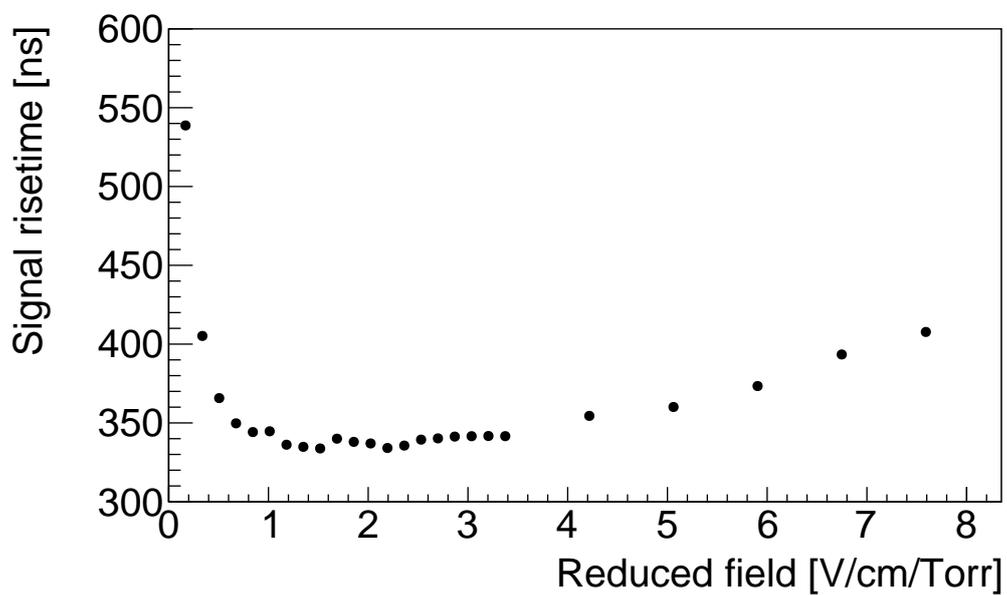


Figure 7: The observed signal risetime as a function of the reduced field. Risetime was defined as the time required for the signal to rise from 10% to 90% of its maximum value. The CF_4 gas pressure was held constant at 91.2 Torr and the applied bias was varied. A minimum occurs at pressure-reduced field E/P of approximately 2 V/cm/Torr.

237 2 hours for 100 Torr operating pressure at 20° C.

238 **3. TRIFIC commissioning**

239 *3.1. Resolving power*

240 The Z resolving power of TRIFIC was tested experimentally in-beam
241 with a cocktail beam consisting of ^{86}Kr ($Z = 36$) and ^{86}Sr ($Z = 38$) ions at
242 an energy of 4 MeV/A (344 MeV). Contaminant species ^{63}Cu (252 MeV,
243 $Z = 29$) and ^{40}Ar (160 MeV, $Z = 18$) were also identified in the beam
244 provided by the TRIUMF Off-Line Ion Source (OLIS) [23]. During this test
245 TRIFIC was operated with 60 Torr of CF_4 gas.

246 Incident charged particle species with different atomic number Z can be
247 separated in TRIFIC due by the differences in their characteristic energy-
248 loss Bragg curves. A particle identification (PID) plot of the energy loss in
249 grids 1–5 ($\Delta E1$) vs the energy deposited at the end of the ion’s range in
250 grids 15–19 ($\Delta E2$) is shown in Fig. 8. Clear loci appear for the primary
251 beam constituents ^{86}Kr and ^{86}Sr as well as the ^{63}Cu and ^{40}Ar contami-
252 nants originating from the ion source. Relative locations of the loci for
253 the detected ions was determined using simulated energy loss curves. The
254 vertically-distributed structures appearing below the ^{86}Kr peak on the $\Delta E2$
255 axis result from the ion hitting one of the wires in the section of the detec-
256 tor where the $\Delta E2$ signal is measured. These features are present for all
257 species, but are most clearly visible for the most intense beam component
258 ^{86}Kr . The data were taken at an incident beam rate of 1 kpps. A separation
259 of 5.2σ between the centroids of ^{86}Kr and ^{86}Sr was determined from a bi-
260 variate normal distribution fit to the data. This leads to a resolving power

261 at 3 FWHM of $Z/\Delta Z \approx 14$ and a separability at 1 FWHM of $Z/\Delta Z \approx 42$
 262 in the “beam monitor” mode.

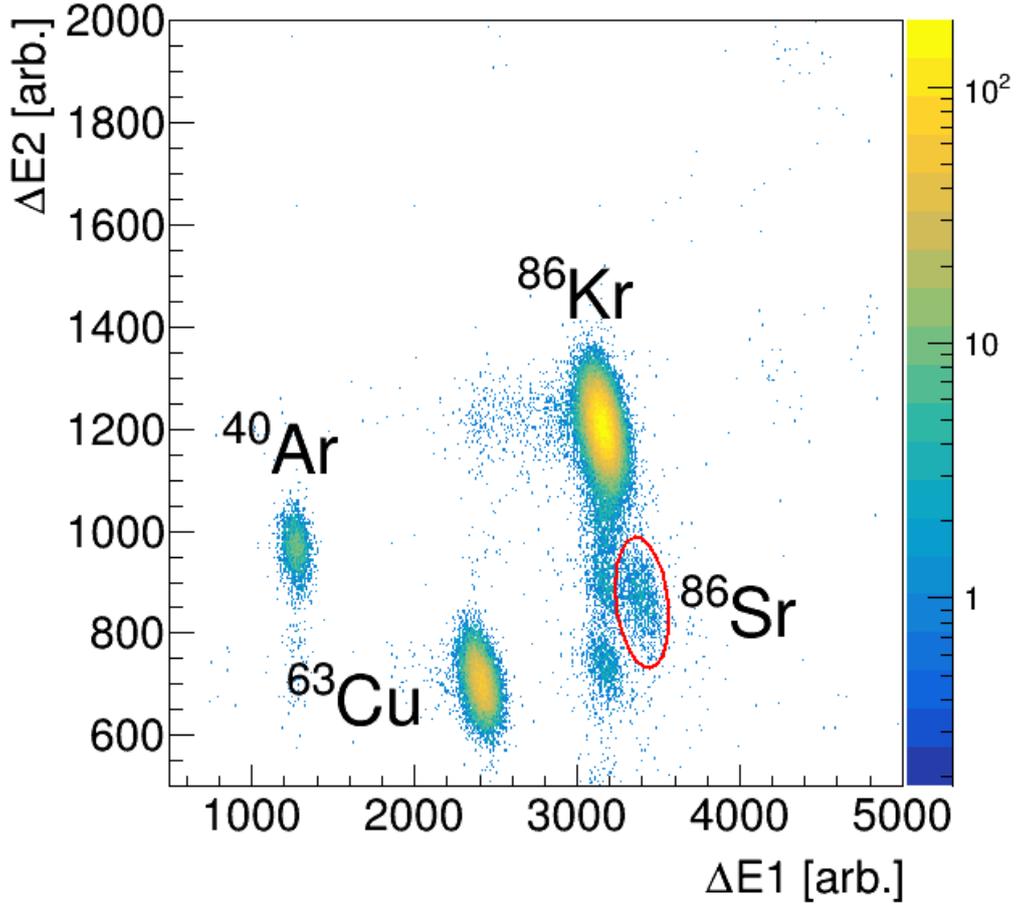


Figure 8: A PID plot demonstrating the separation between various charged particle species ^{86}Sr ($Z = 38$) ^{86}Kr ($Z = 36$), ^{63}Cu ($Z = 29$) and ^{40}Ar ($Z = 18$) at a beam intensity of 1 kpps. A separation of 5.2σ between ^{86}Sr and ^{86}Kr was achieved by plotting energy loss recorded in grids 1–5 ($\Delta E1$) against the energy loss in grids 15–19 ($\Delta E2$). The structures distributed vertically below the ^{86}Kr peak result from the ion hitting one of the wires in the $\Delta E2$ section. (Color online).

263 *3.2. High rate performance*

264 The high-rate performance of TRIFIC was assessed at beam intensities
265 of up to 500 kpps. For these tests, TRIFIC was operated at 95 Torr CF₄.
266 A pure beam of ⁴⁰Ar at 6.75 MeV/A (270 MeV) was provided by OLIS.

267 Signal processing parameters of the GRIFFIN DAQ software described
268 in Ref. [7] were optimized in order to operate TRIFIC with beam intensities
269 up to 500 kpps. Parameters of the pulse-height evaluation algorithm were
270 chosen such that the evaluation occurred in under 1 μs. Signal differenti-
271 ation and integration shaping parameters were set to 260 ns and 200 ns,
272 respectively. Pole-zero correction parameters were optimized on a channel-
273 by-channel basis at low rate. The range of the pole zero parameters was
274 1.063–1.205 μs, in good agreement with the nominal preamplifier decay con-
275 stant $\tau_{RC} = 1.2 \mu\text{s}$. Following these optimization steps, the beam intensity
276 was increased in steps up to 500 kpps to assess the detector performance.
277 The performance of the detector was analyzed at beam intensities of 10,
278 50, 150, and 500 kpps. In the presented data the DAQ was operated in a
279 pileup-rejection mode for optimum resolution, with an enforced deadtime of
280 250 ns between accepted events. Operating in this mode, at 500 kpps 23%
281 of events are lost. The DAQ can alternatively be used in pileup-processing
282 mode [7], in which case only 12% of events cannot be resolved due to coin-
283 cidence summing and pileup.

284 Energy distributions corresponding to the interaction of a single ⁴⁰Ar
285 ion in the first anode grid were fit with a skewed Gaussian function in order
286 to determine the energy resolution. The measured energy distributions in
287 the first anode grid of TRIFIC are shown in Fig. 9 and the corresponding
288 resolutions determined from the fit to the data are presented in Table 1.

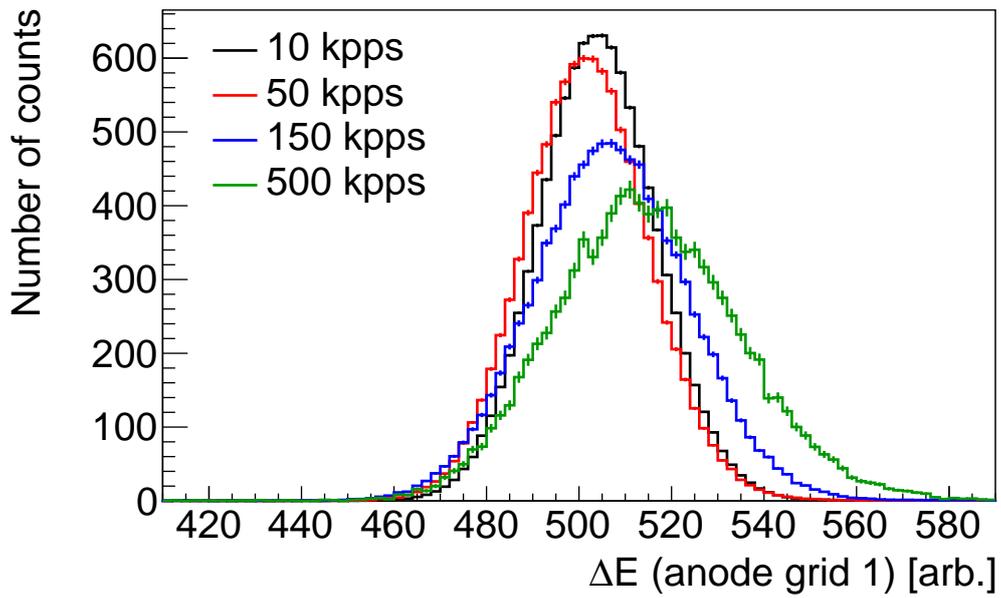


Figure 9: Energy distributions in the first anode grid of TRIFIC measured at 10, 50, 150, and 500 kpps demonstrating the change in energy resolution as a function of beam intensity. The distributions have been normalized to have the same area. The resolutions determined from fitting a skewed Gaussian to the data are given in Table 1. (Color online).

289 Up to 50 kpps, almost no change in the resolution was observed. Increasing
 290 the beam rate to 150 kpps resulted in energy resolution which was approx-
 291 imately 30% worse than the low-intensity data. At 500 kpps the resolution
 292 was approximately 50% worse. In all cases, the energy resolution given by
 293 FWHM/centroid was measured to be less than 10%. TRIM [16] calculations
 294 of the first anode signal region determined the energy straggling to be 1.8%
 295 of the mean energy deposited. The transmission per grid was measured to
 296 be $\approx 98.5\%$ to each successive grid, consistent with the 99% transmission
 297 per grid expected from the design.

Table 1: Measured energy resolution (FWHM/centroid) of the first anode grid in TRIFIC
 as a function of the beam intensity determined by fitting the data shown in Fig. 9 with
 a skewed Gaussian function. The uncertainties at 1σ are given in parenthesis.

Beam intensity [kpps]	Resolution [%]
10	5.910(5)
50	6.234(9)
150	7.714(15)
500	9.01(5)

298 *3.3. Operation of TRIFIC with TIGRESS*

299 Operation of TRIFIC in coincidence with TIGRESS in the “recoil tag-
 300 ging” mode is an important feature of the detector as described in Sec. 1.1.
 301 A test experiment to identify the reaction products of the $^{40}\text{Ar} + \text{d}$ reaction
 302 on an event-by-event basis was performed. The TRIFIC setup and ^{40}Ar
 303 beam properties were the same as described in Sec. 3.2. Four TIGRESS
 304 detectors were placed at 90° relative to the beam axis and a $5 \text{ mg/cm}^2 \text{ CD}_2$

305 (deuterated polyethylene) target was installed at the target position. Data
 306 were collected for approximately 15 hours with a beam intensity of 10 kpps.

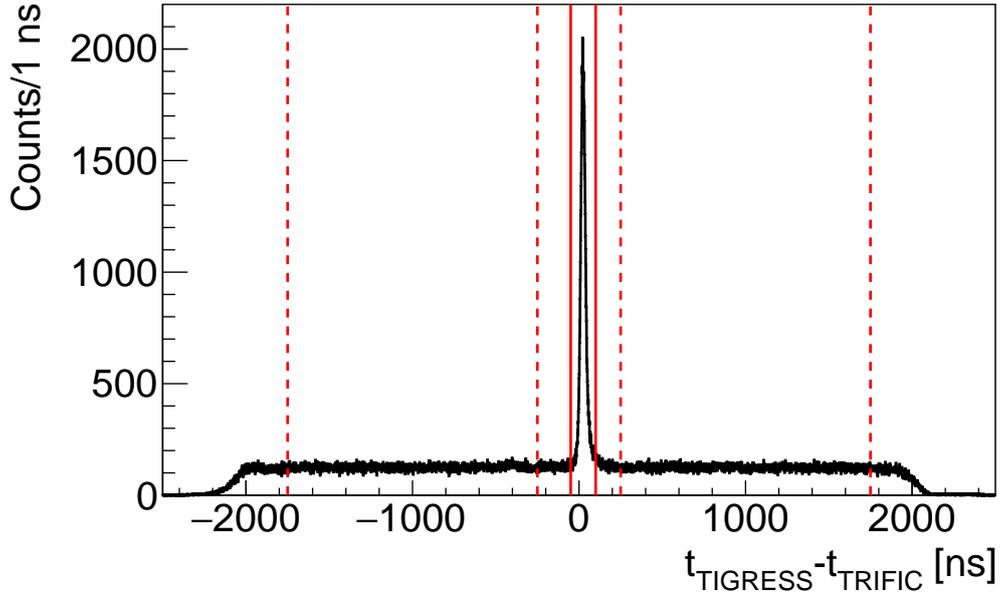


Figure 10: Time coincidence spectrum between events in TIGRESS and the first anode grid of TRIFIC. The gating region for coincident events is shown by the solid lines and the gating region for time-random events used for suppression of background is shown by the dashed lines. (Color online).

307 Timing information for measured detector hits was determined using
 308 the event timestamps and the CFD algorithm in the GRIFFIN DAQ. The
 309 time difference between events in TIGRESS and events in the first anode
 310 grid of TRIFIC was used to identify the coincident detection of a γ -ray
 311 in TIGRESS and a beam-like heavy ion in TRIFIC. The time difference
 312 spectrum is shown in Fig. 10. A 150-ns wide time gate was set around the 32
 313 ns FWHM prompt-coincidence peak. Time-random events were identified
 314 for background subtraction in the analysis of the γ -ray data.

315 In order to identify the reaction products of interest, a PID plot similar

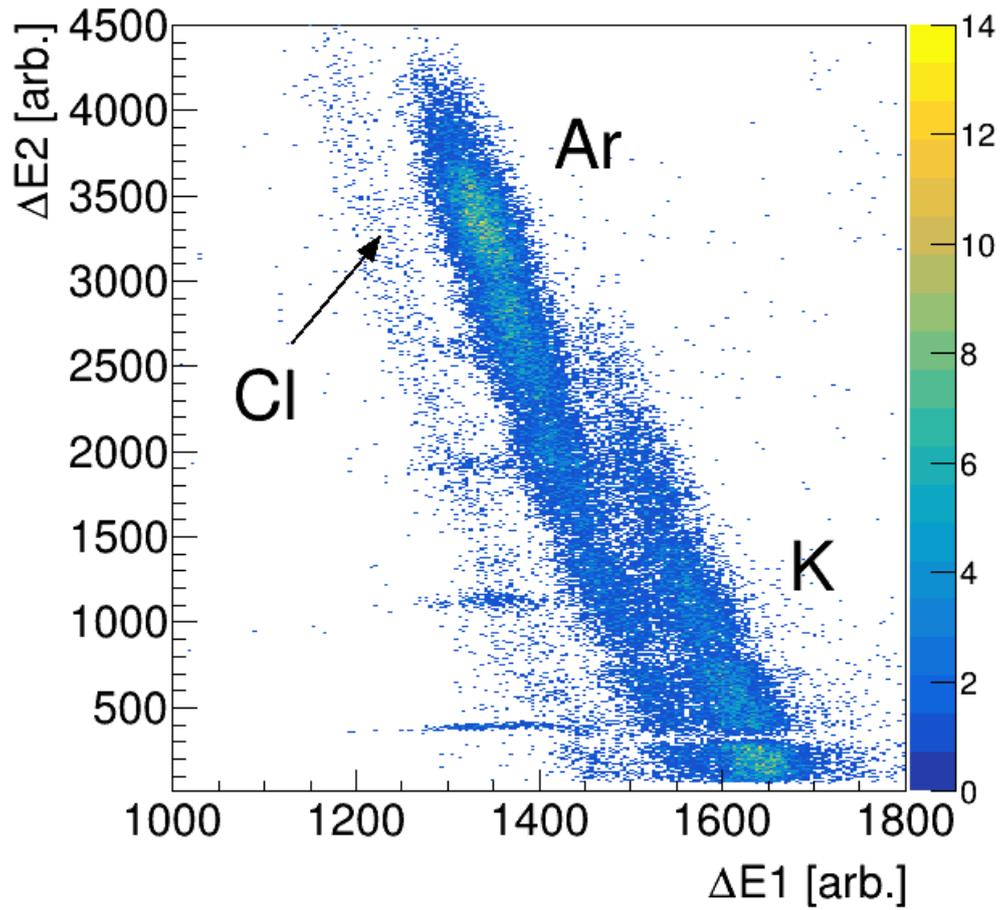


Figure 11: A particle identification plot for the TIGRESS test experiment described in Sec. 3.3. Beam-like Cl, Ar, and K nuclei are separated by plotting the summed energy deposits in grids 1 and 2 ($\Delta E1$) against summed energy deposits in grids ≥ 6 ($\Delta E2$). For a detailed discussion of the structure of this plot refer to Sec. 3.3. (Color online).

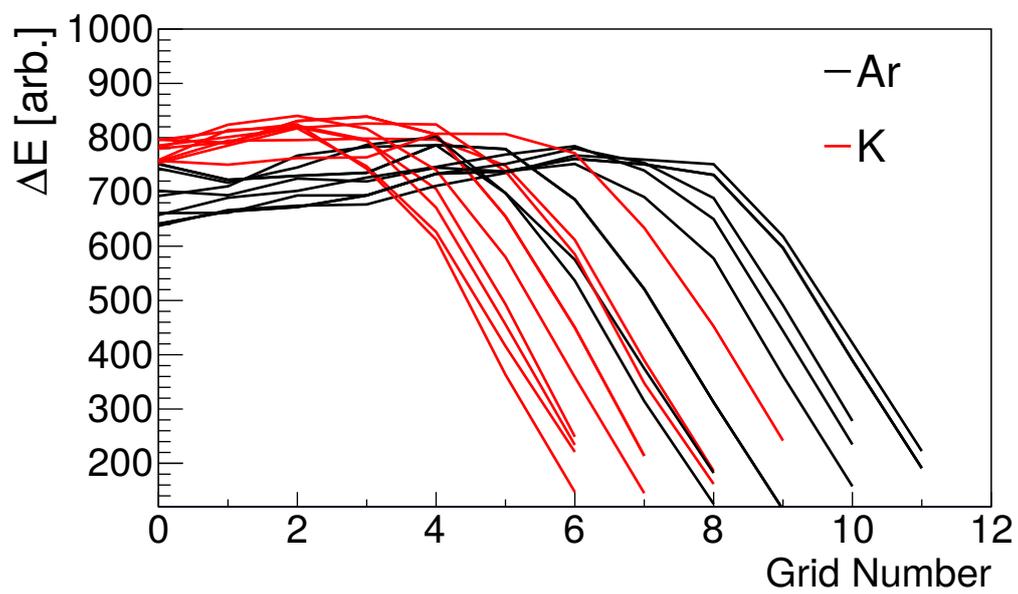


Figure 12: Particle-gated Bragg curve traces for Ar and K in coincidence with events in TIGRESS. Ten traces are shown for each ion. Each trace shows the grid-by-grid energy deposits for a single ion interacting in TRIFIC. The two nuclei with $\Delta Z = 1$ can be distinguished by a combination of the energy deposits and ion range. (Color online).

316 to that shown in Fig. 8 was constructed. Energy deposits in grids 1 and 2
 317 were summed to define the $\Delta E1$ signal and the $\Delta E2$ signal was taken from
 318 the summed energy deposits in grids ≥ 6 . The resultant PID plot of TRIFIC
 319 events in coincidence with TIGRESS demonstrating a clean identification
 320 of Ar, K, and Cl recoils is shown in Fig. 11. Substructures in Fig. 11 result
 321 from the combination of multiple grids. Vertical gaps, seen in the Ar and K
 322 loci, result from the energy thresholds of the individual grids present in the
 323 summing region chosen to define the $\Delta E2$ signals. Vertically-distributed
 324 structures observed between $\Delta E1 = 1300$ and $\Delta E1 = 1400$ result from
 325 incident Ar ions hitting one of the wires in the $\Delta E2$ summing region, similar
 326 to those appearing on Fig. 8 and discussed in Sec. 3.1.

327 Gates were set in the PID spectra on the three identified ion species.
 328 Bragg curves gated on the Ar and K distributions identified in Fig. 11 are
 329 shown in Fig. 12, demonstrating that the two nuclei with $\Delta Z = 1$ are
 330 clearly distinguished by their stopping powers. The broad range distribu-
 331 tions shown in Fig. 11 arise from a combination of the reaction Q-values
 332 and the wide range of possible reaction energies due to the energy loss in
 333 the thick target. Particle-gated γ -ray spectra for events coincident with the
 334 detection of Ar, K, or Cl nuclei are shown in Figs. 13, 14, and 15 respec-
 335 tively. The γ -ray energies have been Doppler-corrected due to the decay in
 336 flight and a background subtraction of time-random events was performed.

337 A number of transitions in ^{41}Ar associated with the $^{40}\text{Ar}(d,p)^{41}\text{Ar}$ re-
 338 action were observed. The 167.1 keV $\frac{5}{21}^- \rightarrow \frac{7}{2\text{g.s.}}^-$ transition, 348.7 keV
 339 $\frac{3}{21}^- \rightarrow \frac{5}{21}^-$ transition, 516.0 keV $\frac{3}{21}^- \rightarrow \frac{7}{2\text{g.s.}}^-$ transition, and the 1186.6 keV
 340 $\frac{3}{22}^- \rightarrow \frac{5}{21}^-$ transition were identified in the data. Also present is the 1460.8
 341 keV $2_1^+ \rightarrow 0_{\text{g.s.}}^+$ transition from inelastic excitation of the ^{40}Ar beam. Tran-

342 sitions in ^{40}K following the $^{40}\text{Ar}(d,2n)^{40}\text{K}$ reaction were also observed. Two
 343 γ -rays in this nucleus were identified: the first at 770.3 keV resulting from
 344 the $2_1^- \rightarrow 4_{\text{g.s.}}^-$ transition and the second at 891.4 keV from the $5_1^- \rightarrow 4_{\text{g.s.}}^-$
 345 transition. No transitions from other isotopes were conclusively identified
 346 in the K gated spectrum. Previous studies [24] found that the $^{40}\text{Ar}(d,n)^{41}\text{K}$
 347 channel primarily populates the ground state and $\frac{7}{2}_1^-$ state. Due to the long
 348 lifetime of the $\frac{7}{2}_1^-$ state, no γ -rays are expected to be observed. In the Cl
 349 gated spectrum, the 1745.7 keV $0^-, 1^- \rightarrow 2_{\text{g.s.}}^-$ transition in ^{38}Cl following
 350 the $^{40}\text{Ar}(d, \alpha)^{38}\text{Cl}$ reaction was observed and is shown on Fig. 15.

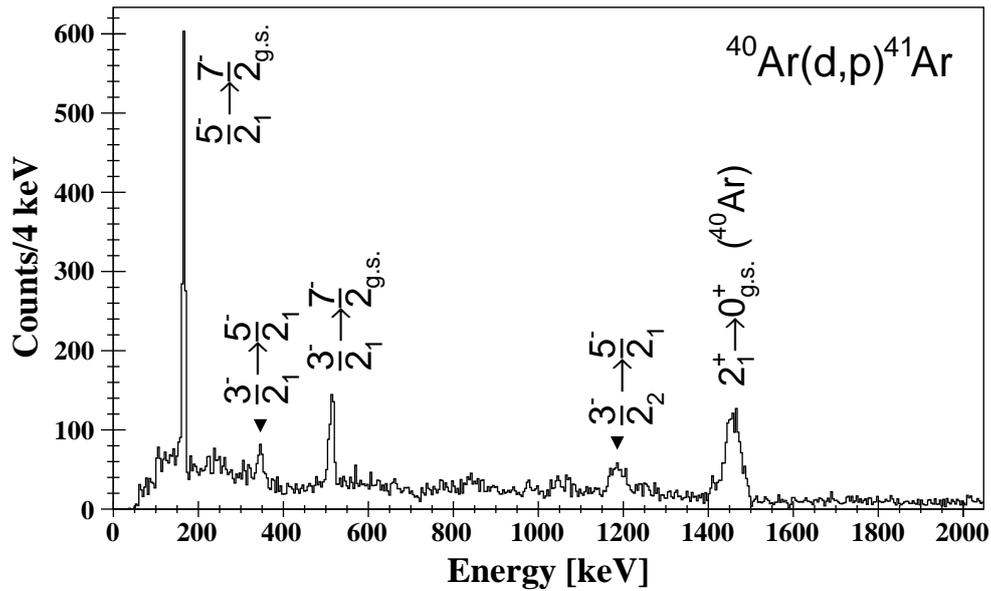


Figure 13: Doppler-corrected, background-subtracted γ -ray spectrum in coincidence with the detection of an Ar nucleus in TRIFIC. Known transitions in ^{41}Ar observed following the the $^{40}\text{Ar}(d, p)^{41}\text{Ar}$ reaction are labeled. The 1460.8 keV transition from the inelastic excitation of the ^{40}Ar beam is also shown.

351 Gamma-rays were successfully detected in coincidence with events in

352 TRIFIC at 10 kpps. The various reaction products of the $^{40}\text{Ar} + \text{d}$ reaction
 353 could be identified by their characteristic energy loss in the gas. Clean
 354 separation of γ -rays arising from decays in $^{40,41}\text{Ar}$, ^{40}K and ^{38}Cl presented
 355 in Figs. 13–15 demonstrates the power of the “recoil tagging” of heavy ions
 356 on an event-by-event basis.

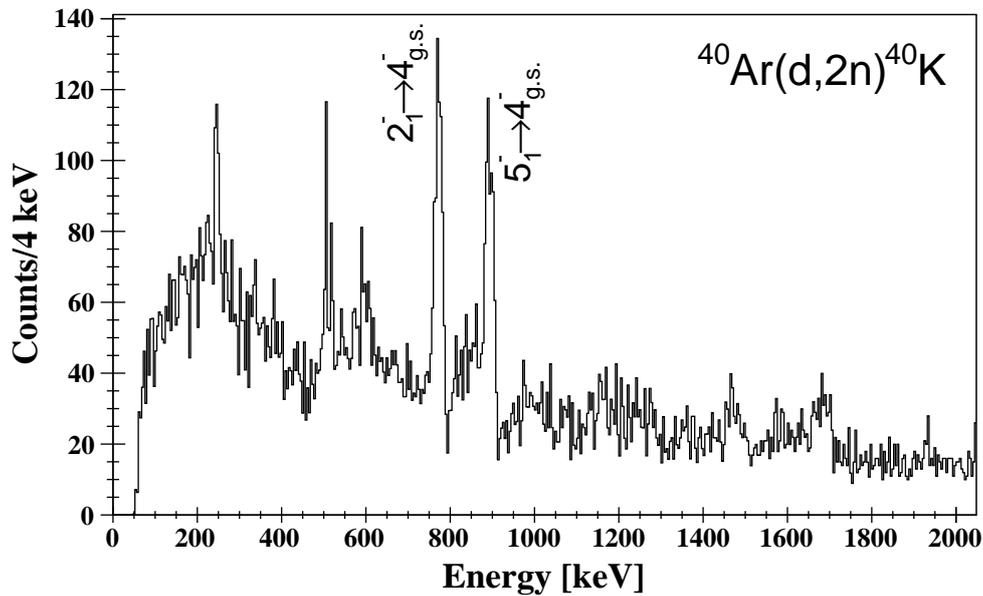


Figure 14: Doppler-corrected, background-subtracted γ -ray spectrum in coincidence with the detection of a K nucleus in TRIFIC. Known transitions in ^{40}K observed following the $^{40}\text{Ar}(d,2n)^{40}\text{K}$ reaction are labeled.

357 4. Conclusions

358 The TRIFIC gas ionization chamber was constructed and commissioned
 359 for RIB experiments at TRIUMF-ISAC. Custom-built fast electronics were
 360 developed to enable individual grid readout of electrode signals from TRIFIC
 361 at high rate. The TRIFIC detector was commissioned following two exper-

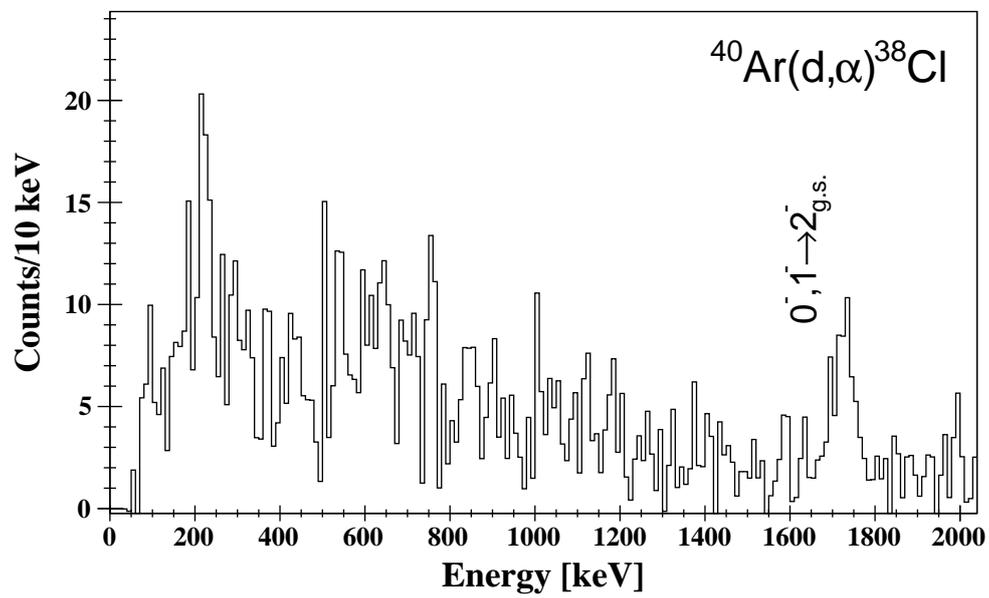


Figure 15: Doppler-corrected, background-subtracted γ -ray spectrum in coincidence with the detection of a Cl nucleus in TRIFIC. One known transition in ^{38}Cl observed following the the $^{40}\text{Ar}(d, \alpha)^{38}\text{Cl}$ reaction is labeled.

362 iments using $^{86}\text{Kr}/^{86}\text{Sr}$ and ^{40}Ar beams at intensities up to 500 kpps with
363 a GRIF-16-based digital DAQ system. A resolving power at 3 FWHM of
364 $Z/\Delta Z \approx 14$ and a separability at 1 FWHM of $Z/\Delta Z \approx 42$ at $Z \approx 40$ has
365 been demonstrated. Gamma-ray spectra recorded by TIGRESS in coinci-
366 dence with TRIFIC demonstrated the viability of event-by-event identifica-
367 tion of beam-like heavy ions. TRIFIC has been successfully commissioned
368 in “beam monitor” mode for beam intensities up to 50 Mpps when using the
369 two $\times 0.1$ attenuator foils. Alternative grid designs which enable scattering
370 angle sensitivity have been designed and will be tested.

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