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PII: S1743-9671(21)00157-4

DOI: https://doi.org/10.1016/j.joei.2021.09.002

Reference: JOEI 957

To appear in: Journal of the Energy Institute

Received Date: 12 July 2021

Revised Date: 29 August 2021

Accepted Date: 2 September 2021

Please cite this article as: Y. Ma, Y. Tian, Y. Zeng, X. Tu, Plasma synthesis of ammonia in a tangled wire dielectric barrier discharge reactor: Effect of electrode materials, *Journal of the Energy Institute* (2021), doi: https://doi.org/10.1016/j.joei.2021.09.002.

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# Plasma synthesis of ammonia in a tangled wire dielectric barrier discharge reactor: Effect of electrode materials

Yichen Ma, Yuxing Tian, Yuxuan Zeng, Xin Tu\*

Department of Electrical Engineering and Electronics, University of Liverpool, Liverpool, L69 3GJ, UK

# \*Corresponding Author

Prof. Xin Tu

Department of Electrical Engineering and Electronics,

University of Liverpool,

Liverpool, L69 3GJ,

UK

E-mail: xin.tu@liverpool.ac.uk

# Abstract

Plasma synthesis of NH<sub>3</sub> from N<sub>2</sub> and renewable H<sub>2</sub> under mild conditions is very attractive for decentralised sustainable green ammonia production using intermittent renewables. In this study, NH<sub>3</sub> synthesis was performed under ambient conditions in a dielectric barrier discharge (DBD) plasma reactor. Different tangled wire internal electrodes were employed to understand the influence of electrode materials on plasma ammonia synthesis. Compared with a rod electrode, a tangled wire electrode substantially enhanced the NH<sub>3</sub> concentration and reduced the energy cost for ammonia production, which can be attributed to the expanded surface area and the chemisorption properties of the tangled electrodes. The influence of the N<sub>2</sub>/H<sub>2</sub> molar ratio and total flow rate on the reaction performance was also evaluated. The lowest energy cost (59.0 MJ mol<sub>NH3</sub><sup>-1</sup>) for ammonia production was achieved using a Cu tangled electrode at a total flow rate of 250 ml min<sup>-1</sup> and a discharge power of 20 W. The electrical diagnostics of the plasma process showed that the tangled wire electrodes decreased the breakdown voltage of the DBD and enhanced charge deposition, which enhanced the  $NH_3$  production. The reaction mechanism was discussed for the process optimisation of ammonia synthesis in a tangled wire DBD system.

**Keywords:** Ammonia synthesis; Dielectric barrier discharge; Non-thermal plasma; Electrode materials; Nitrogen fixation

# 1. Introduction

Recent years have witnessed a rising demand for ammonia due to its vital role in the chemical and agricultural sectors. The estimated global production of ammonia is over 160 million tonnes each year, and approximately 80% of the ammonia is consumed in fertiliser production [1]. The advent of synthetic nitrogen fertiliser has led to fundamental changes in food production and now feeds nearly half of the world's population [2]. Nowadays, ammonia is being considered as a carbon-free energy storage vector for the long-distance transport of hydrogen due to its large hydrogen mass density and the mild temperature required for liquefaction [3]. It is also promising for short-term electrochemical energy storage (i.e. batteries) to deliver on-demand energy in conjunction with fuel cells, which would enable better uptake of the irregular supply from sustainable electricity [4]. Nevertheless, conventional ammonia synthesis via the Haber-Bosch (H-B) process takes up 1-2% of the global energy consumption and releases more than 300 tonnes of CO<sub>2</sub> on an annual basis [5, 6]. Success in developing green, efficient, and commercially viable alternatives to the H-B process that accommodate renewable energy and CO<sub>2</sub>-free hydrogen will reinforce the importance of ammonia in traditional fertiliser production and pioneering energy storage.

Although the ammonia synthesis from  $N_2$  and  $H_2$  is exothermic (R1), elevated temperatures (~700 K) are needed for the dissociation of the robust dinitrogen triple bond, which is the rate-limiting step in the H-B process [7]. In the context of high temperatures, high pressures around 100 bar are required to shift the equilibrium towards the formation of ammonia. The harsh conditions of the H-B process require large-scale centralised plants and continuous operation with an uninterrupted power supply. Thus, activating the inert dinitrogen at lower temperatures and lower pressures would be significant for addressing these challenges and improving the processes efficiency [8].

$$N_2 + 3H_2 \rightleftharpoons 2NH_3 \qquad \qquad \Delta H_{298K} = -46.27 \text{ kJ/mol} \qquad (R1)$$

Non-thermal plasma (NTP) has been considered as an ideal candidate for sustainable  $N_2$  fixation under mild conditions [9]. In an NTP, highly energetic electrons with a mean electron energy of 1-10 eV are initially generated, inducing a cascade of chemically reactive species (e.g., excited molecules, ions, and atoms) that facilitates the kinetically limited dinitrogen activation at low bulk gas temperatures [10-13]. This unique feature

enables the plasma-driven ammonia synthesis to be performed under thermodynamically favourable conditions at atmospheric pressure. Due to the mild working conditions, the NTP technology is compact, flexible, and easily switched on and off; this is desirable for the accommodation of intermittent and highly decentralised renewable energy sources such as solar, wind, and tidal energy for the decentralised small-scale green ammonia production [14, 15]. Moreover, the NTP process can readily integrate with water electrolysis using intermittent renewable electricity to achieve net-zero ammonia synthesis and alleviate the environmental impact [16].

In recent years, considerable efforts have been devoted to the plasma synthesis of ammonia using dielectric barrier discharges (DBDs) [17-23]. Bai et al. reported plasma synthesis of  $NH_3$  in a cylindrical DBD reactor at ambient conditions [20]. Wang et al. developed a unique water-cooled DBD reactor for the synthesis of ammonia at near room temperature and ambient pressure [21]. Aihara et al. employed a metallic wire electrode to synthesise ammonia in a DBD reactor, achieving an NH<sub>3</sub> yield of 3.5% and an energy cost of 18.6 MJ  $mol_{NH3}^{-1}$ . Their results proved that using a metal wire as the high-voltage inner electrode contributes to a more productive ammonia synthesis via the increased surface area [22]. Besides, Iwamoto et al. [23] and Mehta et al. [24] evaluated the activities of different metals via density functional theory (DFT) calculations and microkinetic modelling. The employment of proper metal electrodes in a DBD reactor can open a new route to tailor the formation of reactive species and facilitate ammonia production. However, reducing the energy cost and enhancing the ammonia yield remain challenges that require further innovation and improvement in plasma reactor design. Moreover, the individual effect of metallic electrodes such as electrode materials and electrode configurations on the electrical properties of the discharge is still underexplored in plasma NH<sub>3</sub> synthesis [25, 26]. Further efforts are required to develop a systematic understanding of these fundamental plasma properties in ammonia synthesis, this will reduce the energy consumption of NH<sub>3</sub> production under ambient conditions, shedding light on the reaction mechanism of the plasma ammonia synthesis, and generating essential and invaluable knowledge for the future development of this disruptive and emerging technology.

In this work, the ammonia synthesis from nitrogen and hydrogen was carried out using a DBD reactor with tangled metal electrodes. The influence of process parameters including the N<sub>2</sub>/H<sub>2</sub> molar ratio and total gas flow rate on the NH<sub>3</sub> concentration and energy cost were investigated. The chemical performances and discharge characteristics were also examined using different tangled electrode materials. A possible reaction mechanism was discussed based on the comprehensive analysis of experimental findings with a view to achieving process optimisation of ammonia synthesis in a tangled wire DBD reactor.

# 2. Experimental

#### 2.1 Experimental setup

In this work, a coaxial DBD reactor was used to investigate the plasma-synthesis of ammonia under ambient conditions. Figure 1(a) shows a schematic diagram of the experimental setup. N2 and H2 were controlled by mass flow controllers (Omega, FMA-2404) before being introduced into the DBD reactor. The configuration of the tangled wire DBD reactor is depicted in Figure 1(b). A quartz tube with an outer diameter of 22 mm and a wall thickness of 1.5 mm was used as the dielectric layer. A stainless-steel mesh wrapped around the quartz tube served as a ground electrode, while a metal rod or a loose metal-wool was placed in the middle of the quartz tube and acted as the high voltage electrode. Several metals were used as the tangled wire electrodes, including NiFe alloy, stainless steel (SS), Ti, and Cu. These wires were comprised of fibres with the same diameter (0.2 mm) and total length (10 m), thus providing the same surface area (63 cm<sup>2</sup>). The discharge length was 80 mm with an average effective discharge gap of 8 mm. A hollow stainless-steel rod electrode with an outer diameter of 14 mm was used for comparison, as shown in Figure 1(c). The DBD reactor was connected to a high voltage AC power supply with a maximum peak voltage of 30 kV and a frequency of 5-20 kHz. The voltage on an external capacitor ( $C_{ext} = 0.47 \ \mu\text{F}$ ) connected to the ground electrode was measured to determine the total charge  $(Q_{ext})$  transferred in the plasma, while the applied voltage was recorded by a high voltage probe (Testec, TT-HVP 15 HF) and the current was measured by a current monitor (Magnelab, CT-E0.5). All signals were sampled by a 4-channel digital oscilloscope (Tektronix, DPO2024B). A homemade power measurement system was used to monitor and control the discharge power in realtime via the area calculation of the Q-U Lissajous figure. In this work, the discharge power was fixed at 20 W.



Figure 1. (a) Schematic diagram of the experimental setup; (b) configuration of the tangled wire DBD reactor; (c) configuration of the rod electrode DBD reactor.

# 2.2 Product analysis

A gas mixture with a variable  $N_2/H_2$  molar ratio was used as the reactants and the total feed flow rate was controlled between 50 and 250 ml min<sup>-1</sup> during the experiment. The reaction products were analysed by a Fourier transform infrared (FTIR) spectrometer (Jasco, FTIR-4200) with a resolution of 2 cm<sup>-1</sup>. It contained a gas cell with an optical pathlength of 10 cm (Specac, Storm 10 gas cell). The concentration of ammonia in the product gas was calculated using a series of calibration gas mixtures. The gas products were sampled every five minutes to monitor the time-resolved performances of this DBD system, while the NH<sub>3</sub> concentration was recorded after 120 min running time for each test. Each measurement was repeated three times, and the margin of error in this work was within 3%.

In the ammonia synthesis process, the conversion of  $N_2$  and  $H_2$  is defined as:

$$X_{N_2} = \frac{\text{moles of } N_2 \text{ converted}}{\text{moles of } N_2 \text{ input}} \times 100$$
(1)

$$X_{\rm H_2} = \frac{\text{moles of H}_2 \text{ converted}}{\text{moles of H}_2 \text{ input}} \times 100$$
(2)

The energy cost (EC) of ammonia synthesis is defined as:

$$EC \text{ (MJ mol}_{\text{NH}_3}^{-1}) = \frac{\text{discharge power (W)}}{\text{moles of NH}_3 \text{ per second (mol/s)}} \times \frac{1}{10^6 \left[\frac{\text{J}}{\text{MJ}}\right]}$$
(3)

# 2.3 Evaluation of electrical parameters

Figure 2(a) illustrates the classic equivalent circuit of a DBD reactor, in which  $C_{diel}$  and  $C_{gap}$  correspond to the capacitance of the dielectric layer and the capacitance of the discharge gap, respectively. In the presence of a packing material,  $C_{gap}$  includes the contribution of the gas-solid integration in between the electrodes. Conductive filaments are formed when the gas breakdown happens, thus the switch 'K' in the parallel resistive channel is on.



Figure 2. (a) The equivalent electrical circuit of a DBD reactor and (b) a typical Q-U Lissajous plot of the DBD.

The shape of a Q-U Lissajous figure typically approximates a parallelogram where the internal electrical discharge characteristics can be derived from its dimensions, including the breakdown voltage, reactor charge, and reactor capacitance [27]. Figure 2(b) demonstrates a typical Q-U Lissajous figure from which the charges transferred per halfcycle ( $Q_{trans}$ ) can be obtained. The lines AB and CD in a Lissajous figure stand for the plasma-off period. The slope dQ/dU of these lines equals  $C_{cell}$  in this period, which comprises the gap capacitance  $C_{gap}$  and the dielectric capacitance  $C_{diel}$ :

$$\frac{1}{C_{\text{cell}}} = \frac{1}{C_{\text{diel}}} + \frac{1}{C_{\text{gap}}} \tag{4}$$

Therefore, the gap capacitance  $C_{gap}$  can be expressed as follows:

$$C_{\rm gap} = \frac{C_{\rm diel} \times C_{\rm cell}}{C_{\rm diel} - C_{\rm cell}}$$
(5)

The lines BC and DA in the Lissajous plot correspond to the plasma-on phase. The slope of these lines corresponds to the effective capacitance  $C_{\text{eff}}$  which equals the dielectric capacitance  $C_{\text{diel}}$  in a fully bridged gap [28].

The total charge in the plasma Q can be calculated from the voltage  $U_c$  on an external capacitor  $C_{\text{ext}}$  (0.47 µF), and the voltage on the dielectric material  $U_d$  can be calculated using charge Q and  $C_{\text{diel}}$ :

$$Q = C_{\rm ext} \times U_{\rm c} \tag{6}$$

$$U_{\rm d} = \frac{Q}{C_{\rm diel}} \tag{7}$$

Accordingly, the gas voltage  $U_g$  across the discharge gap is obtained from the applied voltage  $U_a$  and dielectric voltage  $U_d$ :

$$U_{\rm g} = U_{\rm a} - U_{\rm d} \tag{8}$$

The breakdown voltage  $U_b$  can be calculated using  $U_{min}$  from the Lissajous figure as follows [29, 30]:

$$U_{\rm b} = \frac{1}{1 + C_{\rm gas} / C_{\rm diel}} \times U_{\rm min} \tag{9}$$

# 3. Results and discussion

#### 3.1 Effect of electrode materials on the plasma-driven NH<sub>3</sub> synthesis

Figure 3 shows the influence of different electrode materials on ammonia synthesis in terms of NH<sub>3</sub> concentration and energy cost for ammonia production. Compared with the rod electrode, the NH<sub>3</sub> production was more efficient using the tangled wire electrodes, this can be attributed to the larger surface area (63 cm<sup>2</sup>) of the tangled wire electrode compared to the rod electrode (45 cm<sup>2</sup>). Besides, it was reported that the surface of the tangled wire electrode became bumpy after the plasma treatment, which further expands the surface area and facilitates the synthesis of ammonia [22]. Among the tangled electrodes, copper had the most optimal synthesis performance with an N<sub>2</sub> conversion of 0.31%, an NH<sub>3</sub> concentration of 2983 ppm, and an energy cost of 90.2 MJ  $mol_{NH_3}^{-1}$ . The performance of the tangled wire electrodes for the NH<sub>3</sub> synthesis followed the order of Cu > Ti > SS > NiFe, suggesting the plasma-driven ammonia production is affected by the material of the electrodes. Interestingly, in a study of  $NH_3$  decomposition using supported metal catalysts, the activity of the catalysts followed the order of Co > Ni > Fe > Cu, which is the reverse of our NH<sub>3</sub> synthesis study [31]. This finding implies that the favourable performance of copper in this work may be associated with the reduced reverse reaction - decomposition of formed NH<sub>3</sub> on the electrode surface.



Figure 3. Effect of different electrode materials on NH<sub>3</sub> production and the energy cost.  $(N_2/H_2 = 1:1, \text{ total flow rate 100 ml min}^{-1}, \text{ discharge power 20 W})$ 

Table 1. The N<sub>2</sub> and H<sub>2</sub> conversion in the NH<sub>3</sub> synthesis process. (N<sub>2</sub>/H<sub>2</sub> = 1:1, total flow rate 100 ml min<sup>-1</sup> and discharge power 20 W)

Electrode	Conversion (%)				
materials	N <sub>2</sub>	$H_2$			
SS Rod	0.19	0.57			
NiFe	0.27	0.80			
SS	0.27	0.82			
Ti	0.30	0.89			
Cu	0.31	0.93			

#### 3.2 Effect of process parameters on the plasma synthesis of ammonia

Figure 4 shows the effect of the  $N_2/H_2$  molar ratio on the plasma NH<sub>3</sub> synthesis. The NH<sub>3</sub> concentration increased with the elevated N<sub>2</sub> content and reached a maximum at an N<sub>2</sub>/H<sub>2</sub> ratio of 1:1, then dropped when further increasing the N<sub>2</sub>/H<sub>2</sub> ratio to 3:1. The influence of the N<sub>2</sub>/H<sub>2</sub> ratio on the energy cost of NH<sub>3</sub> production showed the reverse trend. As shown in Figure 4, The highest ammonia concentration and the lowest energy cost were achieved at the optimum N<sub>2</sub>/H<sub>2</sub> ratio of 1:1. This result is consistent with the findings in previous studies that non-stoichiometric ratios of N<sub>2</sub>/H<sub>2</sub> lead to higher ammonia yields than the stoichiometric ratio (1:3) [32-37]. Peng and co-workers reported that the minimum energy cost of plasma-synthesis of NH<sub>3</sub> was achieved at an N<sub>2</sub>/H<sub>2</sub> ratio of 1:1 regardless of the applied voltage, and further increasing N<sub>2</sub> content increased the

energy cost [32]. Gomez et al. achieved the lowest energy cost of ammonia production at an N<sub>2</sub>/H<sub>2</sub> molar ratio in the range of 1:3 to 1:1 [33]. This phenomenon can be explained by a trade-off between the reaction kinetics of NH<sub>3</sub> synthesis and the discharge properties. Compared with the stoichiometric N<sub>2</sub>/H<sub>2</sub> ratio (1:3), higher N<sub>2</sub> concentrations can contribute to a higher fraction of plasma energy deposited in N<sub>2</sub> molecules, facilitating the rate-limiting step of dinitrogen dissociation. However, excessive N<sub>2</sub> content may decrease the mean electron energy in DBD plasmas and suppress the plasma dissociation of N<sub>2</sub> [34].



Figure 4. Effect of the  $N_2/H_2$  molar ratio on  $NH_3$  production and the energy cost. (Cu tangled electrode, total flow rate 100 ml min<sup>-1</sup>, discharge power 20 W)

Figure 5 shows the effect of the total feed flow rate on the NH<sub>3</sub> production and energy cost using the tangled Cu electrode at a constant  $N_2/H_2$  molar ratio of 1:1 and a discharge power of 20 W. The NH<sub>3</sub> concentration declined with the rising total flow rate, which can be ascribed to the decreased residence time in the discharge area reducing the number of collisions of the reactant molecules with energetic electrons and chemically reactive species [32, 38]. Nevertheless, the higher flow rate increases the total number of reactants passing through the plasma zone and enhances the number of converted molecules at a constant discharge power. As a result, the energy cost of ammonia production decreased from 139.3 to 59.0 MJ mol<sub>NH3</sub><sup>-1</sup> when increasing the total flow rate from 50 to 250 ml min<sup>-1</sup>.



Figure 5. Effect of total flow rate on  $NH_3$  production and energy cost. (Cu tangled electrode,  $N_2/H_2$  molar ratio 1:1, discharge power 20 W)

#### 3.3 Effect on electrical properties when using different electrode materials

Figure 6 shows the time-resolved electrical signals of DBD plasma in the NH<sub>3</sub> synthesis process. The current signals are similar when using different tangled electrode materials, suggesting the discharge model is not changed by varying the electrode. The strong current pulses corresponded to the filamentary discharges bridging the gas gap. As the tangled wire loosely filled the whole discharge gap and was in contact with the inner surface of the quartz tube, the presence of numerous weak current pulses can be attributed to the formation of the local filamentary discharges in between the dielectric layer and the metal wire. The DBD with the tangled Cu electrode showed the highest amplitude of the current pulses. As a result, the chance for collisions between electrons and reactants and the average electron density were enhanced due to the higher discharge current and charge transfer (Table 2). This enhancement in current and charge transfer would increase the chance of collisions between electrons and reactants as well as the average electron density, both of which contribute to the enhanced dissociation of nitrogen molecules, the rate-limiting step in the plasma synthesis of ammonia. The gas voltage became quasi-flat over time after the ignition of the plasma, suggesting that the formation of filamentary discharges is not affected by the applied voltage after the electrical gas breakdown [30]. The gas voltage was in the sequence of SS rod > NiFe > SS > Ti > Cu, consistent with the concentration of synthesised ammonia (Figure 3). This finding can be associated with the production of NH<sub>3</sub> in the plasma reactor: as the dielectric strength of NH<sub>3</sub> is lower than that of  $N_2$  and  $H_2$ , the presence of the produced  $NH_3$  in the DBD reactor changes the dielectric properties of the working gas and thus reduces the breakdown voltage of the DBD.



Figure 6. Typical electrical signals of the DBD using different electrodes. ( $N_2/H_2 = 1:1$ , total flow rate 100 ml min<sup>-1</sup>, frequency 9 kHz, discharge power 20 W)

The typical Lissajous plots obtained during the  $NH_3$  synthesis using different inner electrodes are illustrated in Figure 7. The Lissajous figure of the DBD using the SS rod electrode was a strict parallelogram shape, while the Lissajous figure of the discharge morphed to an oval shape when using the tangled electrodes. This also indicates a change in the discharge characteristics. Table 2 summarises the influence of the different electrodes on the peak-to-peak applied voltage ( $U_{pp}$ ) and charge transferred across the

gap during the discharge ( $Q_{trans}$ ). The use of tangled wire electrodes has a clear effect on the charge characteristics of the DBD plasma. Compared with other electrode materials, the DBD with the Cu wire showed the lowest applied voltage, as well as an enhanced amplitude of the current pulses (Figure 6) and the charge transfer of the discharge.



Figure 7. Lissajous figure obtained during the plasma synthesis of NH<sub>3</sub>. (N<sub>2</sub>/H<sub>2</sub> = 1:1, total flow rate 100 ml min<sup>-1</sup>, frequency 9 kHz, discharge power 20 W)

Table 2. Electrical properties of the DBD reactor using different electrodes. ( $N_2/H_2 = 1:1$ , total flow rate 100 ml min<sup>-1</sup>, discharge power 20 W)

Electrode	$Q_{ m trans}$	$U_{ m pp}$
material	(µC)	(kV)
Rod	0.82	13.8
NiFe	0.87	13.3
SS	0.89	13.0
Ti	0.92	12.8
Cu	0.95	12.5

# 4. Discussion

In the Haber-Bosch process, initially the dissociative adsorption of N<sub>2</sub> and H<sub>2</sub> takes place on the catalyst surface, followed by the step-wise hydrogenation of adsorbed N atoms to form NH<sub>3</sub> (R2-R6, \* denotes the adsorption site on the catalyst surface) [39]. N<sub>2</sub> + \*  $\rightarrow$  2N(s) (R2) H<sub>2</sub> + \*  $\rightarrow$  2H(s) (R3)

$N(s) + H(s) \rightarrow NH(s)$	(R4)

$$NH(s) + H(s) \rightarrow NH_2(s)$$
 (R5)

$$NH_2(s) + H(s) \rightarrow NH_3(s)$$
 (R6)

In contrast, NTP enables the activation and dissociation of reactants in the gas phase, thus creating new reaction routes for ammonia production. It is well accepted that NTP improves the activity of ammonia synthesis via overcoming the prohibitively high energy barrier for the dissociation of the robust dinitrogen triple bond, generally through four basic channels: direct dissociation, ionisation, electronic excitation, and vibrational excitation [40]. It was reported that the reactions involving radicals and vibrationally-excited molecules are significant in the formation of NH<sub>3</sub> in plasma, while the ions are considered less important [24, 34]. Moreover, the vibrational excitations can facilitate the N<sub>2</sub> dissociation in both gas-phase and surface reactions [19]. The presence of plasma-generated excited intermediates was confirmed using OES diagnostics [41].

The reaction pathways for ammonia synthesis involving surface reactions can be divided into Eley-Rideal (E-R) and Langmuir-Hinshelwood (L-H) reactions [42]. For the E-R mechanism, the H atoms and NH<sub>x</sub> intermediates are formed in gas-phase reactions and the ammonia synthesis takes place on the metal surface. More specifically, the NH species generated in the gas phase react with the surface adsorbed H thereby forming ammonia [32, 34]. In the L-H mechanism, the reactive species (e.g., surface-adsorbed N and H atoms) are primarily formed via dissociative adsorption of molecules [43]. Previous experimental and simulation studies proposed the significance of excited molecular N<sub>2</sub> species [23, 24]. Instead of direct dissociation in the gas phase, the N<sub>2</sub> excited states undergo dissociative adsorption to form surface-adsorbed atomic N species. Thereafter, mutual reactions between species adsorbed on the catalyst surface are responsible for ammonia production. In this study, both pathways may take place and contribute to ammonia production.

Iwamoto et al. performed DFT calculations to understand the formation energy ( $\Delta E_f$ ) of metal nitride and the adsorption energy of an N atom on different metal surfaces in a metal-wire DBD reactor [23]. Their studies showed that Cu surfaces are more favourable for adsorption of N atoms compared to Ni, Ti, and Fe surfaces. Shah et al. found the

presence of the intermediate GaN on the surface of a Ga-In alloy catalyst in the plasmacatalytic synthesis of ammonia [44]. Their finding suggests that the formation of the metal nitride on the metal electrode surface also contributes to the ammonia synthesis in a DBD reactor. The high surface area of the metal wire electrodes enables the surface metal sites to derive N atoms from  $N_2$  excited states followed by the subsequent step-wise hydrogenation of N with H to form NH<sub>3</sub>.

Table 3 compares the performance of ammonia synthesis using different types of plasma. Note that the energy cost achieved in this work (59.0 MJ  $mol_{NH3}^{-1}$ ) is strongly competitive compared with other plasma processes. Previous studies also utilised radiofrequency (RF) plasmas and microwave (MW) discharges in NH<sub>3</sub> production; these processes usually achieve high N<sub>2</sub> conversion but consume excessive energy due to high power input [44-46]. Further enhancement of the reaction activity could be achieved by adding suitable catalysts into the plasma, a hybrid plasma-catalytic system has significant potential to take advantage of the low-temperature synergistic effect in ammonia synthesis. Mehta et al. focused on supported metal catalysts and plotted volcano curves of their activity for ammonia synthesis [24]. Compared to conventional heterogeneous catalysis, the optimal catalysts for plasma catalysis are metal sites that weakly bind with nitrogen. Moreover, using different packed-bed materials in a DBD reactor can also affect the formation of a range of reactive species and influence the chemical reactions [33]. For instance, Gómez-Ramírez et al. reported an N<sub>2</sub> conversion of >7% using ceramic-lead zirconate titanate (PZT) pellets in a DBD reactor. Their work showed that the presence of ferroelectric materials enhanced the ammonia production through the influenced discharge properties and the catalytic reactions on the surface of ferroelectric pellets [41]. As innovative plasma reactor design and rational design of catalysts have been considered as feasible strategies to reduce the energy cost of plasma processes, the integration of both strategies could be a promising route for future development.

Table 3. Comparison of key parameters in our study with other plasma processes used for ammonia synthesis.

Plasma	Catalyst	Flow rate (ml min <sup>-1</sup> )	N <sub>2</sub> /H <sub>2</sub> ratio	Power (W)	X <sub>N2</sub> (%)	EC (MJ mol <sub>NH3</sub> -1)	Ref.
MW	-	15000	9:1	1100	0.75	<mark>1532.8</mark>	[45]

RF	Ga-In molten alloy	20	1:4	300	-	<mark>197.8</mark>	[44]
RF	Au wire	20	1:4	300	-	<mark>322.7</mark>	[46]
RF	Ni-MOF-74	20	1:4	50	-	<mark>266.6</mark>	[47]
DBD	$Ru/Al_2O_3$	500	3:2	12	-	<mark>95.8</mark>	[48]
DBD	Ni/SiO <sub>2</sub>	25	1:3	107	6.4	<mark>81.7</mark>	[49]
DBD	Ni/Al <sub>2</sub> O <sub>3</sub>	100	1:2	10	-	<mark>68.9</mark>	[24]
Water- electrode DBD	Ni/Al <sub>2</sub> O <sub>3</sub>	56	1:2	20	0.09	211.4	[21]
DBD	Ru/alumina membrane	40	1:3	127	4.7	<mark>165.7</mark>	[50]
DBD	Ru/alumina membrane	30	1:3	127	4.8	<mark>153.3</mark>	[37]
DBD	Carbon coatings on Al <sub>2</sub> O <sub>3</sub>	60	1:3	98	2.3	<mark>383.2</mark>	[19]
DBD	PZT	11.5	1:3	-	7.2	<mark>278.7</mark>	[41]
DBD	PZT	11.5	1:3	5 -	2.7	<mark>175.2</mark>	[33]
DBD	-	250	1:1	20	0.31	<mark>59.0</mark>	this work

## **5.** Conclusions

The NH<sub>3</sub> synthesis was carried out in a DBD plasma reactor under ambient conditions. A tangled wire electrode was used to improve NH<sub>3</sub> production and decrease energy costs. Compared with the rod electrode, the tangled wire electrode substantially enhanced the conversion of N<sub>2</sub> and H<sub>2</sub>, increased the NH<sub>3</sub> concentration, and reduced the energy cost of the synthesis process. The material of the electrode significantly influenced the NH<sub>3</sub> production. Among the tested materials, including NiFe, SS, Ti, and Cu, the Cu electrode achieved the highest concentration of NH<sub>3</sub> (2983 ppm) and the lowest energy cost (90.2 MJ mol<sub>NH3</sub><sup>-1</sup>) at an N<sub>2</sub>/H<sub>2</sub> molar ratio of 1:1 and a flow rate of 100 ml min<sup>-1</sup>. This finding can be attributed to the chemisorption properties of the tangled electrode. By changing the total flow rate and the N<sub>2</sub>/H<sub>2</sub> molar ratio in the feed gas, the production of NH<sub>3</sub> can be further optimised. The energy cost for the NH<sub>3</sub> synthesis dropped to 59.0 MJ mol<sub>NH3</sub><sup>-1</sup> when using the Cu electrode at a flow rate of 250 ml min<sup>-1</sup>. In addition, the effect of electrode material on the electrical properties of the reactor was discussed. Compared to the DBD using the rod electrode, the use of tangled wire electrodes decreased the breakdown voltage and enhanced charge deposition, both of which contributed to the

enhanced NH<sub>3</sub> production. The possible reaction pathways for the plasma NH<sub>3</sub> synthesis were discussed with a view to providing knowledge for the future development of this attractive and emerging technology.

# Acknowledgement

The support of this work by the UK EPSRC Impact Acceleration Account (IAA) is gratefully acknowledged. Y. Ma also acknowledges the PhD fellowship co-funded by the University of Liverpool and the Chinese Scholarship Council (CSC).

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Journal Pre-proof

# Highlights

- o Plasma synthesis of ammonia was carried out using a DBD plasma reactor.
- Using a tangled wire electrode enhanced the production of ammonia.
- The optimal energy efficiency for ammonia production was achieved using a Cu tangled electrode.

Journal Pre-proof

### **Declaration of interests**

 $\boxtimes$  The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

□The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: