

An efficient algorithm for computing smoothness indicators for WENO schemes

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Abstract

1 WENO schemes are a popular class of shock-capturing schemes which adopt an
2 adaptive-stencil approach to interpolation. WENO schemes rely on smoothness
3 indicators to assess the relative smoothness of the solution within the sub-stencils.
4 Computing these smoothness indicators is the most expensive operation in the
5 WENO reconstruction procedure. In this paper, an efficient algorithm is proposed to
6 compute these quantities without sacrificing the positivity property of the
7 smoothness indicators. The proposed algorithm involves linear combinations of the
8 undivided differences which can be computed efficiently in a recursive manner.
9 This allows the computation of the smoothness indicators to be performed using
10 significantly fewer floating-point operations compared to conventional
11 implementations. Moreover, the proposed algorithm is simple to implement and
12 involves fewer constants.

13 **1 Introduction**

14 Hyperbolic conservation laws admit discontinuous solutions. Solving such problems numerically
15 requires nonlinear reconstruction schemes, known as shock-capturing schemes, which introduce
16 numerical dissipation to prevent the formation of spurious oscillations near sharp gradients. Weighted
17 essentially non-oscillatory (WENO) schemes are one such class of high order shock-capturing
18 schemes. Introduced by Liu, *et al.* [1], WENO schemes adopt an adaptive-stencil approach (as
19 opposed to the fixed-stencil approach of linear schemes) by combining the reconstructions from
20 several sub-stencils (subsets of a stencil) using weights which are determined based on the relative
21 smoothness of the solution within each sub-stencil. This allows WENO schemes to eliminate
22 contributions from sub-stencils containing discontinuities and, at the same time, to achieve the
23 optimal order of accuracy on the stencil when the solution is smooth in all the sub-stencils.

24 Key to achieving the optimal order of accuracy is the design of the sub-stencil smoothness indicator.
25 The smoothness indicator proposed by Liu, *et al.* [1], though simple to compute, does not satisfy the
26 requirement for optimal accuracy. Jiang and Shu [2] proposed a different smoothness indicator based
27 on the cell average of the squares of derivatives which satisfy the requirement for optimal accuracy in
28 regions away from critical points [3]. The Jiang-Shu smoothness indicators have since become the
29 most popular choice of smoothness indicators. However, they are more expensive to compute
30 compared to the Liu-Osher-Chan smoothness indicators, especially for high order WENO schemes.
31 Since computing these quantities is the most demanding step in the WENO reconstruction procedure,
32 overall computational efficiency could be vastly improved by speeding up this step. While much
33 effort has been devoted to devise new smoothness indicators for better accuracy (e.g., [4-7]), the
34 computational efficiency of such indicators has not received the nearly same attention. Notable
35 exceptions include the works of Teng, *et al.* [8] and Baeza, *et al.* [9]. Teng, *et al.* [8] avoided WENO
36 reconstructions altogether where the solution is deemed nearly uniform based on first order undivided
37 differences. Baeza, *et al.* [9] introduced a set of efficient smoothness indicators for a $(2r - 1)$ th order
38 WENO scheme using squared undivided differences of only the first and $(2r - 2)$ th orders.

39 Instead of introducing new smoothness indicators, this paper proposes a more efficient algorithm for
 40 computing the Jiang-Shu smoothness indicators, the most common choice in the community. The
 41 algorithm mimics the form of the Liu-Osher-Chan smoothness indicators in that it uses squared
 42 undivided differences up to $(r - 1)$ th order. The proposed algorithm is simpler-to-implement and
 43 requires fewer floating-point operations compared to conventional implementations. The paper is
 44 organized as follows: First, a review of the WENO reconstruction procedure is described along with a
 45 discussion on two common implementations of computing the Jiang-Shu smoothness indicators.
 46 Finally, the fast algorithm is derived and a comparison of the computational efficiency of the
 47 proposed algorithm is provided by counting the number of floating-point operations.

48

49 **2 Methodology**

50 **2.1 Review of WENO scheme**

51 In the finite volume approach, the computational domain is discretized into non-overlapping control
 52 volumes (cells) and the solution is obtained in terms of cell averages. On a uniform grid, the i th cell
 53 average \bar{u}_i of a scalar function $u(x)$ is defined as,

$$\bar{u}_i = \frac{1}{\Delta x} \int_{x_{i-1/2}}^{x_{i+1/2}} u(x) dx, \quad i = 0, \dots, N - 1 \quad (1)$$

54 where Δx denotes the cell width, x_i the cell centres and $x_{i\pm 1/2} = x_i \pm \Delta x/2$ the cell interface
 55 locations. Without loss of generality, let us consider the left-biased reconstruction of the cell averages
 56 at the cell interface $x_{i+1/2}$. The right-biased reconstruction can be derived by symmetry. For a
 57 $(2r - 1)$ th order WENO scheme, the left-biased reconstruction $u_{i+1/2}^L$ is computed on the stencil
 58 $\mathcal{S}_{i+1/2}^L = \{i - r + 1, \dots, i + r - 1\}$. $\mathcal{S}_{i+1/2}^L$ is split into r overlapping sub-stencils $\mathcal{S}_{j,i+1/2}^L =$
 59 $\{i - r + 1 + j, \dots, i + j\}$ each consisting of r cells. The sub-stencil index j runs from 0 to $r - 1$.

60 Each sub-stencil $\mathcal{S}_{j,i+1/2}^L$ yields an r th order approximation $u_{j,i+1/2}^L$ which can be computed as,

$$u_{j,i+1/2}^L = \sum_{k=0}^{r-1} M_{jk}^{(r)} \bar{u}_{i-r+1+j+k} \quad (2)$$

61 using a reconstruction matrix $M^{(r)}$. The WENO reconstruction $u_{i+1/2}^L$ is computed as a convex
 62 combination of $u_{j,i+1/2}^L$ given below.

$$u_{i+1/2}^L = \sum_{j=0}^{r-1} \omega_j u_{j,i+1/2}^L \quad (3)$$

63 The nonlinear sub-stencil weights ω_j in Eq. (3) are computed using the ideal weights $d_j^{(r)}$ smoothness
 64 indicators $IS_j^{(r)}$ are as follows.

$$\omega_j = \frac{d_j^{(r)} / (IS_j^{(r)} + \epsilon)^2}{\sum_{j=0}^{r-1} d_j^{(r)} / (IS_j^{(r)} + \epsilon)^2} \quad (4)$$

65 The smoothness indicator proposed by Jiang and Shu [2] is given below.

$$IS_j^{(r)} = \frac{1}{\Delta x} \int_{x_{i-1/2}}^{x_{i+1/2}} \sum_{l=1}^{r-1} \left(\frac{d^l \mathcal{U}_{j,i+1/2}^L(x)}{dx^l} \Delta x^l \right)^2 dx \quad (5)$$

66 $\mathcal{U}_{j,i+1/2}^L(x)$ in the above definition refers to the r th order polynomial reconstructed on sub-stencil
 67 $s_{j,i+1/2}^L$. Computation of $IS_j^{(r)}$ is usually implemented using the cell averages belonging to sub-stencil
 68 j in the following form,

$$IS_j^{(r)} = \sum_{m=1}^{r-1} Q_m \left(\sum_{k=0}^{r-1} P_{j,mk}^{(r)} \bar{u}_{i-r+1+j+k} \right)^2 \quad (6)$$

69 where Q_m and $P_{j,mk}^{(r)}$ are constants. This is referred to as the compact implementation because when
 70 the polynomial $\mathcal{U}_{j,i+1/2}^L(x)$ in Eq. (5) is expressed in the basis of Hermite polynomials, the
 71 expressions for $IS_j^{(r)}$ reduce to a compact form in terms of the modal coefficients [10-12]. Since
 72 $IS_j^{(r)}$ is computed as a sum of squares, the compact implementation ensures its positivity, and this

73 property has been demonstrated to improve accuracy [13]. Despite its name, the compact
74 implementation is computationally expensive. As the order of the WENO scheme increases, the
75 number of sub-stencils increases and, the expressions for each $IS_j^{(r)}$ become longer and more
76 unwieldy. It should come as no surprise that computation of smoothness indicators is the most
77 demanding operation in the WENO reconstruction procedure. Therefore, it would be of tremendous
78 advantage to devise a faster algorithm to compute them without sacrificing their positivity.

79 2.2 Proposed algorithm for computing $IS_j^{(r)}$

80 To motivate the design of a more efficient algorithm, consider the compact form of $IS_0^{(4)}$.

$$\begin{aligned}
IS_0^{(4)} = & \left(\frac{1}{3}\bar{u}_{i-3} - \frac{3}{2}\bar{u}_{i-2} + 3\bar{u}_{i-1} - \frac{11}{6}\bar{u}_i \right)^2 + \frac{13}{3} \left(\frac{1}{2}\bar{u}_{i-3} - 2\bar{u}_{i-2} + \frac{5}{2}\bar{u}_{i-1} - \bar{u}_i \right)^2 \\
& + \frac{781}{20} \left(\frac{1}{6}\bar{u}_{i-3} - \frac{1}{2}\bar{u}_{i-2} + \frac{1}{2}\bar{u}_{i-1} - \frac{1}{6}\bar{u}_i \right)^2
\end{aligned} \tag{7}$$

81 Eq. (7) can be re-arranged into a slightly different form below.

$$\begin{aligned}
IS_0^{(4)} = & \left[-\frac{1}{3}(\bar{u}_{i-2} - \bar{u}_{i-3}) + \frac{7}{6}(\bar{u}_{i-1} - \bar{u}_{i-2}) - \frac{11}{6}(\bar{u}_i - \bar{u}_{i-1}) \right]^2 \\
& + \frac{13}{12} [(\bar{u}_{i-1} - 2\bar{u}_{i-2} + \bar{u}_{i-3}) - 2(\bar{u}_i - 2\bar{u}_{i-1} + \bar{u}_{i-2})]^2 \\
& + \frac{781}{720} [-(\bar{u}_i - 3\bar{u}_{i-1} + 3\bar{u}_{i-2} - \bar{u}_{i-3})]^2
\end{aligned} \tag{8}$$

82 Observe that the terms inside the first, second and third pair of square brackets are linear
83 combinations of the first, second and third order undivided differences, respectively, computed on the
84 four cells which belong to sub-stencil $j = 0$. Indeed, it is possible to cast $IS_j^{(r)}$ into the general form,

$$IS_j^{(r)} = \sum_{m=1}^{r-1} \frac{Q_m}{(m!)^2} \left[\sum_{k=0}^{r-1-m} A_{j,mk}^{(r)} \Delta^m [\bar{u}_{i-r+1+j+k}] \right]^2 \tag{9}$$

85 where $\Delta^0[\bar{u}_i] = \bar{u}_i$ and $\Delta^{m+1}[\bar{u}_i] = \Delta^m[\bar{u}_{i+1}] - \Delta^m[\bar{u}_i]$ denote the undivided differences. Q_m are
86 the same constants which appear in Eq. (6) for the compact implementation. Eqs. (6) and (9) result in
87 identical expressions when expanded in terms of the cell averages. The main advantage of using Eq.
88 (9) is that it is written in terms of the undivided differences which can be computed efficiently in a

89 recursive fashion, i.e., the first order differences can be computed from the zeroth order differences,
 90 the second order differences from the first, and so on.

91 The constants Q_m and $A_{j,mk}^{(r)}$ can be determined in a straightforward manner. The derivation of Q_m
 92 and $A_{0,mk}^{(4)}$ used in Eq. (8) for computing $IS_0^{(4)}$ will be presented next. For $r = 4$, a cubic polynomial
 93 is reconstructed from each sub-stencil. Let the cubic polynomial be expressed in terms of the Taylor
 94 series coefficients about the cell centre x_i as shown below.

$$\mathcal{U}(x) = \mathcal{U}_i + \frac{d\mathcal{U}}{dx}(x - x_i) + \frac{1}{2} \frac{d^2\mathcal{U}}{dx^2}(x - x_i)^2 + \frac{1}{6} \frac{d^3\mathcal{U}}{dx^3}(x - x_i)^3 \quad (10)$$

95 $\mathcal{U}_i = \mathcal{U}(x_i)$ refers to the point value at x_i and the derivatives are also evaluated at x_i . Substituting
 96 Eq. (10) into Eq. (5) and simplifying yields the general expression for $IS_j^{(4)}$.

$$IS_j^{(4)} = 1 \cdot \left[\frac{d\mathcal{U}}{dx} \Delta x + \frac{1}{24} \frac{d^3\mathcal{U}}{dx^3} \Delta x^3 \right]^2 + \frac{13}{12} \cdot \left[\frac{d^2\mathcal{U}}{dx^2} \Delta x^2 \right]^2 + \frac{781}{720} \cdot \left[\frac{d^3\mathcal{U}}{dx^3} \Delta x^3 \right]^2 \quad (11)$$

97 The constants which pre-multiply each pair of square brackets in Eq. (11) are $Q_m/(m!)^2$. These
 98 constants factor out when the smoothness indicator is written as a sum of squares under the condition
 99 that the coefficient of the leading order term inside each pair of square brackets be unity. It must be
 100 remarked that these constants are the same for all combinations of r and j . They are listed in Table 3
 101 in the Appendix for $m = 1$ to $m = 5$.

102 For $j = 0$, the sub-stencil $\mathcal{S}_{0,i+1/2}^L$ consists of cells $\{i - 3, i - 2, i - 1, i\}$. Averaging Eq. (10) over
 103 each of these four cells yields the expression for the respective cell average in terms of the Taylor
 104 series terms which can be cast into a linear system as follows.

$$\begin{pmatrix} \bar{u}_{i-3} \\ \bar{u}_{i-2} \\ \bar{u}_{i-1} \\ \bar{u}_i \end{pmatrix} = \begin{bmatrix} 1 & -3 & \frac{109}{24} & -\frac{37}{8} \\ 1 & -2 & \frac{49}{24} & -\frac{17}{12} \\ 1 & -1 & \frac{13}{24} & -\frac{5}{24} \\ 1 & 0 & \frac{1}{24} & 0 \end{bmatrix} \begin{pmatrix} \mathcal{U}_i \\ \frac{d\mathcal{U}}{dx} \Delta x \\ \frac{d^2\mathcal{U}}{dx^2} \Delta x^2 \\ \frac{d^3\mathcal{U}}{dx^3} \Delta x^3 \end{pmatrix} \quad (12)$$

105

106 The first order undivided differences ($m = 1$) can be computed from Eq. (12) as follows.

$$\begin{pmatrix} \Delta^1[\bar{u}_{i-3}] \\ \Delta^1[\bar{u}_{i-2}] \\ \Delta^1[\bar{u}_{i-1}] \end{pmatrix} = \begin{bmatrix} -1 & 1 & & \\ & -1 & 1 & \\ & & -1 & 1 \end{bmatrix} \begin{pmatrix} \bar{u}_{i-3} \\ \bar{u}_{i-2} \\ \bar{u}_{i-1} \\ \bar{u}_i \end{pmatrix} = \begin{bmatrix} 1 & -\frac{5}{2} & \frac{77}{24} \\ \mathbf{1} & -\frac{3}{2} & \frac{29}{24} \\ \mathbf{1} & -\frac{1}{2} & \frac{5}{24} \end{bmatrix} \begin{pmatrix} \frac{dU}{dx}\Delta x \\ \frac{d^2U}{dx^2}\Delta x^2 \\ \frac{d^3U}{dx^3}\Delta x^3 \end{pmatrix} \quad (13)$$

107 Now, a linear combination of the first order undivided differences is sought such that it results in the
108 term inside the first pair of square brackets on the RHS of Eq. (11).

$$A_{0,10}^{(4)}\Delta^1[\bar{u}_{i-3}] + A_{0,11}^{(4)}\Delta^1[\bar{u}_{i-2}] + A_{0,12}^{(4)}\Delta^1[\bar{u}_{i-1}] = \frac{dU}{dx}\Delta x + \frac{1}{24}\frac{d^3U}{dx^3}\Delta x^3$$

$$\begin{pmatrix} A_{0,10}^{(4)} \\ A_{0,11}^{(4)} \\ A_{0,12}^{(4)} \end{pmatrix}^T \begin{pmatrix} \Delta^1[\bar{u}_{i-3}] \\ \Delta^1[\bar{u}_{i-2}] \\ \Delta^1[\bar{u}_{i-1}] \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ \frac{1}{24} \end{pmatrix}^T \begin{pmatrix} \frac{dU}{dx}\Delta x \\ \frac{d^2U}{dx^2}\Delta x^2 \\ \frac{d^3U}{dx^3}\Delta x^3 \end{pmatrix} \quad (14)$$

109 Eqs. (13) and (14) lead to the following linear system which can be solved for the constants $A_{0,1k}^{(4)}$.

$$\begin{bmatrix} 1 & 1 & 1 \\ -\frac{5}{2} & -\frac{3}{2} & -\frac{1}{2} \\ \frac{77}{24} & \frac{29}{24} & \frac{5}{24} \end{bmatrix} \begin{pmatrix} A_{0,10}^{(4)} \\ A_{0,11}^{(4)} \\ A_{0,12}^{(4)} \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ \frac{1}{24} \end{pmatrix} \Rightarrow \begin{pmatrix} A_{0,10}^{(4)} \\ A_{0,11}^{(4)} \\ A_{0,12}^{(4)} \end{pmatrix} = \begin{pmatrix} \frac{1}{3} \\ -\frac{7}{6} \\ \frac{11}{6} \end{pmatrix} \quad (15)$$

110 Comparing the values of $A_{0,1k}^{(4)}$ with those in Eq. (8), it can be observed that there is a difference in
111 sign. However, this is inconsequential as the term inside each square bracket is squared.

112 Next, the second order undivided differences ($m = 2$) can be computed from Eq. (13) as follows.

$$\begin{pmatrix} \Delta^2[\bar{u}_{i-3}] \\ \Delta^2[\bar{u}_{i-2}] \end{pmatrix} = \begin{bmatrix} -1 & 1 & \\ & -1 & 1 \end{bmatrix} \begin{pmatrix} \Delta^1[\bar{u}_{i-3}] \\ \Delta^1[\bar{u}_{i-2}] \\ \Delta^1[\bar{u}_{i-1}] \end{pmatrix} = \begin{bmatrix} 1 & -2 \\ \mathbf{1} & -1 \end{bmatrix} \begin{pmatrix} \frac{d^2U}{dx^2}\Delta x^2 \\ \frac{d^3U}{dx^3}\Delta x^3 \end{pmatrix} \quad (16)$$

113 Now, a linear combination of the second order undivided differences is sought such that it results in
114 the term inside the second pair of square brackets on the RHS of Eq. (11).

$$A_{0,20}^{(4)}\Delta^2[\bar{u}_{i-3}] + A_{0,21}^{(4)}\Delta^2[\bar{u}_{i-2}] = \frac{d^2U}{dx^2}\Delta x^2 \quad (17)$$

$$\begin{pmatrix} A_{0,20}^{(4)} \\ A_{0,21}^{(4)} \end{pmatrix}^T \begin{pmatrix} \Delta^2[\bar{u}_{i-3}] \\ \Delta^2[\bar{u}_{i-2}] \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \end{pmatrix}^T \begin{pmatrix} \frac{d^2\mathcal{U}}{dx^2}\Delta x^2 \\ \frac{d^3\mathcal{U}}{dx^3}\Delta x^3 \end{pmatrix}$$

115 Eqs. (16) and (17) lead to the following linear system which can be solved for the constants $A_{0,2k}^{(4)}$.

$$\begin{bmatrix} 1 & 1 \\ -2 & -1 \end{bmatrix} \begin{pmatrix} A_{0,20}^{(4)} \\ A_{0,21}^{(4)} \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \end{pmatrix} \Rightarrow \begin{pmatrix} A_{0,20}^{(4)} \\ A_{0,21}^{(4)} \end{pmatrix} = \begin{pmatrix} -1 \\ 2 \end{pmatrix} \quad (18)$$

116 Finally, the third order undivided difference ($m = 3$) can be computed from Eq. (16) as follows.

$$\Delta^3[\bar{u}_{i-3}] = \begin{bmatrix} -1 & 1 \end{bmatrix} \begin{pmatrix} \Delta^2[\bar{u}_{i-3}] \\ \Delta^2[\bar{u}_{i-2}] \end{pmatrix} = \frac{d^3\mathcal{U}}{dx^3}\Delta x^3 \quad (19)$$

117 By inspection with the term inside the third pair of square brackets on the RHS of Eq. (11), it can be
 118 seen that the constant $A_{0,30}^{(4)} = 1$. The derivation procedure is similar for other combinations of r and
 119 j . The constants $A_{j,mk}^{(r)}$ are listed in Tables 4-7 in the Appendix for $r = 3$ to $r = 6$.

120 Determining the constants $A_{j,mk}^{(r)}$ for a $(2r - 1)$ th order WENO scheme requires solving $r - 1$ linear
 121 systems, one for each order of undivided differences from first order to $(r - 1)$ th order. Obviously,
 122 all $r - 1$ matrices must remain non-singular for the procedure to be successful. The fact that the
 123 matrices remain non-singular for any r can be proved as follows. The general expression for the cell
 124 average \bar{u}_{i+k} can be obtained from an $(r - 1)$ th order polynomial approximation as given below.

$$\begin{aligned} \bar{u}_{i+k} = \Delta^0[\bar{u}_{i+k}] &= \frac{1}{\Delta x} \int_{x_i+(k-1/2)\Delta x}^{x_i+(k+1/2)\Delta x} \left[\sum_{n=0}^{r-1} \frac{1}{n!} \frac{d^n \mathcal{U}}{dx^n} (x - x_i)^n \right] dx \\ &= \sum_{n=0}^{r-1} \left\{ \frac{1}{(n+1)!} \left[\left(k + \frac{1}{2}\right)^{n+1} - \left(k - \frac{1}{2}\right)^{n+1} \right] \right\} \frac{d^n \mathcal{U}}{dx^n} \Delta x^n \end{aligned} \quad (20)$$

125 For simplicity, the notation $\frac{d^0 \mathcal{U}}{dx^0} = \mathcal{U}_i$ has been introduced in the above result. The derivation
 126 procedure begins with the linear system $\Delta^0[\bar{\mathbf{u}}] = R_0 d\mathcal{U}_0$ similar to Eq. (12) where $\Delta^0[\bar{\mathbf{u}}]$ represents
 127 the vector of r cell averages in sub-stencil j and $d\mathcal{U}_0$ the vector of the Taylor series terms $\frac{d^n \mathcal{U}}{dx^n} \Delta x^n$

128 from $n = 0$ to $n = r - 1$. Elements of the $r \times r$ matrix R_0 are the coefficients inside the curly
 129 brackets in Eq. (20) evaluated for appropriate values of k and n . Since the point value $\mathcal{U}_i =$
 130 $(R_0^{-1} \Delta^0[\bar{\mathbf{u}}])$ can be uniquely determined from the polynomial approximation, R_0 must be invertible.

131 The vector of first order undivided differences $\Delta^1[\bar{\mathbf{u}}]$ is obtained by multiplying the $(r - 1) \times r$
 132 difference matrix D_r to $\Delta^0[\bar{\mathbf{u}}]$ as shown below.

$$\Delta^1[\bar{\mathbf{u}}] = \overbrace{\begin{bmatrix} -1 & 1 & & & \\ & -1 & 1 & & \\ & & \ddots & \ddots & \\ & & & -1 & 1 \end{bmatrix}}^{D_r} \Delta^0[\bar{\mathbf{u}}] = (D_r R_0) d\mathcal{U}_0 \quad (21)$$

133 The difference matrix D_r has a rank of $r - 1$. The $(r - 1) \times r$ matrix $(D_r R_0)$ must also have a rank
 134 of $r - 1$ since multiplication by an invertible matrix preserves rank. Substituting $n = 0$ into the term
 135 inside the curly brackets in Eq. (20), it can be easily verified that the coefficient of $\frac{d^0 \mathcal{U}}{dx^0} \Delta x^0$ in
 136 $\Delta^0[\bar{u}_{i+k}]$ is one for all values of k . Therefore, the first column of R_0 consists of ones. Applying the
 137 difference matrix D_r to R_0 results in the first column of $(D_r R_0)$ being all zeros, i.e., $(D_r R_0)$ has the
 138 form $(D_r R_0) = [\mathbf{0} \quad R_1]$ where R_1 is an $(r - 1) \times (r - 1)$ matrix. For $(D_r R_0)$ to have rank $(r - 1)$,
 139 R_1 must have the full rank of $r - 1$ since $\text{span}\{\text{cols}(D_r R_0)\} = \text{span}\{\text{cols}(R_1)\}$. Thus, R_1 is also
 140 non-singular. Since the first column of $(D_r R_0)$ consists of zeros, Eq. (21) can be simplified to
 141 $\Delta^1[\bar{\mathbf{u}}] = R_1 d\mathcal{U}_1$ where $d\mathcal{U}_1$ is the vector of Taylor series terms $\frac{d^n \mathcal{U}}{dx^n} \Delta x^n$ from $n = 1$ to $n = r - 1$.
 142 This is precisely the result obtained earlier in Eq. (13) for the particular case of $r = 3$ and $j = 0$.
 143 Comparing the matrices in Eqs. (13) and (15), it can be concluded that determining constants $A_{j,1k}^{(r)}$
 144 requires R_1^T to be non-singular. Since $(R_1^T)^{-1} = (R_1^{-1})^T$ and since R_1 has been shown to be non-
 145 singular, R_1^T is also non-singular and the constants $A_{j,1k}^{(r)}$ can be uniquely determined.

146 The argument for higher orders proceeds inductively in the same manner. In general, $\Delta^m[\bar{\mathbf{u}}] =$
 147 $R_m d\mathcal{U}_m$ and $\Delta^{m+1}[\bar{\mathbf{u}}] = D_{r-m} \Delta^m[\bar{\mathbf{u}}] = (D_{r-m} R_m) d\mathcal{U}_m$. Here R_m is an $(r - m) \times (r - m)$
 148 matrix, $d\mathcal{U}_m$ is the vector of Taylor series terms $\frac{d^n \mathcal{U}}{dx^n} \Delta x^n$ from $n = m$ to $n = r - 1$, and D_{r-m} is the

149 $(r - m - 1) \times (r - m)$ difference matrix. The crucial point is that the first column of R_m consists of
 150 ones for all m . In other words, the coefficient of $\frac{d^m u}{dx^m} \Delta x^m$ in $\Delta^m[\bar{u}_{i+k}]$ is one regardless of the value
 151 of k . Denoting this coefficient as C_m , it can be shown from Eq. (20) that C_m has the following form.

$$C_m = \frac{1}{(m+1)!} \sum_{n=0}^{m+1} (-1)^n \binom{m+1}{n} \left(k + m + \frac{1}{2} - n\right)^{m+1} \quad (22)$$

152 The proof that $C_m = 1$ follows from Eq. (6.22) in Ref. [14]. So, the $(r - m - 1) \times (r - m)$ matrix
 153 $(D_{r-m} R_m)$ has a first column of zeros. The remaining $(r - m - 1)$ columns form the matrix R_{m+1} .
 154 Based on the same argument used for $m = 0$, it follows that if R_m is non-singular, then so is R_{m+1} .
 155 Since an $(r - 1)$ th polynomial reconstruction on uniform grid always produces a non-singular matrix
 156 R_0 , all matrices R_m for $m = 1$ to $m = r - 1$ are non-singular. Therefore, the procedure can be
 157 successfully extended to any order.

158 2.3 Comparison of algorithms

159 Since the undivided differences $\Delta^m[\bar{u}_i]$ can be computed efficiently, the proposed algorithm brings
 160 about significant computational savings compared to the compact implementation. The approximate
 161 number of floating-point operations required for computing the r smoothness indicators of a $(2r -$
 162 $1)$ th order WENO scheme using the different implementations is listed in Table 1. The operations
 163 required to compute the undivided differences have been accounted for in the operation count for
 164 the proposed algorithm. The proposed algorithm requires only about 60% the number of
 165 multiplication operations and about 80% the number of addition/subtraction operations as the compact
 166 implementation. A comparison of the number of constants required (including Q_m) is also given in
 167 Table 1. It can be seen that the proposed algorithm requires only about half the number of constants as
 168 the compact implementation. Hence, the proposed algorithm can be implemented relatively faster.

169 The compact and proposed algorithms were implemented in an in-house Euler code which uses a
 170 hybrid flux methodology [15]. Unlike conventional Euler codes which reconstruct fluxes, the hybrid
 171 flux methodology relies on the reconstruction of primitive variables predominantly. This allows the

Table 1: Comparison of number of floating-point operations (\pm , \times) and constants (C) required for smoothness indicators

	Compact [Eq. (6)]			Proposed [Eq. (9)]		
WENO5	15 \pm	30 \times	20 C	13 \pm	18 \times	11 C
WENO7	44 \pm	72 \times	51 C	35 \pm	44 \times	27 C
WENO9	95 \pm	140 \times	104 C	71 \pm	85 \times	54 C
WENO11	174 \pm	240 \times	185 C	124 \pm	144 \times	95 C

172 undivided differences to be reused for the left- and right-biased WENO reconstructions. The in-house
173 code was used to compute the Shu-Osher shock-entropy wave interaction problem [16] and the double
174 Mach reflection problem [17] at several difference resolutions. The double Mach reflection problem
175 was set up using the second alternative method described in Ref. [18] to obtain clean, artefact-free
176 solutions. Solutions obtained from both algorithms were identical. The speedups achieved by the
177 proposed algorithm over the compact algorithm are given in Table 2.

178 Though the speedups were somewhat marginal for fifth order, they started to increase quickly for
179 higher orders. The proposed algorithm shortened the computation time by about 6% and 10% for
180 ninth and eleventh orders, respectively. The speedups are expected to increase further for even higher
181 orders. With a proper implementation, there is a potential for greater savings when the undivided
182 differences are computed for an entire row/column of cells at a time in structured Cartesian grids as
183 adjacent faces along a row/column share all but one sub-stencils.

184

185 **3 Conclusion**

186 Computing sub-stencil smoothness indicators is the most expensive operation in the WENO
187 reconstruction procedure. In this paper, an efficient algorithm for computing these quantities is
188 presented. For a $(2r - 1)$ th order WENO scheme, a table of undivided differences is constructed up
189 to order $r - 1$ in a recursive manner. Then, the smoothness indicators are computed as squares of
190 linear combinations of these undivided differences ensuring positivity of the computed values. It has

Table 2: Comparison of speedups achieved using proposed algorithm [Eq. (9)] over compact algorithm [Eq. (6)]

Case	Resolution	WENO5	WENO7	WENO9	WENO11
Shock-entropy	400	1.014	1.024	1.049	1.081
wave interaction	800	1.016	1.011	1.058	1.117
problem	1600	1.021	1.018	1.064	1.130
Double Mach	480×120	1.002	1.017	1.067	1.092
reflection	960×240	1.008	1.032	1.062	1.094
problem	1920×480	1.003	1.038	1.067	1.098

191 been shown that the proposed algorithm requires considerably fewer floating-point operations and
 192 fewer constants compared to the compact implementation.

193

194 4 Appendix

195 The constants $Q_m/(m!)^2$ are given in Table 3.

Table 3: Constants $Q_m/(m!)^2$

m	1	2	3	4	5
$Q_m/(m!)^2$	1	$\frac{13}{12}$	$\frac{781}{720}$	$\frac{1421461}{1310400}$	$\frac{21520059541}{19838649600}$

196 The constants $A_{j,mk}^{(r)}$ are given in Tables 4-7 for $r = 3$ to $r = 6$.

Table 4: Constants $A_{j,mk}^{(r)}$ for $r = 3$

		k	
j	m	0	1
0	1	$-\frac{1}{2}$	$\frac{3}{2}$
	2	1	-
1	1	$\frac{1}{2}$	$\frac{1}{2}$
	2	1	-

197

2	1	$\frac{3}{2}$	$-\frac{1}{2}$
	2	1	-

Table 5: Constants $A_{j,mk}^{(r)}$ for $r = 4$

		k		
j	m	0	1	2
0	1	$\frac{1}{3}$	$-\frac{7}{6}$	$\frac{11}{6}$
	2	-1	2	-
	3	1	-	-
1	1	$-\frac{1}{6}$	$\frac{5}{6}$	$\frac{1}{3}$
	2	0	1	-
	3	1	-	-
2	1	$\frac{1}{3}$	$\frac{5}{6}$	$-\frac{1}{6}$
	2	1	0	-
	3	1	-	-
3	1	$\frac{11}{6}$	$-\frac{7}{6}$	$\frac{1}{3}$
	2	2	-1	-
	3	1	-	-

198

Table 6: Constants $A_{j,mk}^{(r)}$ for $r = 5$

		k			
j	m	0	1	2	3
0	1	$-\frac{1}{4}$	$\frac{13}{12}$	$-\frac{23}{12}$	$\frac{25}{12}$
	2	$\frac{119}{130}$	$-\frac{184}{65}$	$\frac{379}{130}$	-
	3	$-\frac{3}{2}$	$\frac{5}{2}$	-	-
	4	1	-	-	-
1	1	$\frac{1}{12}$	$-\frac{5}{12}$	$\frac{13}{12}$	$\frac{1}{4}$
	2	$-\frac{11}{130}$	$\frac{11}{65}$	$\frac{119}{130}$	-
	3	$-\frac{1}{2}$	$\frac{3}{2}$	-	-

	4	1	-	-	-
2	1	$-\frac{1}{12}$	$\frac{7}{12}$	$\frac{7}{12}$	$-\frac{1}{12}$
	2	$-\frac{11}{130}$	$\frac{76}{65}$	$-\frac{11}{130}$	-
	3	$\frac{1}{2}$	$\frac{1}{2}$	-	-
	4	1	-	-	-
3	1	$\frac{1}{4}$	$\frac{13}{12}$	$-\frac{5}{12}$	$\frac{1}{12}$
	2	$\frac{119}{130}$	$\frac{11}{65}$	$-\frac{11}{130}$	-
	3	$\frac{3}{2}$	$-\frac{1}{2}$	-	-
	4	1	-	-	-
4	1	$\frac{25}{12}$	$-\frac{23}{12}$	$\frac{13}{12}$	$-\frac{1}{4}$
	2	$\frac{379}{130}$	$-\frac{184}{65}$	$\frac{119}{130}$	-
	3	$\frac{5}{2}$	$-\frac{3}{2}$	-	-
	4	1	-	-	-

Table 7: Constants $A_{j,mk}^{(r)}$ for $r = 6$

j	m	k				
		0	1	2	3	4
0	1	$\frac{1}{5}$	$-\frac{21}{20}$	$\frac{137}{60}$	$-\frac{163}{60}$	$\frac{137}{60}$
	2	$-\frac{54}{65}$	$\frac{443}{130}$	$-\frac{346}{65}$	$\frac{487}{130}$	-
	3	$\frac{114721}{65604}$	$-\frac{81962}{16401}$	$\frac{278731}{65604}$	-	-
	4	-2	3	-	-	-
	5	1	-	-	-	-
1	1	$-\frac{1}{20}$	$\frac{17}{60}$	$-\frac{43}{60}$	$\frac{77}{60}$	$\frac{1}{5}$
	2	$\frac{11}{130}$	$-\frac{22}{65}$	$\frac{11}{26}$	$\frac{54}{65}$	-
	3	$\frac{16315}{65604}$	$-\frac{16358}{16401}$	$\frac{114721}{65604}$	-	-
	4	-1	2	-	-	-
	5	1	-	-	-	-
2	1	$\frac{1}{30}$	$-\frac{13}{60}$	$\frac{47}{60}$	$\frac{9}{20}$	$-\frac{1}{20}$
	2	0	$-\frac{11}{130}$	$\frac{76}{65}$	$-\frac{11}{130}$	-
	3	$-\frac{16487}{65604}$	$\frac{16444}{16401}$	$\frac{16315}{65604}$	-	-

	4	0	1	-	-	-
	5	1	-	-	-	-
3	1	$-\frac{1}{20}$	$\frac{9}{20}$	$\frac{47}{60}$	$-\frac{13}{60}$	$\frac{1}{30}$
	2	$-\frac{11}{130}$	$\frac{76}{65}$	$-\frac{11}{130}$	0	-
	3	$\frac{16315}{65604}$	$\frac{16444}{16401}$	$-\frac{16487}{65604}$	-	-
	4	1	0	-	-	-
	5	1	-	-	-	-
4	1	$\frac{1}{5}$	$\frac{77}{60}$	$-\frac{43}{60}$	$\frac{17}{60}$	$-\frac{1}{20}$
	2	$\frac{54}{65}$	$\frac{11}{26}$	$-\frac{22}{65}$	$\frac{11}{130}$	-
	3	$\frac{114721}{65604}$	$-\frac{16358}{16401}$	$\frac{16315}{65604}$	-	-
	4	2	-1	-	-	-
	5	1	-	-	-	-
5	1	$\frac{137}{60}$	$-\frac{163}{60}$	$\frac{137}{60}$	$-\frac{21}{20}$	$\frac{1}{5}$
	2	$\frac{487}{130}$	$-\frac{346}{65}$	$\frac{443}{130}$	$-\frac{54}{65}$	-
	3	$\frac{278731}{65604}$	$-\frac{81962}{16401}$	$\frac{114721}{65604}$	-	-
	4	3	-2	-	-	-
	5	1	-	-	-	-

200

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204

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