

# From skin mechanics to tactile neural coding: Predicting afferent neural dynamics during active touch and perception

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1  
2 **Abstract**— First order cutaneous neurons allow object  
3 recognition, texture discrimination, and sensorimotor  
4 feedback. Their function is well-investigated under passive  
5 stimulation while their role during active touch or  
6 sensorimotor control is understudied. To understand how  
7 human perception and sensorimotor controlling strategy  
8 depend on cutaneous neural signals under active tactile  
9 exploration, the finite element (FE) hand and Izhikevich  
10 neural dynamic model were combined to predict the  
11 cutaneous neural dynamics and the resulting perception  
12 during a discrimination test. Using *in-vivo* microneurography  
13 generated single afferent recordings, 75% of the data was  
14 applied for the model optimization and another 25% was  
15 used for validation. By using this integrated numerical model,  
16 the predicted tactile neural signals of the single afferent fibers  
17 agreed well with the microneurography test results, achieving  
18 the out-of-sample values of 0.94 and 0.82 for slowly adapting  
19 type I (SAI) and fast adapting type I unit (FAI) respectively.  
20 Similar discriminating capability with the human subject was  
21 achieved based on this computational model. Comparable  
22 performance with the published numerical model on  
23 predicting the cutaneous neural response under passive  
24 stimuli was also presented, ensuring the potential  
25 applicability of this multi-level numerical model in studying  
26 the human tactile sensing mechanisms during active touch.  
27 The predicted population-level 1st order afferent neural  
28 signals under active touch suggest that different coding  
29 strategies might be applied to the afferent neural signals  
30 elicited from different cutaneous neurons simultaneously.

31  
32 **Index Terms**—Neurophysiological, skin mechanics, FE  
33 Human hand, neural coding, active touch.

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I. INTRODUCTION

35 **O**ur ability to perceive and manipulate objects relies  
36 fundamentally on subclasses of primary mechanosensory  
37 neurons in the glabrous skin of the hand. They provide  
38 tactile feedback enabling our somatosensory system to  
39 inform the sensorimotor control loop and build the  
40 interface between the world and the somatosensory cortex.  
41 The closed-loop control allows us to voluntarily perceive  
42 and manipulate objects during active touch, acquiring the  
43 information based on perception. The typical case of  
44 sensorimotor control is the reflex caused between  
45 cutaneous mechanoreceptors and the efferent motor neuron  
46 modulating muscle forces [1, 2]. The external stimuli are  
47 encoded by cutaneous receptors as 1<sup>st</sup> order afferent neural  
48 signals and then transmitted to the spinal cord and higher  
49 central nervous system (CNS) for further processing and  
50 decoding [3].

51 Over the past decades, research has focused on capturing  
52 the single-fiber afferent signals from the peripheral neural  
53 system [4, 5] using the technique of microneurography,  
54 applying numerical models to understand the neural  
55 dynamics and the mechano-electrical mechanisms of the  
56 cutaneous receptors under different stimulus conditions.  
57 Quantifying the relationships between the stimuli and the  
58 state of stress/strain at the site of mechanoreceptors. In  
59 2003, Dandekar et al. showed that the strain energy density  
60 can be quantitatively related with the membrane current  
61 through the cutaneous receptor and then applied this for  
62 predicting neural dynamics [6]. Another study was  
63 conducted by delivering passive stimuli to the finite  
64 element (FE) model, strain energy density (SED) was  
65 extracted for evaluating the afferent neural signals and  
66 validated against the microneurography results [7]. Similar  
67 numerical models based on continuum mechanics have  
68 also been applied to simulate population-level afferent  
69 signals under passive stimulation using model parameters  
70 derived from afferent spiking data in monkey glabrous skin  
71 [8]. However, previous numerical models did not  
72 incorporate the lateral sliding, realistic skin contact  
73 mechanism, or the hyper-elastic material properties of soft  
74 tissues. Also, muscle actuated active touch was not  
75 integrated with the numerical model, only passive stimuli

76 were simulated with the simplified FE finger-tip model [7,  
77 9]. It has been shown that different skin mechanics and  
78 neural responses during active touch could be altered from  
79 those evoked by passive stimuli [10-12]. However, the  
80 neural dynamics under muscle-driven active touch are  
81 difficult to capture using microneurography since the  
82 subject needs to be restrained and have relaxed muscles  
83 since electromyography signals may mask the afferent  
84 signals [13]. Therefore, the neural response or the  
85 mechano-electrical properties of cutaneous neurons under  
86 active touch still remains unknown [8, 14] warranting  
87 being explicitly studied through the muscle-driven FE hand  
88 model.

89 Tactile perception is based on the integrated and  
90 processed population-level afferent signals from 1<sup>st</sup> order  
91 low threshold mechanoreceptors (LTM) in the skin, relays  
92 in the dorsal column nuclei and then via the thalamus to the  
93 somatosensory cortex. Research has shown that the  
94 collection of the group responses from 1st order cutaneous  
95 neurons is critical for understanding the tactile neural  
96 coding and the sensorimotor mechanism [2, 14]. Therefore,  
97 the second step of neural coding after the 1<sup>st</sup> order  
98 cutaneous mechanoreceptors is to understand how  
99 perception depends on these population-level afferent  
100 dynamics [3], the external stimuli should be related to the  
101 final human percept across the intact afferent transduction  
102 path under the active touch. The relationship between

103 perception and afferent dynamics has been studied using  
104 *in-vivo* neural microstimulation of single peripheral  
105 afferents and the somatosensory cortex in awake subjects.  
106 Electrical stimulation of single afferent fibers in awake  
107 humans through a microneurography recording electrode, a  
108 technique termed intra-neural microstimulation, first  
109 reported by Ochoa et al [15], indicating that activity in a  
110 single afferent fiber could be perceived with perceptual  
111 qualities that depend upon the afferent type. A series of  
112 *in-vivo* tests conducted by stimulating area 3b to study  
113 temporal coding mechanisms in non-human primates [16]  
114 showed that the frequency discrimination of the subjects  
115 may depend on temporal coding and is more general than  
116 rate coding. However, recording afferent dynamics from  
117 population-level afferent fibers is technically demanding,  
118 and the invasive experiment on living subjects cannot be  
119 avoided [17, 18]. Implementation of the numerical model  
120 might be an effective method to obtain the fairly accurate  
121 population-level cutaneous signals and study the coding  
122 mechanism across the intact somatosensory path from the  
123 external stimuli to the final perception. Also, this study  
124 presents the possibility of using FE based integrated  
125 numerical model as a novel method to investigate the  
126 human sensorimotor mechanisms.

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## II. METHODOLOGY

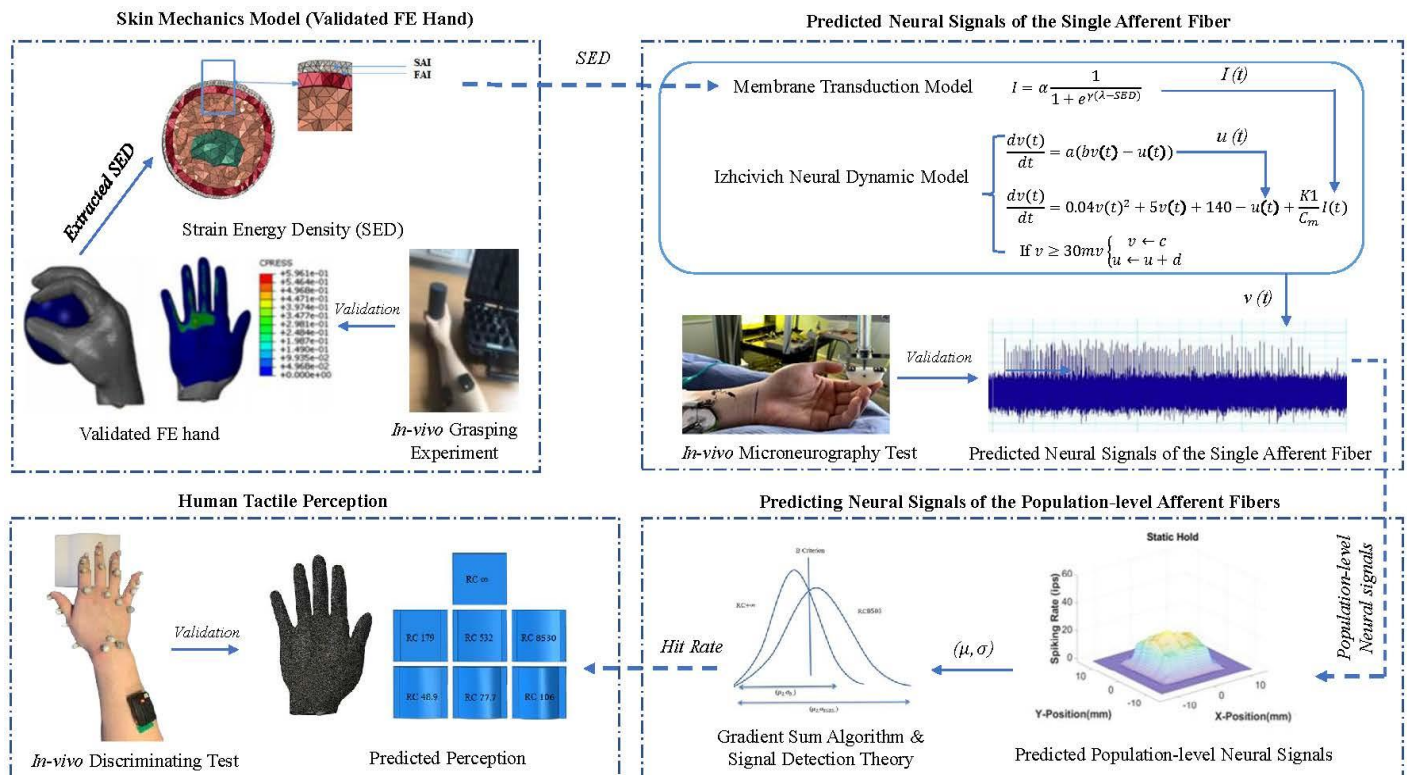


Fig. 1. Main procedure of this research. From the development of the FE human hand model to the predictions of the tactile neural signals. At the first step (Skin mechanics model), the SED during active touch was extracted at the site of mechanoreceptors as input of the membrane transduction model of step 2 (Predicting neural signals of the single afferent fiber). The neural signals from a single afferent tactile fiber were predicted and validated against microneurography results, this procedure was duplicated in step 3 (Predicting neural signals of the population-level afferent fibers) to derive the population-level afferent tactile neural signals. The signal detection theory was employed to correlate the computed neural signals with predicted human perception or the hit rate in step 4 (human tactile perception). The predicted hit rate was validated with the results of the *in-vivo* discrimination test.

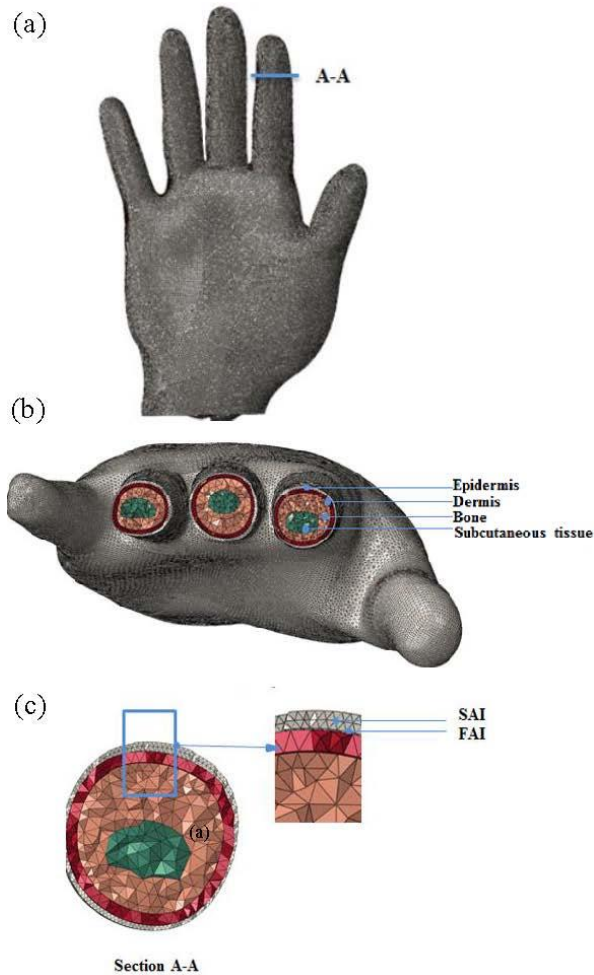


Fig. 2. The skin mechanics model (a). The FE human hand model. (b). The four-layered structure was modelled for extracting proper SED during the active touch including bones, subcutaneous tissue, dermis and epidermis from inside to outside. (c). The cross-sectional view of the index finger. The locations for extracting strain energy density of SAI/FAI mechanoreceptor. The SED of SAI was extracted at the top point of the tetrahedral element at the boundary between the epidermis and dermis while for FAI unit, the SED was computed at the bottom points of the elements on the epidermis-dermis boundary.

129 The integrated numerical model was developed,  
 130 optimized and validated on three different levels (see Fig.  
 131 1): A) Skin mechanics (strain/stress environment at the site  
 132 of the cutaneous mechanoreceptors). B) To give the  
 133 explicit transformation between skin mechanics and neural  
 134 activity. (Predicted neural action potentials of a signal  
 135 tactile fiber were optimized and validated against the  
 136 results of microneurography). C) Population-level neural  
 137 signals to human perception. (Predicted population-level  
 138 tactile neural signals were compared with the *in-vivo*  
 139 experimental results, signal detection theory was used to  
 140 make the decision). This research began with finding the  
 141 parameter to link the skin mechanics with the transduction  
 142 membrane current across cutaneous neurons. The SED and  
 143 other stress/strain values were compared with the  
 144 experimental results of microneurography, and it was  
 145 found that SED achieved the most accurate representation  
 146 of cutaneous neuron dynamics. The neural signal of a  
 147 single tactile afferent fiber was predicted as follows: The  
 148 3D FE human hand was used to simulate the procedure of

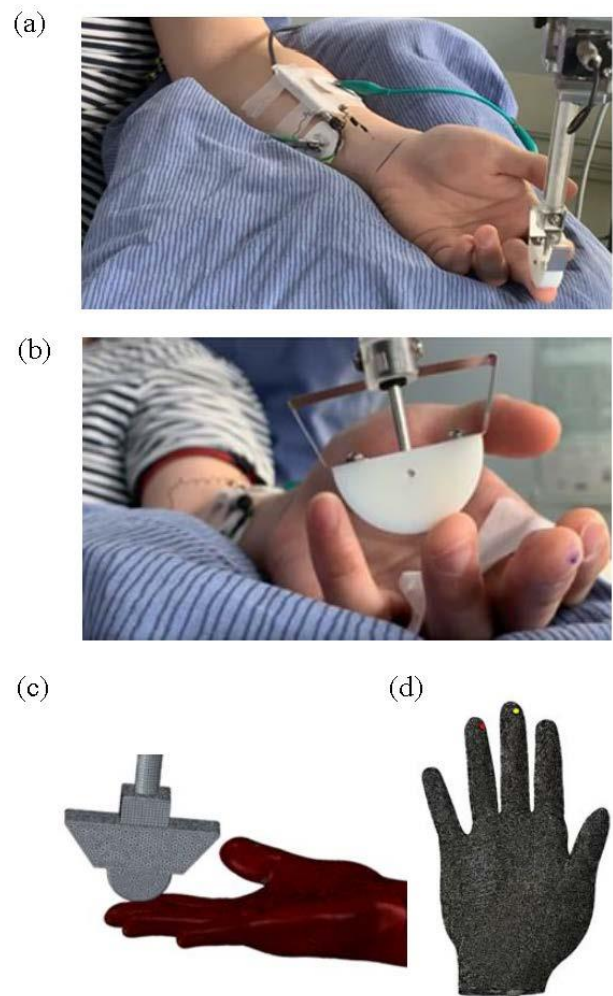


Fig. 3. The Microneurography test and the corresponding FE simulations. (a) Tungsten electrode (FHC Inc. Bowdoin, ME USA ) was inserted into median nerve, capturing the single-afferent neural signals. (b). The Robotic Tactile Stimulator (RTS) (Dancer Design Inc. Merseyside, UK) was used to deliver the stimuli onto the receptive field of a tactile unit. The RTS delivered a sweeping motion across the receptive field of the tactile unit with a specified contact force. (c) The FE simulation of the experiment. (d) The locations of the SAI and FAI tactile unit captured during microneurography which are highlighted with yellow and red dot respectively on the FE hand.

149 active touch as skin mechanics model, the SED was chosen  
 150 among the stress/strain related values and transferred into  
 151 membrane current flowing over the mechanoreceptors by  
 152 using the mechano-electrical transduction model. The  
 153 Izhikevich neural model was applied to generate the action  
 154 potentials based on the predicted membrane current. The  
 155 population-level afferent tactile signals were computed  
 156 over the fingertips by duplicating the procedure of  
 157 converting SED to neural dynamics for the single tactile  
 158 afferent fiber. At the same time, the published numerical  
 159 model 'TouchSim' [8] was employed as the benchmark to  
 160 compute neural response under passive stimuli and  
 161 compare with the performance of the multi-level numerical  
 162 model developed in this research.

#### 163 A. Skin mechanics model-FE human hand

164 A subject-specific FE human hand model [19] (see Fig.  
 165 2(a)) was developed to obtain the propagation of  
 166 stress/strain during the procedure of active touch. The FE  
 167 model includes the geometry of the epidermis, dermis,

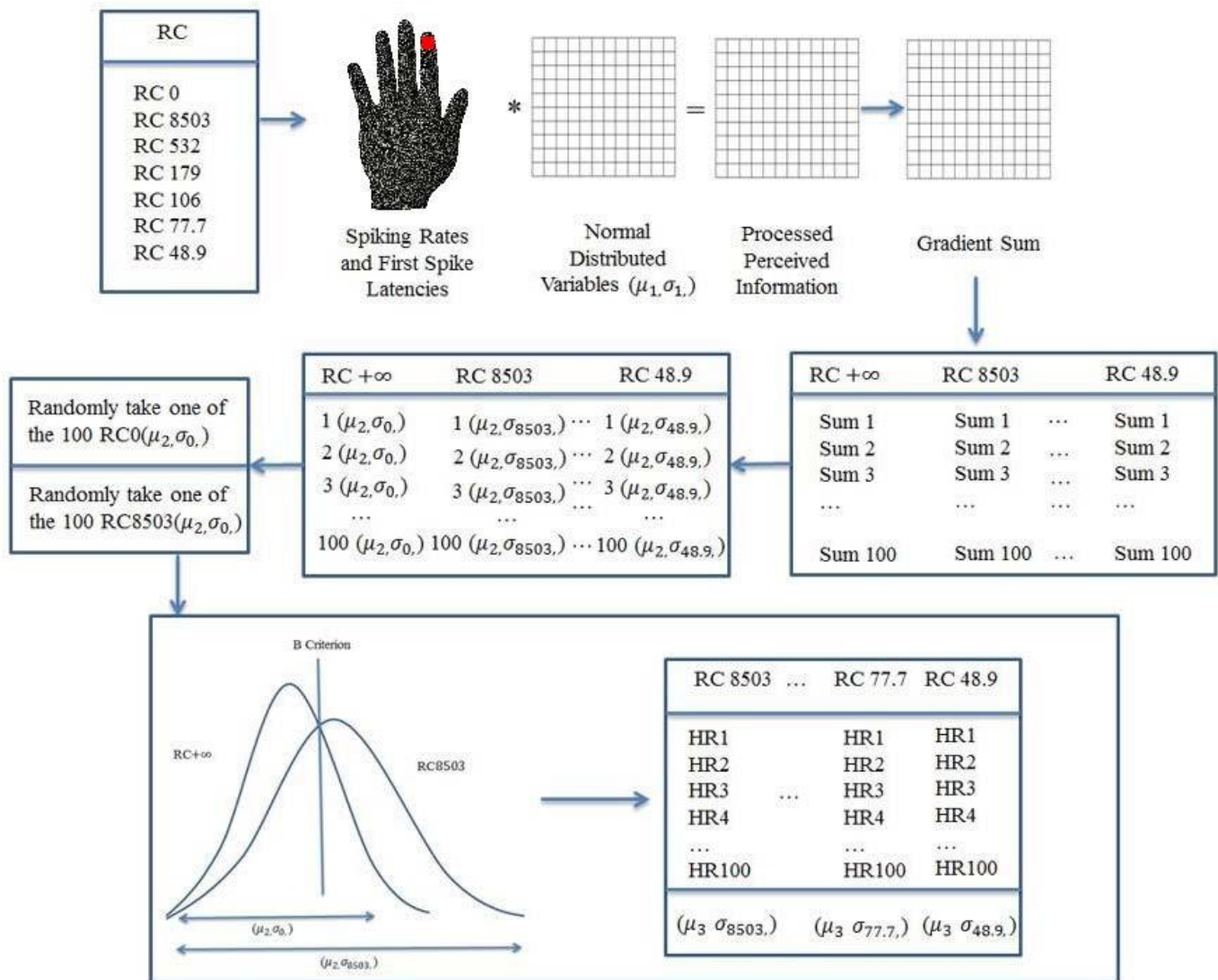


Fig. 4. The flow chart of the gradient sum approach for the population-level validation. Six convex with different radius were discriminated from the flat plate. First, the random noise is added through multiplying the neural action potential or the first spike latency of the tactile units by a pair of random variables with a mean value  $\mu=1$  and the standard deviation  $\sigma$  varied between 0.015 and 0.085. Second, the gradient sum of the elements is calculated by summing the gradients of all 100 elements together (100 SAI mechanoreceptors (elements) distributing over  $1\text{cm}^2$  area on the finger pad). Third, the first and second steps are repeated 100 times for all the 6 convex resulting in 600 gradient sums totally, 100 pairs of  $\mu_2, \sigma_2$  are derived for each convex. Fourthly, two pairs of ( $\mu_2, \sigma_2$ ) from the plate and convex were randomly selected. The signal detection theory (SDT) was used to judge whether the FE hand can differentiate the convex from the flat plate. This procedure is repeated for 100 times and the 100 discrimination accuracies or hit rates (HR) were computed for discriminating each convex surface.

168 subcutaneous tissue (see Fig. 2(b)), and the bones  
 169 reconstructed based on the MR and CT images taken from  
 170 a 23-year-old male subject. The material properties of soft  
 171 tissues were defined as isotropic hyper-elastic, and the  
 172 bones were assigned with the isotropic linear elastic  
 173 material.

174 The mesh size of the epidermis and dermis was set to be  
 175 0.1mm, 0.7mm-mesh size was assigned for subcutaneous  
 176 tissue and the bones. 1,002,915 C3D8H elements were  
 177 meshed onto this FE hand model. Three grasping (cylinder  
 178 grasping, spherical grasping, and precision gripping) were  
 179 performed. The predicted results agreed well with the  
 180 *in-vivo* experiment in terms of contact pressure and contact  
 181 area and the relative differences between the two results are  
 182 below 20%. The predicted contact area and contact  
 183 pressure can provide the bulk mechanical response of the  
 184 tissue layers [19, 20]. The detailed process for developing

185 and validating the FE human hand can be found in our  
 186 previous study [19]. Therefore, this FE human hand model  
 187 is employed to produce the stress/strain related quantities  
 188 as the skin mechanics model.

## 189 B. Predicting tactile signals of the single afferent neural 190 fiber

### 191 1) The combined transduction and neural dynamic model 192 for predicting cutaneous neural signals

193 The mechano-electrical transduction function was firstly  
 194 applied on the hair cell to explain the transducer adapting  
 195 property [21]. Researchers also used these transduction  
 196 functions to describe the mechano-electrical transaction  
 197 properties of the cutaneous mechanoreceptors and gained a  
 198 good accuracy [7, 9, 22]. The SED at the site of the  
 199 mechanoreceptor (see Fig. 2(c)) was extracted from the FE  
 200 human hand and transformed to membrane current using  
 201 the transduction function (equation 1).  $\alpha, \gamma, \lambda$  are the

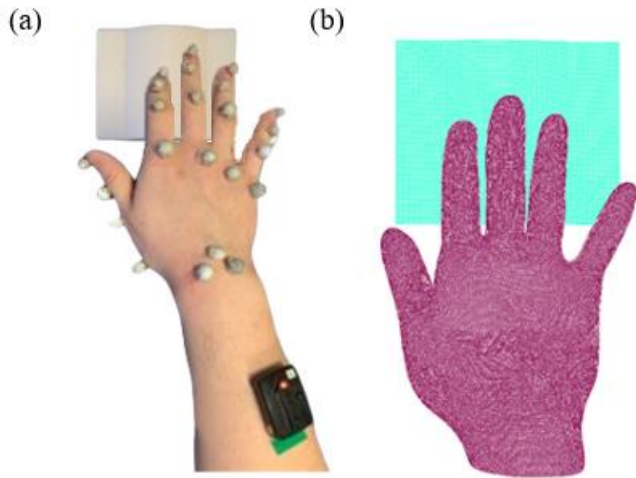


Fig. 5. *In-vivo* differentiation test and the corresponding simulation with the FE human hand (a). The *in-vivo* discrimination test. The subject was blind-folded and asked to differentiate two convex with different radius only through tactile perception. The markers were used to capture the hand kinematics during active touch using the Vicon System (Oxford Metrics Ltd., Bilston, UK). The Delsys Trigno (Delsys Inc., Boston, US) was applied to record EMG signal of the muscle. (b) The FE simulation of the discrimination test.

parameters determined through model fitting when the difference between predicted values and results of microneurography test are minimized.

$$I(SED) = \alpha \frac{1}{1 + e^{\gamma(\lambda - SED)}} \dots \dots \dots (1)$$

The cutaneous LTMs found in the glabrous skin of the human hand have distal axons that branch in the skin with irregularly spaced transduction sites [23, 24]. The spatially complex and overlapped receptive fields of the cutaneous neurons and the distance between the interdigitating subfields might determine the limit of the spatial resolution of human [25]. For this multi-level numerical model, each cutaneous tactile neuron is assumed to branch into 16 sensory organs according to the literature [26-30], echoing the fact that the first-order tactile neurons innervate on the order of ten mechanoreceptors. To simulate the heterogeneous receptive fields with highly sensitive zones of the branched axons, the SED was randomly selected at the nodes in the circular area with a diameter of 3mm [31]. At the same time, the SED was also extracted from the evenly distributed nodes for comparison and evaluating the effects of the non-uniformly distributed receptive fields of cutaneous neurons on tactile performance as is shown in Fig. S1. The neural responses were then computed based on the SED extracted from these nodes under the two different distribution patterns.

To mimic the biological neural dynamics of the tactile mechanoreceptor, the Izhikevich neural dynamic model was applied [32]. This neural dynamic model has been found to be able to reproduce the spiking, bursting response and the adaptation properties of the cutaneous mechanoreceptors [9, 22]. Among the four major types of low-threshold mechanoreceptors in the human hand, the SAI and FAI units were modelled to investigate the human sensing mechanism during spatial discrimination or active exploration in this study. Because the responses of SAI and FAI are critical to detailed feature discrimination [30, 33,

34] and sensorimotor control [35] which enables the explorative role of the hand. The responses of SAI and FAI units play a minor role in feature discrimination [34] which were not included in this numerical model.

The dynamic of the membrane potentials of SAI and FAI are defined as follows:

$$SAI: \frac{dv(t)}{dt} = 0.04v(t)^2 + 5v(t) + 140 - u(t) + \frac{K1}{Cm} I(t) \dots \dots \dots (2)$$

$$\frac{du(t)}{dt} = a(bv(t) - u(t)) \dots \dots \dots (3)$$

$$FAI: \frac{dv(t)}{dt} = 0.04v(t)^2 + 5v(t) + 140 - u(t) + \frac{K2}{Cm} \frac{dl(t)}{dt} \dots \dots \dots (4)$$

$$\frac{du(t)}{dt} = a(bv(t) - u(t)) \dots \dots \dots (5)$$

The auxiliary function is defined as followed:

$$\text{If } v \geq 30mv \begin{cases} v \leftarrow c \\ u \leftarrow u + d \end{cases} \dots \dots \dots (6)$$

Where a,b,c,d are neuron parameters, u is the membrane recovery variable, v is the membrane potential.

### 2) *In-vivo microneurography test*

The subject gave informed consent to participate in the microneurography recording, which was approved by the Liverpool John Moores University Research Ethics Committee.

To optimize and validate the predicted afferent neural signals, microneurography was carried out. We have found that the spiking features and the selective response property of the same type of tactile units located at fingertips are similar to each other according to our microneurography results and the literature [36-38]. Therefore, the response of a single SAI/FAI tactile unit was recorded and used for developing the integrated numerical model. The same subject involved in developing the FE hand was recruited again for microneurography. The subject was required to lie on a medical chair with the forearm restrained. A tungsten microelectrode (FHC Inc. Bowdoin, US) was inserted into the skin at the wrist and electrical stimulation was delivered through the electrode to roughly determine its position in relation to the median nerve (see Fig. 3(a)). After locating and entering the nerve, the electrode was adjusted manually to search for tactile units. The action potentials were amplified and visualized by Neuro Amp EX and physiological data analysis software LabChart (ADInstruments Ltd. Oxford, UK) respectively. The receptive field was stimulated by the rotatory tactile stimulator (RTS) (Dancer Design Inc. Merseyside, UK) with varying forces (ranging from 0.2 to 2.4N with an increment of 0.2N). The stimulator delivered a ‘sweep’ stimulus onto the marked receptive field of the afferent tactile fiber as are shown in Figure 3(b) and the corresponding FE simulation is presented in Figure 3(c). The locations of the SAI (yellow dot) and FAI (red dot) tactile units captured during microneurography are shown in Figure 3(d). The spiking rates were derived for each second, resulting in 121 data points for the SAI unit under five stimulating forces (0.6, 1.0, 1.4, 1.8, 2.4N) while 131 data points were obtained for the FAI unit under six stimulating forces (0.4, 0.8, 1.2, 1.6, 2.0, 2.4N). The firing rate was calculated by taking the average of the reciprocal inter-spike intervals (ISI):

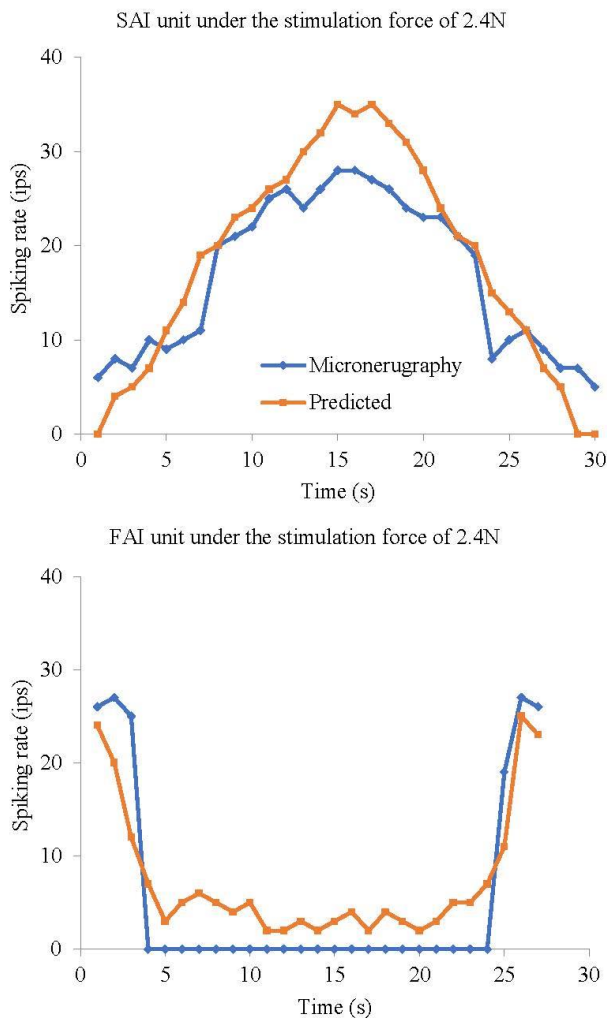


Fig. 6. The validation results for the single SAI and FAI tactile fiber. The predicted neural signals of SAI and FAI unit were compared with the results of microneurography.

295  $ISI_i = t_i - t_{i-1}$ ..... (7)

296  $ISI_i = \frac{1}{a-b} \sum_{i=b}^a ISI_i$ ..... (8)

297  $f = \frac{1}{ISI_d}$ ..... (9)

298 Where a-b= the number of ISIs.

299 3) Parameter optimization and validation for  
300 transduction and neural dynamic model based on the  
301 subject-specific microneurography data

302 The membrane current transduction and neural dynamic  
303 model were optimized against the results of the  
304 microneurography data by using the response surface  
305 method (RSM). Seven parameters in this integrated model  
306 were optimized against experimental results. Similar cross  
307 validation algorithm has been applied by other researchers  
308 to fit the parameters of neural dynamic model with  
309 experimental results [7].

310 The action potential signals under the stimulating force  
311 of 2.4N for SAI and FAI unit were separated for the  
312 validation (out-of-sample validation) while the rest of the  
313 data (Stimulating forces of 0.6, 1.0, 1.4 and 1.8N for SAI  
314 and 0.4, 0.8, 1.2, 1.6, 2.0 for FAI unit) were used to fit the  
315 computational model by using the RSM algorithm. The  
316 seven parameters:  $\alpha$ ,  $\gamma$ ,  $\lambda$  of the transduction model and a, b,

317 c, d of the Izhikevich model were optimized. The RSM  
318 algorithm aims to derive the specific combinations of these  
319 parameters which produce the best goodness of fit. (The  
320 fractional sum of squares (FSS, see equation 10.) between  
321 our subject-specific microneurography data and the  
322 predictions were minimized).

323  $FSS = 1 - \frac{\sum_{i=1}^n [(exp)_i - (pre)_i]^2}{\sum_{i=1}^n (exp)_i^2}$ ..... (10)

324 Where the *exp* stands for the microneurography test result,  
325 *pre* is the predictive result, n is the number of the data  
326 points.

327 The initial parameters values are  $\alpha = 2.46 \times$   
328  $10^{-5}$  mA,  $\gamma = 0.0046 Pa^{-1}$ ,  $\lambda = 506.74 Pa$ , a = 0.02  
329 Ohm, b = 0.2, c = -65mv, d = 6mv, these values are  
330 obtained from the literature [9, 39]. The procedure of  
331 parameter optimization was carried out in 4 steps. (a)  
332 Firstly, all the seven parameters were coded with specific  
333 increments less than two orders of magnitude of the initial  
334 values. (b) Secondly, all the parameters were increased or  
335 decreased for one increment and the FSS was derived for  
336 each trial resulting in totally  $2^7$  combinations. (c) Thirdly,  
337 the relationship between the optimized parameters and the  
338 FSSs was obtained through linear regression. (d) Fourthly,  
339 the magnitude and direction in which to optimize the  
340 parameters were determined by the combinations of the  
341 variation resulting in the largest increment of FSS. (e) Step  
342 (d) was repeated several times until the FSS was no longer  
343 increased. This optimizing procedure was conducted in  
344 Design Expert (Stat-Ease, Inc. US). After optimizing the  
345 parameters by using the RSM algorithm, the predicted  
346 neural signals of the integrated model achieved a good  
347 agreement with the results of microneurography in this  
348 study.

349 C. Predicting tactile signals of the population-level  
350 afferent neural fiber and its perception

351 1) The gradient sum algorithm and signal detection  
352 theory for relating the population-level neural activities  
353 with human perception

354 The psychophysical prediction is made by simulating the  
355 procedure of active touch during the discrimination test.  
356 The active touch was divided into two different  
357 procedures: 'dynamic ramp-up' and 'static hold', the  
358 former stands for the onset of the contact with an increased  
359 fingertip contact force and the latter represents the  
360 procedure of the stable contact with the object. The FE  
361 hand model was configured in a population density of 100  
362 and 144 receptors/ $cm^2$  for SAI and FAI units within the  
363 contact area of  $1cm^2$  on the fingertip, discriminating the  
364 convex surfaces with different radius of curvature (RC)  
365 ranging from RC8530mm to RC48.9mm. Active touch was  
366 simulated by using the FE hand with the muscle forces and  
367 kinematics captured during the *in-vivo* discriminating  
368 experiment. The neural activities of the afferent tactile  
369 fibers within the contact area were computed and the  
370 Gradient Sum method [7] was used to correlate the FE  
371 hand's population-level neural dynamic signals with the  
372 discrimination accuracy or the tactile perception. The  
373 Gradient Sum method transmits the parameters between  
374 receptors and derives the gradients of spiking rates or first

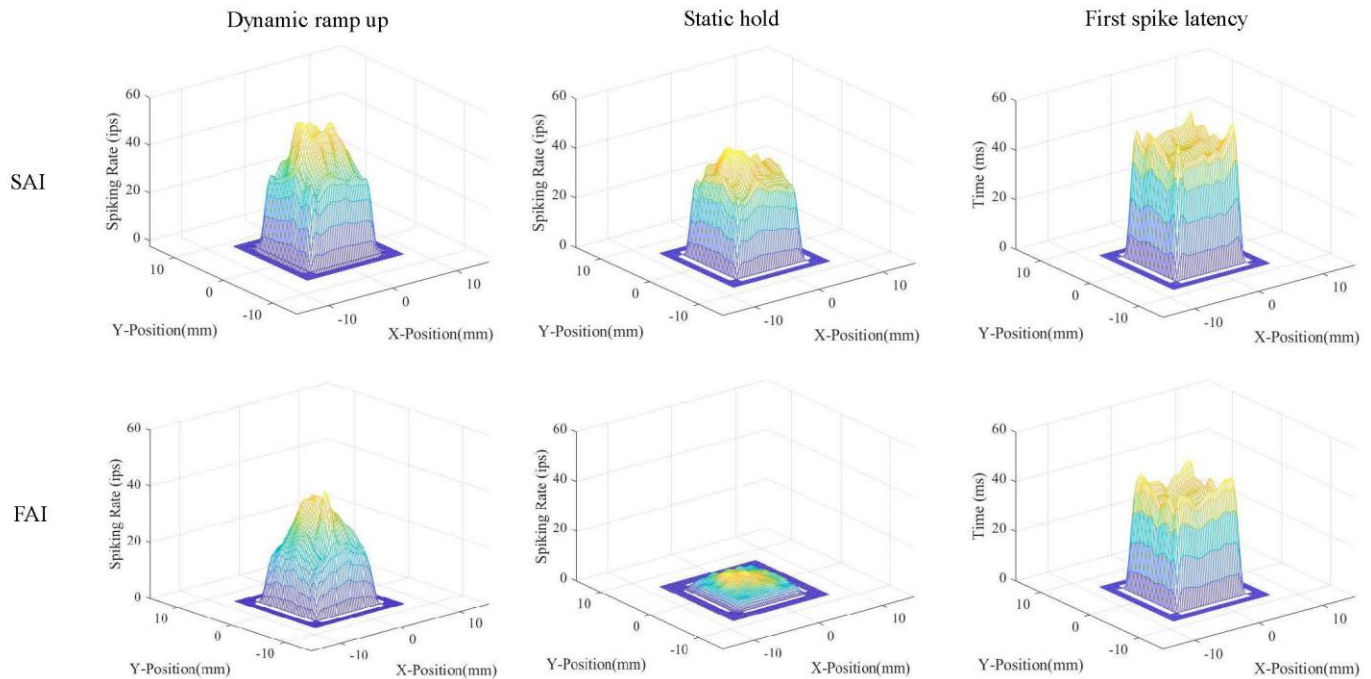


Fig. 7. Predicted neural activities of population-level SAI (first row) and FAI (second row) tactile units on index fingertip under the contact with the convex surface of RC77.7 mm. The horizontal axis stands for the locations of mechanoreceptors within the areas for extracting the SED, the vertical axis is the spiking rate or first spike latency. The active touch was divided into two separate stages including the ‘dynamic ramp-up’ and ‘static hold’.

375 spike latencies from adjacent elements. The procedure of  
 376 predicting the population-level tactile neural spike is  
 377 shown in Figure 4(a) First, random noises were added  
 378 through multiplying neural action potential and first spike  
 379 latency of all units in one convex surface by a pair of  
 380 random variables ( $\mu_1, \sigma_1$ ) with mean value  $\mu_1=1$  and the  
 381 standard deviation  $\sigma$  varied between 0.015 and 0.085. (b)  
 382 Second, the gradient sum of the elements is calculated by  
 383 summing all the parameter gradients around one single  
 384 element. 100 gradients were derived per convex surface  
 385 since 100 SAI mechanoreceptors (element) distributing  
 386 over  $1\text{cm}^2$  area was configured for each finger. All the  
 387 gradients were added as the gradient sum. (c) Third, steps  
 388 (a) to (b) are repeated 100 times for all the 7 convex  
 389 surfaces resulting in 700 gradient sums totally, each time  
 390 multiplying a new pair of ( $\mu_1, \sigma_1$ ). The corresponding 100  
 391 pairs of ( $\mu_2, \sigma_2$ ) are derived for each convex. (d) The signal  
 392 detection theory (SDT) was used to judge whether the FE  
 393 hand can differentiate the convex surface from the flat plate.  
 394 For example, two pairs of ( $\mu_2, \sigma_2$ ) are randomly selected  
 395 from RC8503mm convex surface and the flat plate as the  
 396 inputs to SDT with the  $\beta=0.5$ . Therefore, the hit rate (HR)  
 397 of convex surface RC8503mm is obtained. This procedure  
 398 is repeated for 100 times to derive the 100 HR for  
 399 discriminating convex surface RC8503mm. The hit rates  
 400 were calculated as below:

$$d' = \frac{\mu_s - \mu_n}{\sigma} \dots \dots \dots (11)$$

$$d' = \Phi^{-1}(H) - \Phi^{-1}(F) \dots \dots \dots (12)$$

$$\ln(\beta) = \frac{[\Phi^{-1}(F)]^2 - [\Phi^{-1}(H)]^2}{2} \dots \dots \dots (13)$$

404  $d'$  is the distance between the means of the signal and noise  
 405 in standard deviation unites.  $\mu_s$  and  $\mu_n$  are the mean values

406 of the signal and noise,  $\sigma$  stands for the standard deviation  
 407 of the noise.  $\beta$  is the criterion value and  $\Phi^{-1}$  is the inverse  
 408 ‘Phi’ function of the Z distribution, the detailed  
 409 information and calculation related to SDT can be found in  
 410 [40].

411 (e) Finally, the step (d) is repeated for the other 5 convex  
 412 surface and generates 500 HR. The ( $\mu_3, \sigma_3$ ) for each 100  
 413 HR of all the 6 convex surfaces are calculated. The  
 414 procedure of predicting population-level neural signals of  
 415 FAI units is the same with SAI.

416 2) *In-vivo discrimination test*

417 A psychophysical test of convex surface differentiation  
 418 was performed to validate the predicted population-level  
 419 afferent signals and study the neural coding mechanisms  
 420 under the active touch. The *in-vivo* discrimination test was  
 421 performed based on Goodwin’s research to determine the  
 422 discrimination ability of humans [41].

423 To perform the discrimination test of population-level  
 424 validation of SAI afferents, six convex surfaces with radius  
 425 of RC8503, RC532, RC179, RC106, RC77.7, RC48.9mm  
 426 and a flat plate ( $RC\infty$ ) were 3D printed. The same subject  
 427 of the FE human hand model was recruited for the  
 428 discrimination test. The capability of the subject to  
 429 discriminate surfaces during the procedure of active touch  
 430 was evaluated with 6 comparisons between different  
 431 convex surfaces and the flat plates conducted. The subject  
 432 was blindfolded and asked to sit at a table where the convex  
 433 surfaces were presented in pairs, either with the same or  
 434 different radius. The subject was required to judge whether  
 435 the convex surfaces were the same or not. Only the  
 436 fingertip of the index was allowed to touch the convex  
 437 surfaces and the finger was restricted from

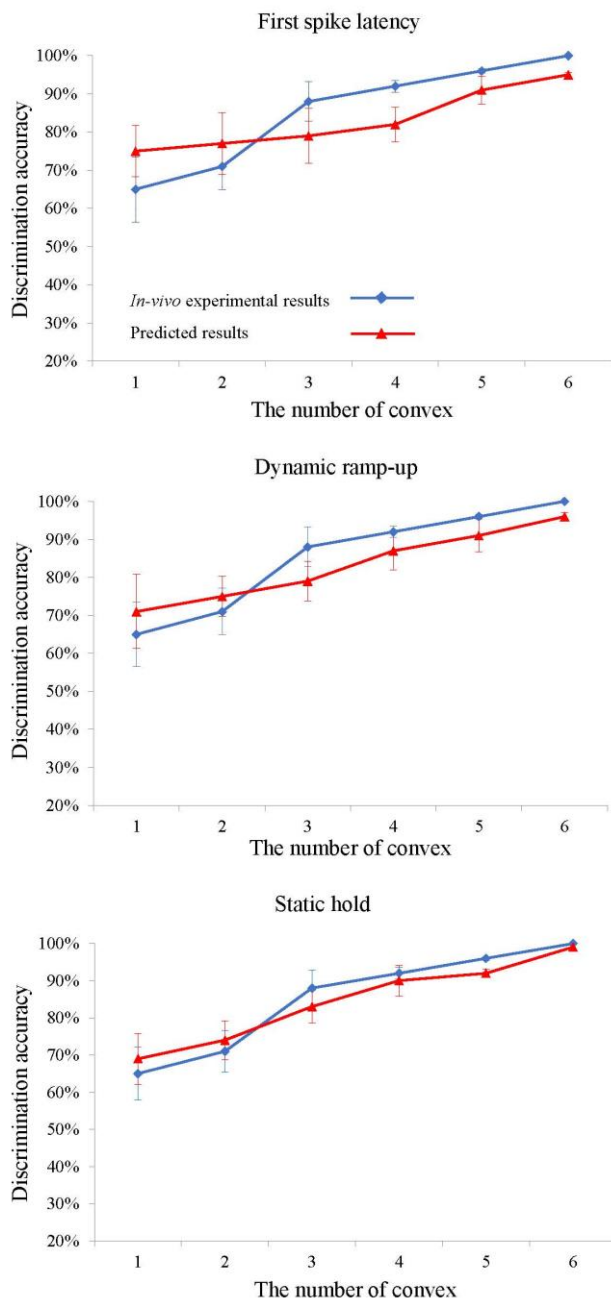


Fig. 8. The validation results of the population-level SAI tactile fibers. The predicted discrimination accuracy based on the afferent neural signals of SAI units were compared with the results of the *in-vivo* discrimination experiment.

438 adduction/abduction. The vertical distance between the  
 439 peak of the convex surfaces and the index fingertip was  
 440 kept the same, ensuring similar finger kinematics during  
 441 touching different convex to avoid the effect of the  
 442 proprioceptors located at finger joints. The test was carried  
 443 out in blocks, each block contained 12 comparisons (6 pairs  
 444 of flat-flat plate and 6 pairs of flat-convex, all convex  
 445 surfaces were presented in each session), and the pair of  
 446 surfaces varied randomly from block to block. In total, 30  
 447 blocks were performed, and the probability of detection  
 448 was calculated for each convex surface, the whole test was  
 449 repeated 6 times to achieve generality. Before the test, a  
 450 few practice blocks were performed to train the subjects  
 451 and ensure the reliability of the experimental results.

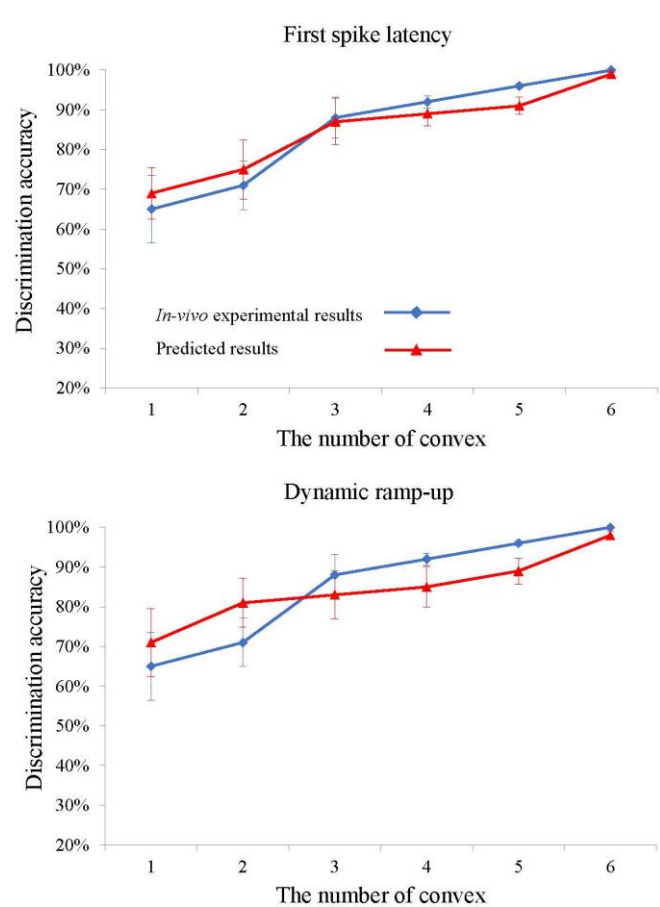


Fig. 9. The validation results of the population-level FAI tactile fibers. The predicted discrimination accuracy based on the afferent neural signals of FAI units were compared with the results of the *in-vivo* discrimination experiment.

452 During the discrimination test, the hand kinematics and  
 453 muscle forces were captured by using the Vicon system  
 454 (Oxford Metrics Ltd., Bilston, UK) and Delsys EMG  
 455 Trigno (Delsys Inc., Boston, US) respectively (see Fig.  
 456 5(a)). The muscle forces were estimated based on the  
 457 electromyography (EMG) signals. Before the  
 458 discrimination test, maximum voluntary contraction (MVC)  
 459 tests were carried out for each muscle using a Jamar  
 460 dynamometer. The recorded EMG data was band-pass  
 461 filtered (20–400 Hz) with a Butterworth filter and then  
 462 rectified. The muscle forces were computed based on the  
 463 maximum voluntary contraction forces. It was assumed  
 464 that a linear relationship between the EMG signal and  
 465 muscle force for isometric muscle contracting. Similar  
 466 methods have been used by other researchers to calculate  
 467 muscle forces under isometric contract [42–44]. These  
 468 kinematic data and muscle forces were applied onto the FE  
 469 human hand to simulate the discriminating experiment and  
 470 then made the prediction (see Fig. 5(b)). The active touch  
 471 procedure was divided into two steps: dynamic ramp-up of  
 472 the contact force and static hold (Static hold procedure is  
 473 not included in FAI validation since it only responds to  
 474 onset and offset of the stimulation).

475 The benchmark model 'TouchSim' [8] for predicting the  
 476 cutaneous neural response was employed to compare with  
 477 the performance of this multi-level numerical model. Only  
 478 passive stimuli could be simulated by using 'TouchSim'.



479 Therefore, the *in-vivo* discrimination test based on passive  
 480 stimuli was also conducted under the instruction of [41].  
 481 The discrimination accuracy achieved by ‘TouchSim’ was  
 482 then compared with the multi-level numerical model under  
 483 passive stimuli together with the *in-vivo* experimental  
 484 results in this study.

### 485 III. RESULTS

#### 486 A. Predicted tactile signals of the single afferent neural 487 fiber

488 The stress/strain related quantities including maximum  
 489 principal strain/stress, vertical strain etc. were correlated  
 490 with the results of microneurography and the quantity  
 491 achieving the best fit with the experimental results was  
 492 selected to be the input of the membrane current  
 493 transduction model. The stimulation onto the fingertip  
 494 during microneurography was simulated by using the FE  
 495 hand model. The strain energy density and other  
 496 stress/strain related mechanical quantities were obtained  
 497 under the stimulating force of 2N for the receptive field of  
 498 SAI and FAI unit. The spatial profiles of strain energy  
 499 density, maximum principal stress/strain and vertical stress  
 500 were compared with the microneurography results in Fig.  
 501 S2. A linear relationship between the neural action  
 502 potential level and mechanical quantities was assumed in  
 503 the form of:

$$504 \quad N_i = aS_i + b \dots \dots \dots (14)$$

505 Where  $N_i$  is the neural activation potential level and  $S_i$   
 506 stands for the simulated results. The constants a and b were  
 507 derived by maximizing the FSS (equation 10) between the  
 508 microneurography data and the predicted mechanical  
 509 quantities.

510 The FSS value of 1 means a perfect match between  
 511 predictions and experiment results. Predictions were made  
 512 based on twelve different stress/strain related quantities  
 513 (see Table. S1) and it was found that strain energy density  
 514 can provide the best fit with the FSS values of 0.92 and  
 515 0.69 for SAI and FAI unit, respectively. This conclusion is  
 516 in agreement with other researchers [22]. Therefore, the  
 517 strain energy density was used to correlate the skin  
 518 mechanics with neural activity for this research.

519 The original and optimized parameters of the  
 520 transduction and Izhikevich neural dynamic model were  
 521 presented in Table S2 and S3. Four and six iterations of  
 522 RSM were performed for SAI and FAI unit respectively,  
 523 resulting in the FSS values of 0.9377 and 0.8235.

524 The neural action potential level under the stimulating  
 525 force of 2.4N for SAI and FAI unit are used as  
 526 out-of-sample validation (see Fig. 6). The predicted and  
 527 experimental spiking rates are close to each other for both  
 528 SAI and FAI units. For the SAI unit, the predicted results  
 529 got a wider range of variation than the experimental results.  
 530 The FAI unit only responded to the ‘onset’ and ‘offset’ of  
 531 the stimulation during the microneurography test while for  
 532 the predicted results, the FAI unit still fired a few spikes at  
 533 the lower frequencies.

#### 534 B. Predicted tactile signals of the population-level 535 afferent neural fiber and its validation

536 The predicted spiking rates and first spike latency in  
 537 terms of the population-level afferent tactile units over the  
 538 finger pad were plotted and visualized in Figure 7. The  
 539 comparison between the predicted discrimination accuracy  
 540 and the *in-vivo* psychophysical experimental results is  
 541 presented in Figure 8 and 9. The active touch is divided  
 542 into two stages including the dynamic ramp-up of the  
 543 contact force and static hold of the finger.

544 It can be seen from Figure 8, the predicted  
 545 discrimination accuracy agreed well with the experimental  
 546 results. the convex with the curvature of RC8503, RC532,  
 547 RC179, RC106, RC77.7, RC48.9mm were numbered from  
 548 convex 1 to 6. The hit rates are all increased with the  
 549 curvature of the convex surfaces with regard to the first  
 550 spike latency and the two stages of the active touch. In the  
 551 case of the SAI unit, the predicted accuracies are larger  
 552 than those of the human subject for discriminating the  
 553 smaller curvatures (convex surface of RC8503, RC532mm  
 554 differentiated from the flat plate). Whereas the curvature  
 555 increases, the predicted accuracies are lower than the  
 556 subject’s (hit rate was close to 100%) for the convex  
 557 surface of RC77.7 and RC48.9mm. The predicted accuracy  
 558 during the static hold is closer to experimental results than  
 559 those in terms of the first spike latency and dynamic  
 560 ramp-up. The standard deviations for the predicted and  
 561 experimental results decrease with the curvature of the  
 562 convex.

563 Figure 9 shows the predictive accuracy and experimental  
 564 results for the FAI unit. The static hold is not included  
 565 since the FAI unit mainly responds to the dynamic  
 566 stimulation. In contrast to the SAI unit, the most accurate  
 567 prediction was achieved based on the first spike latency.  
 568 For the procedure of ‘Dynamic ramp-up’, the predicted  
 569 accuracies for discriminating convex surface with a small  
 570 radius are larger than the experimental results, while in the  
 571 case of discriminating convex surface with a larger radius  
 572 the predicted accuracies were smaller than the  
 573 experimental results. This is similar to the SAI unit. The  
 574 standard deviations for predicted and experimental results  
 575 are all decreased with the radius of the stimulator. The  
 576 discrimination accuracy predicted based on the uniformly  
 577 distributed receptive field of cutaneous neurons was  
 578 compared with that of heterogeneous one (See Fig. S3 and  
 579 S4). The results suggested that most of the discrimination  
 580 accuracy computed based on the tactile units with  
 581 heterogeneous receptive fields achieved a better agreement  
 582 with the human subject than the predicted results based on  
 583 the uniformly distributed receptive fields.

584 The discrimination accuracy achieved based on the  
 585 predicted afferent tactile signals through ‘TouchSim’ [8]  
 586 was compared with that using the multi-level numerical  
 587 model (See Fig. S5 and S6). The results showed that the  
 588 predicted neural signals through ‘TouchSim’ are consistent  
 589 with those based on the multi-level numerical model while  
 590 the predicted discrimination accuracy of ‘TouchSim’ is  
 591 slightly closer to the human subject than that of the  
 592 multi-level numerical model. However, these afferent

593 tactile signals were computed under the condition of  
594 passive stimuli, the skin mechanics under active touch is  
595 not accessible through ‘TouchSim’ [8]. Therefore, the  
596 multi-level model developed in this research achieved  
597 comparable performance with ‘TouchSim’ on predicting  
598 the afferent tactile signals under passive stimuli but with a  
599 further capability to obtain the cutaneous neural response  
600 evoked during active touch.

#### 601 IV. DISCUSSION

602 In this study an integrated numerical model was  
603 developed and validated for SAI and FAI afferent,  
604 combining the skin mechanics and neural dynamics to  
605 predict the single and population-level response of the 1<sup>st</sup>  
606 order cutaneous neurons. The model development was  
607 carried out on three levels: (A) on the skin mechanics level  
608 by using a subject-specific FE human hand model, (B)  
609 validation of the signals from single afferent fiber with the  
610 FSS of 0.94 and 0.82 for SAI and FAI unit respectively  
611 compared to the microneurography results, (C) the  
612 discrimination accuracies of two tactile units achieved the  
613 good agreement with the *in-vivo* discrimination test results.  
614 The model of population-level neural tactile SAI and FAI  
615 unit can differentiate the convex surface with RC8503mm  
616 from a flat plate.

617 The FE human hand served as the skin mechanics model  
618 so that the muscle forces and kinematics of active touch can  
619 be incorporated. The transduction mechanism between the  
620 afferent neural signal and neural activation level of the  
621 muscle synergy during active touch can also be  
622 investigated. Therefore, this integrated numerical model  
623 provides the possibility and push a further step to the  
624 explicit studying of sensorimotor mechanism compared  
625 with previous studies [9, 22, 45]. The realistic contact  
626 mechanism and anatomically intact human hand model  
627 provide the actual skin mechanics for predicting neural  
628 signals, rather than using the simplified continuum model  
629 or regression algorithm [8, 41, 46]. Also, this integrated  
630 model can help to predict reliable afferent cutaneous neural  
631 signals without the need to carry out microneurography or  
632 microsimulation as done previously [15-17, 47]. The  
633 subject-specific microneurography and *in-vivo*  
634 psychophysical experimental data with an integrated  
635 numerical model were employed to study the tactile neural  
636 coding and human perception. The predicted  
637 population-level 1<sup>st</sup> order neural signals under active tactile  
638 exploration suggest that different coding mechanisms  
639 might be applied for the afferent tactile signals elicited  
640 from different mechanoreceptors simultaneously.

641 Microneurography was performed on the subject of the  
642 FE hand model. Approximately 75% of the test results  
643 were applied for the optimization of the transduction and  
644 Izhikevich neural dynamic model, the other 25% of data  
645 was used for validation against the predicted results. For  
646 the validation of an SAI tactile unit the predicted firing  
647 rates varied more greatly than the experimental results, this  
648 may be due to the hyperplastic material properties defined  
649 for soft tissues in the FE model. The stress is sensitive to  
650 the strain variation resulting in large variations of SED and

651 membrane current. In the case of the FAI unit, the predicted  
652 firing rates agreed well with the microneurography results  
653 during the ‘onset’ and ‘offset’, achieving the FSS of 0.82  
654 for all the data points. However, when the RTS was  
655 sweeping over the receptive area of the FAI unit, the  
656 receptors gave no response with the neural action potential  
657 level of 0 spikes/second while the predicted spiking rate  
658 was maintained at approximately 20 spikes/second. It can  
659 be found from the neural dynamic model for the FAI unit  
660 (see equation 4), the firing rate depends on the derivative of  
661 the membrane current on the time domain. The SED varied  
662 slightly when the stimulator was sweeping over FE hand  
663 while this variation may initiate the drifting of the  
664 predicted membrane current.

665 The probabilistic psychophysical prediction was made  
666 by using the Gradient Sum method. The spiking rate or the  
667 first spike latency was transferred element by element  
668 throughout the population. Therefore, each convexity can  
669 be represented as a single number as the gradient sum. Here,  
670 the population responses during active touch were obtained  
671 and compared with the subject-specific discrimination  
672 results. The predicted discrimination results for both SAI  
673 and FAI units agreed well with the experimental results.  
674 During the *in-vivo* discrimination test, the convex surfaces  
675 with a small curvature like RC48.9mm is easy to be  
676 discriminated from flat plate for the human subject (from  
677 the subject’s personal feeling). Therefore, the experimental  
678 discrimination accuracies of population-level SAI and FAI  
679 units are smaller than the predicted ones for discriminating  
680 convex surfaces with small curvatures while in case of  
681 discriminating the convex surface with a large radius, the  
682 subject’s success rate became smaller than the simulated  
683 results. This might be affected by the subject’s human  
684 factor since a large number of comparisons need to be  
685 completed through the experiment. The two stages of  
686 active touch and the first spike latency are good candidates  
687 to make the prediction based on this multi-physics model.  
688 However, the static hold can provide the best fit for the  
689 human discrimination test results which means the  
690 perception may rely on rate coding for the signals from SAI  
691 units. Unlike the SAI units, perception may depend on the  
692 temporal coding of FAI afferents since the predicted  
693 accuracy based on first spike latency achieved the best  
694 agreement with the experimental results. These findings  
695 support the assumptions made by other researchers [48, 49]  
696 that humans may use multiple coding strategies  
697 simultaneously. The temporal coding may be used for fast  
698 identification of a stimulus and triggering the reactions  
699 while rate coding can represent the quantities of the  
700 stimulus. The similar perception was evoked based on the  
701 neural information conveyed by these two tactile afferents  
702 but relying on two different coding mechanisms,  
703 suggesting that different types of tactile neurons could be  
704 independent in haptic systems. The noise applied to the  
705 firing rates and first spike latency can affect the predicted  
706 accuracy, the effect was shown in Fig. S7. The simulation  
707 results have shown that the complex and heterogeneous  
708 distributed receptive field of cutaneous neurons help to  
709 enhance the discrimination accuracy compared with those  
710 under the uniform distribution. These larger and more

711 complex overlapped receptive fields with multiple ‘hotpots’  
712 or sensitive zones enable a higher spatial resolution which  
713 echoes the finding of other researchers [25]. However, the  
714 afferent branching mechanism through which the end  
715 organs of the cutaneous receptors are integrated to elicit the  
716 afferent neural signals is still unclear so far [29, 50]. More  
717 simulations on active touch could be conducted to study the  
718 effects of these heterogeneous receptive fields on human  
719 tactile performance after gaining a solid understanding of  
720 the branching mechanism of cutaneous receptors.

721 The discrimination accuracy archived based on the  
722 cutaneous neural responses predicted through this  
723 multi-level model was compared with that of ‘TouchSim’  
724 [8]. ‘TouchSim’ achieved a more human-like tactile  
725 performance than the multi-level numerical model based  
726 on the passive external stimuli. Despite the high computing  
727 efficiency and better performance of ‘TouchSim’ under  
728 passive stimuli [8], the multilevel numerical model  
729 developed in this study takes the 3D geometry of the  
730 human hand and the muscle-driven active touch into  
731 consideration while maintaining a comparable  
732 performance on predicting the afferent tactile signals with  
733 ‘TouchSim’.

734 This validated multi-level numerical model provides the  
735 possibility for pioneering research on human tactile  
736 sensing under the active touch and sensorimotor  
737 mechanism. For example, the relationship between  
738 population-level afferent signals and the neural activation  
739 level of muscle synergy could be explicitly summarized  
740 and applied to the control of bionic or prosthetic hand to  
741 restore the performance of the human hand [51, 52].  
742 However, the FE human hand model was involved in this  
743 numerical tool, resulting in the high computational cost.  
744 The surrogate modelling based on this FE model needs to  
745 be developed to reduce the computational cost and make it  
746 user-friendly to other researchers. Also, this multi-level  
747 numerical model can only predict the neural response of  
748 two type I tactile units. The convergence of the 1st order  
749 tactile signals from the ulna and median nerve and their  
750 post-processing were not included in this research. Future  
751 work can focus on simulating the responses of the two type  
752 II mechanoreceptors and the convergent mechanism of the  
753 population-level cutaneous neural signals transferred along  
754 different nerves.

755 V. CONCLUSION

756 The FE human hand model was combined with  
757 mechano-electrical transduction and neural dynamic model  
758 for predicting afferent tactile neural signals during active  
759 tactile exploration. The relationship between external  
760 stimuli and cutaneous neural activities was computed  
761 based on subject-specific microneurography data,  
762 approximately 75% of the test results was applied for the  
763 model optimization and another 25% was used for  
764 validation. Human perception during an active  
765 discriminating test was correlated with the population-level  
766 tactile neural signals achieving similar tactile  
767 discrimination abilities to the human subject. The predicted  
768 cutaneous neural signals under active touch suggest that

769 human perception during active touch exploration may  
770 simultaneously rely on different coding mechanisms for  
771 the neural signals elicited from different classes of  
772 cutaneous receptors. It was found that the heterogeneously  
773 distributed receptive fields may help to achieve a better  
774 sensing performance than the uniformly distributed ones.  
775 Comparable discrimination accuracies are observed  
776 between this multi-level numerical model and the  
777 published benchmark model [8], while the former presents  
778 the further capability of predicting the afferent neural  
779 response under the active touch. The 3D geometry of the  
780 finger pad and hand kinematics are also involved. This  
781 integrated numerical model provides a new concept to  
782 effectively study the human tactile seeing and sensorimotor  
783 mechanism under the active touch.

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791 CONFLICT OF INTEREST

792  
793 The authors declare that they have no conflicts of  
794 interest.

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