

A review of particle size analysis with X-ray CT

Julia G. Behnsen ^{1*}, Kate Black ¹, James E. Houghton ² and Richard H. Worden ^{2*}

¹ School of Engineering, University of Liverpool, Liverpool L69 3GH, United Kingdom

² Department of Earth, Ocean and Ecological Science, University of Liverpool, Liverpool L69 3GH, United Kingdom

* Correspondence: rworden@liverpool.ac.uk, julia.behnsen@liverpool.ac.uk

Abstract: Particle size and morphology analysis is a problem common to a wide range of applications, including additive manufacturing, geological and agricultural materials' characterisation, food manufacturing and pharmaceuticals. Here we review the use of microfocus X-ray computed tomography (X-ray CT) for particle analysis. We give an overview over different sample preparation methods, image processing protocols, the morphology parameters that can be determined, and types of materials that are suitable for analysis of particle size using X-ray CT. The main conclusion is that size and shape parameters can be determined for particles larger than approximately 2 to 3 μm , given adequate resolution of the X-ray CT setup. Particles composed of high atomic number materials ($Z > 40$) require careful sample preparation to ensure X-ray transmission. Problems occur when particles with a broad range of sizes are closely packed together, or when particles are fused (sintered or cemented). The use of X-ray CT for particle size analysis promises to become increasingly widespread, offering measurements of size, shape, and porosity of large numbers of particles within one X-ray CT scan.

Keywords: X-ray computed tomography; Particle size distribution; Particle shape measurements; Powder sample preparation

1. Introduction

Over the last 20 years (Figure 1a), more than 60 publications [1–61] have utilised microfocus X-ray computed tomography (also known as micro-CT, μX -ray CT, and XCT) for the analysis of particles in the range of micro- to millimetres. The applications derive from such diverse fields as additive manufacturing [8,19,21,23,28,31–35,37,40,43,45,46,52,58,61], granular packing studies [1,5,11,17,49,59,62], food processing [12,20,24], and pharmaceutical applications [10,51,55,57], because they all involve finely divided materials and benefit from particle size characterisation. The ease of sample preparation (section 2.1) and the amount of information available for each single particle (section 2.5) are other reasons for the breadth of use of X-ray CT. The 3D size, morphology, internal porosity, and the position of a given particle in the granular assembly are types of information that are available from a single scan (Figure 2). Due to the non-destructive nature of X-ray CT imaging, repeated scans of the same sample after an intervention such as loading [11,16,49,56] or heating [3] are possible and allow for time-lapse (4D) studies of changes in the assembly [53]. The digital data, collected with each scan, can feed directly into computed models about the particles and their behaviour in the granular assembly [27,47,48,54]. After early use of synchrotron beam lines [1,3,6,7,14,28,33,34,46], the emergence of laboratory X-ray CT instruments [2,4,8–13,18,20–27,30–32,36–45,47–52,54,55,57–60] has made the technique more widely accessible (Figure 1b).

This review summarises studies that have utilised X-ray CT for particle size (and morphology) quantification. In this context, a particle is a small (micro- to millimetre scale) rigid body. The distribution of particle properties, such as size and shape over a large number of similar particles, rather than the properties of a specific single particle,

Citation: Behnsen, J.G.; Black, K.; Houghton, J.E.; Worden, R.H. A review of particle size analysis with X-ray CT. *Materials* **2022**, *1*, 0. <https://doi.org/>

Received:

Accepted:

Published:

Publisher's Note: MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.

Copyright: © 2023 by the authors. Submitted to *Materials* for possible open access publication under the terms and conditions of the Creative Commons Attribution (CC BY) license (<https://creativecommons.org/licenses/by/4.0/>).

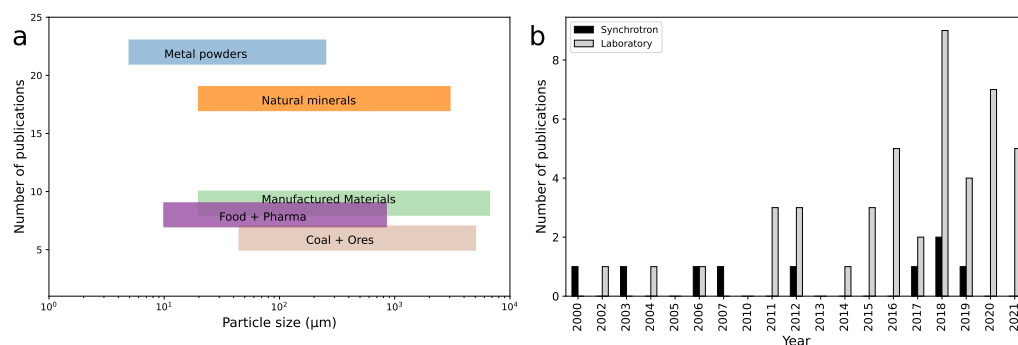


Figure 1. Diagrams summarising the history of use of X-ray CT for particle size characterisation. (a) The number of publications for different material categories. The category “natural minerals” contains studies that used naturally occurring minerals, such as naturally occurring sand [6,11,14,27,49,56,59] or crushed granite [42], while the category “manufactured materials” contains purposefully made particles, such as beads made from glass [1], acrylic [5], gypsum [17], or ceramic [39]. The particle size ranges measured within each category are shown on the x-axis. (b) The number of publications utilising particle size characterisation with X-ray CT since the year 2000, split into use of synchrotron vs. laboratory X-ray sources.

is typically of interest to the analysis. In different research fields, individual particles might also be called grains; similarly, a collection of particles may be known as a granular assembly, a powder, or bulk material. We will refer to “loose particles” for a collection of particles that have no strong binding forces or adhesion between them and will flow freely if not constrained in a container. To be clear, terms such as grain size analysis or powder analysis are equally used for the same methodology in different scientific disciplines.

Reviews of the general use of X-ray CT for the broad field of materials research [63], and specifically additive manufacturing [64,65], have recently been published, but these did not focus on particle characterisation. A detailed description of the experimental approach to particle size analysis that was employed by a single laboratory is available [52], but it excludes methods used at other institutions. The use of X-ray CT for the time-lapse study of particulate systems has also been recently published [53], but omitted the basic characterisation of the loose particles, which is our focus here.

The aim of this review is to address particle characterisation using X-ray CT, answering the following specific questions:

- What materials and particle sizes have been analysed with this method?
- What are the options for sample preparation, and are they influenced by the particles to be measured?
- What influence does the image processing methodology have on the results?
- Where are the limits of the method in terms of material suitability and particle size range?

We intend that this review will serve as a guide for researchers and others new to particle analysis with X-ray CT, who are considering using this method for their own samples. A further objective of this review is to develop a common language related to particle size analysis that can be adopted across different disciplines.

1.1. History of particle analysis with X-ray CT

X-ray computed tomography, the method of taking a series of X-ray projection images around the object of interest, and computing a tomographic dataset (a 3D image) from the result, has become a major diagnostic tool since the first commercial medical scanner was built in 1973 [67]. Since then, the development of industrial scanners [68] and improvements to microfocus X-ray sources and detectors to enable micron and submicron-range resolution [69,70] (often termed micro-CT) opened the door to characterise a wide range of materials, including particles of the μm to mm range.

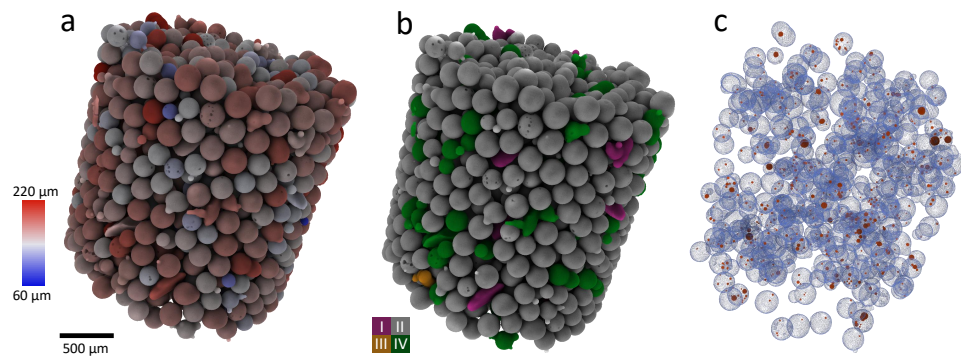


Figure 2. Micrometre-size glass bead quantification with X-ray CT. (a) Glass beads coloured according to size from blue ($60\ \mu\text{m}$) to red ($220\ \mu\text{m}$). (b) The same glass beads coloured according to Zingg's [66] shape classification (discs (I): purple, spheres (II) grey, blades (III): orange, rods (IV): green). (c) Only beads with internal pores shown (beads in blue, pores in red).

A simple schematic diagram of the X-ray CT data acquisition system is presented in Figure 3. More comprehensive descriptions are available elsewhere [63,68], but a brief summary is included here. In laboratory X-ray CT instruments, typically a sample is positioned upright between the microfocus X-ray source, and the detector. The X-ray source usually allows variation of the maximum energy of the X-ray beam, with common maximum energies up to 225 keV. Beam filters can be used to remove the low-energy component of the X-ray spectrum and achieve a higher relative transmission through the sample. The X-ray beam is transmitted through the sample and attenuated by the materials that compose it. The attenuation of the beam is revealed in the intensity distribution recorded by the detector for each projection image. The detector consists of a scintillator, and a photon counting device. Flat panel detectors are most commonly used, but some high-resolution instruments utilise multiple objectives with different optical magnification instead (typically called X-ray microscopes). A series of projection images are captured while rotating the sample. While a rotation of 180° is sufficient for parallel-beam geometries, such as in synchrotrons, cone-beam laboratory instruments generally require a rotation over 360° [71]. The projection images are converted into a stack of slice images by a reconstruction algorithm, typically a variation of the FDK-algorithm for divergent (cone) beam systems [72]. The study of small particles with X-ray CT started in 2000, when the individual positions of $63\ \mu\text{m}$ diameter glass beads were determined at beamline 20-ID at the Advanced Photon Source, USA, to study 3D granular packing [1]. In the first decade of the millennium, approximately half of the published studies were undertaken at synchrotron beamlines; however, the increasing availability of laboratory-based X-ray CT instruments has meant that, in the last 10 years, 90% of the published studies were carried out using laboratory systems (Figure 1b). Laboratory-based X-ray CT systems are typically easier to use and timelier to access than synchrotron beamlines, and they are also easily available for commercial companies to carry out their own testing, which is an advantage for regular quality control of, for example, manufacturing feedstocks, products or food powders.

1.2. Summary of materials examined

X-ray CT methods are suitable for a broad range of materials, and a summary of those particles characterised with this method is given in Figure 1a. The characterisation of metal powders is of great interest for powder-based additive manufacturing (AM) processes, where powder properties such as particle size distribution and particle shape affect the flow and spreadability of the powder [73]. Imperfections, such as pores inside powder particles, or contamination of the powder with particles of a different material, are also of great interest since they can affect the strength of the final build-part [74]. Metal powders analysed by X-ray CT, of interest to the AM industry, include titanium alloys

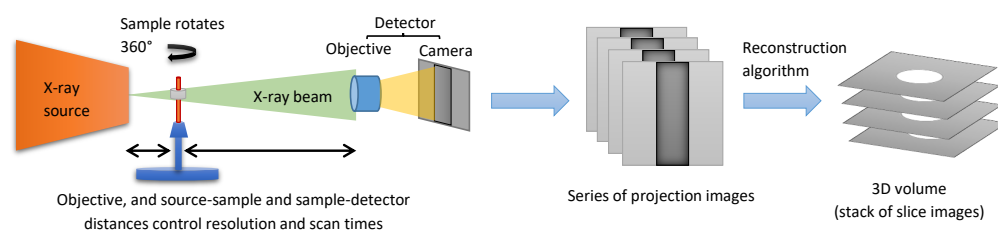


Figure 3. Schematic of a typical laboratory microfocus X-ray CT acquisition system, showing the source, sample with sample holder, and flat-detector. Source-sample, and sample-detector distances affect image magnification in addition to the objective. A series of projection images is captured while rotating the sample, commonly over 360° , which is then reconstructed into the slice images that form the 3D data volume.

[8,21,28,31,33,34,46,52,58,64], steels [40,43,46,61] and nickel-based alloy [37]. These studies aimed to evaluate the quality and suitability of a powder, for example after several rounds of recycling, or of powder particles made by different production processes [8,34,37]. Other objectives have included understanding if the porosity inside the powder particles transfers into the build part, or how particles change during sintering [3] or compaction [16]. X-ray tomography has been used to study geological material, mainly quartz-rich sand [9,11,13,18,49,50,56], but also ores and coal [4,7,25,38,48]. A field of interest is the behaviour of sand particles during deformation [11,13,36,49,53,56]. Other studies have been concerned with the development of image processing methods to aid with the identification, description, and tracking of particles during deformation [6,44], and often use a specific reference material, such as Caicos ooids [36], ceramic proppant [39], or industrially-made zeolite particles [44]. Related is the analysis of granular assemblies to describe pore networks and grain contacts [15,17,59]. Another field of research is the development of digital models of sand grains to virtually study particle breakage or failure modes [27,47,48]. Granulated organic materials, including foods, such as milk powder [12] or maltodextrin [24], pesticide-containing dust from seeds [20] and pharmaceutical powders (lactose, [51], hexamine [57], L-glutamic acid [55], acetylsalicyl acid [10]) have also been studied using X-ray CT.

1.3. Particle size ranges

Along with different material size classes, Figure 1a also shows the particle size ranges that have been studied. The smallest particle sizes analysed involve studies of metal powder, with successful analysis of particles as small as $5\ \mu\text{m}$ to $25\ \mu\text{m}$ [40]. However, it was noted that shape analysis of the smallest particles was not possible with the employed X-ray CT setup, which had a voxel (a 3D pixel) size of $2.9\ \mu\text{m}$. The largest particles studied that are included in this review are in the centimetre range [25,75]. Only a few dozen large particles fit the field of view at higher resolution, but scans of small particles, such as in metal powders, typically contain tens of thousands of particles; multiple scans along a sample can detail over 100,000 particles [19]. Most studies have been of spherical or equiaxial particles (e.g., sand grains). Needle or disk-shape particles have not been extensively examined, although dust particles, with more complex shapes, have been scanned [20], and irregular agglomerates resulting from spray fluidisation have been analysed [24]. As well as characterising the particle size and morphology, the internal porosity of particles has also been examined [21,23,58] (Figure 2c).

2. Scanning protocol for particle size analysis

Figure 4 illustrates the steps taken to analyse particles with X-ray CT. Several variations of the individual steps have been employed; they will be compared and discussed in this section.

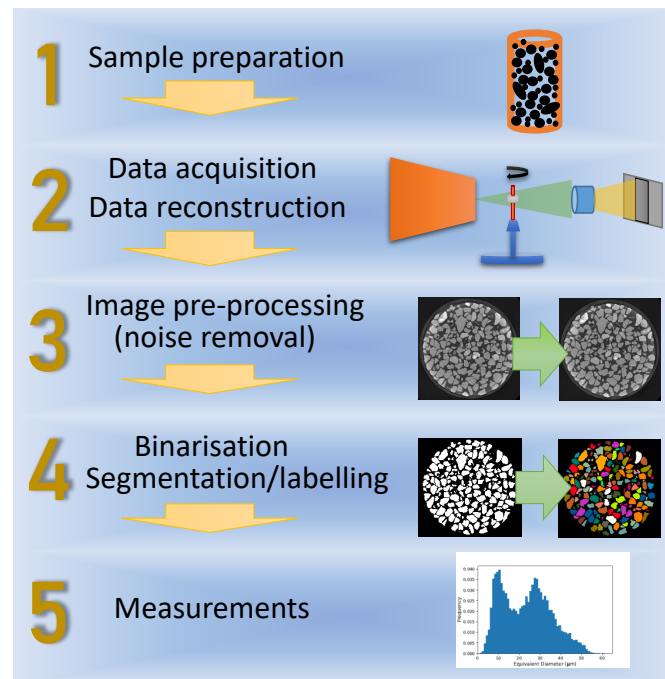


Figure 4. Generalised scanning and analysis workflow for particle characterisation with X-ray CT. After sample preparation (section 2.1), the X-ray CT data are acquired and reconstructed. The resulting greyscale data are usually pre-processed, for example for noise smoothing, before further processing. To enable quantification, each particle must be segmented (or labelled) individually (section 2.4), which typically follows a general binarisation step that separates all particles from the surrounding medium. Once segmented, individual particle size and shape parameters can be determined (section 2.5).

2.1. Step 1: Sample preparation

In a typical laboratory X-ray CT scanner, the ideal sample is cylindrical and positioned upright with the base securely fixed (Figure 3). To enable scanning of powders, the loose particles must be held in a form that is compatible with this geometry. Four common sample preparation methods, discussed below, are illustrated in Figure 5.

The simplest preparation method is to pour loose particles into a capillary, or similar cylindrical container (Figure 5a) [8,20,21,35,51,55]. The diameter of the capillary is adjusted to the particle size to ensure enough particles are in the field of view. Both full field of view (full diameter of the capillary) and scans of an internal region of the capillary are possible to further adjust the resolution. This method is suitable for a large range of materials, additional steps at the image processing stage typically are later needed to separate the touching particles into individual ones (see section 2.4).

To avoid the need to separate the particles with image processing steps, particles have also been dispersed in a containing medium at the sample preparation stage. One method is to mix the powder with a viscous epoxy and let this cure either inside a capillary (Figure 5b) [7,19,31–33,43,52,58,61] or as a block, which can then be cored (Figure 5d) [18,23]. The downside of this method is that it takes longer to prepare the sample than pouring loose material into a capillary and it is not suitable for all materials (e.g., carbon-based materials such as pharmaceuticals) due to low contrast with the epoxy, or even a possible chemical reaction between the sample and the epoxy. Size segregation, for example by preferential settling of large particles during curing, is a concern, and it has been proposed that the epoxy plus powder mixture in the capillary should be agitated by shaking until the epoxy has set [29]. Furthermore it is not easy to discern if mixing with epoxy has actually separated all particles, or if small agglomerates have been adhered together. Because of this particle

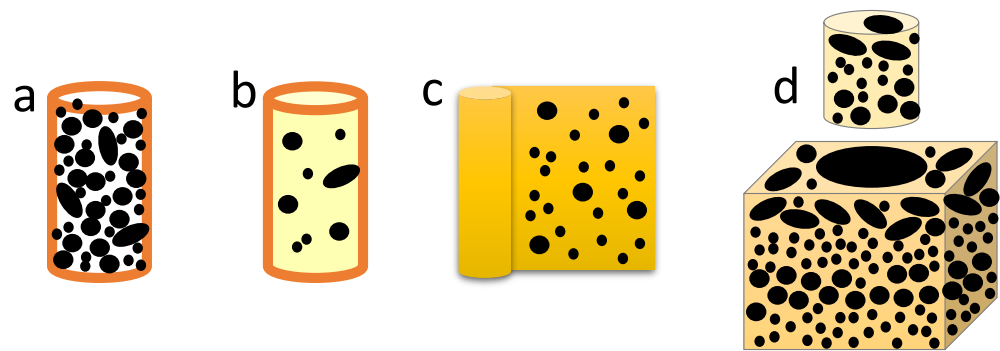


Figure 5. Sample preparation methods for loose particles. (a) Particles can be poured into a capillary. (b) Particles can be mixed with epoxy and cured inside a capillary. (c) Particles can be sprayed onto adhesive material such as wax or adhesive tape, and rolled into a cylinder. (d) Larger assemblies of particles can be infused with resin and then cored to obtain a smaller cylindrical sample.

agglomeration, there might still be a need to subsequently separate particles digitally in the dataset. Alternatively, even though the agglomerates might be of interest in the characterisation, they can be excluded from quantification out of caution [40].

A different way of dispersing the particles is to spray them as a thin layer on a flat adhesive material, such as adhesive tape [40] or wax [37], which can then be rolled into a cylindrical shape for scanning (Figure 5c). The downsides of this method are like those due to mixing with epoxy, in that contrast might be low and an even distribution of particles on the material cannot easily be ascertained.

For samples in which particle arrangement needs to be preserved, a way of preparing samples is to impregnate a larger core or sample with resin, and then use a small core drill to extract samples with a diameter suitable for scanning [18]. Such an approach has the advantage of leaving the grains in their natural position, so that features such as grading of sand grains can be studied (Figure 5d).

A special case involves studies that place high priority on accurate shape description, such as those working on particle modelling. In such cases, individual particles are typically spaced manually inside a larger container, and supported in a high-viscosity matrix, for example silicon oil [26,42,54].

2.2. Step 2: Data acquisition and reconstruction

X-ray CT data acquisition parameters, such as source energy and image exposure times, depend on the specific instrument, and a comparison is not very informative. Of the 62 studies surveyed in this review, 29 included laboratory X-ray source energy parameters. There was a wide range of source accelerating voltages, for example, quartz sand and glass containing samples were scanned at accelerating voltages between 25 kV and 150 kV. Exposure times for the projection images, which are dependent on the detector sensitivity, the source parameters, the sample attenuation, and the source-detector distance, are largely not available in the methods descriptions. In general, it must be assumed that scan data acquisition and reconstruction were carried out with settings that ensure good quality data [68]. Apart from the capabilities of the instrument, consideration must be given to the sample material composition and attenuation, the sample size, and the resolution required to image the particles. These parameters are discussed in more detail in section 3.2 and section 3.1 below.

2.3. Step 3: Image pre-processing

As image noise is an inherent feature of X-ray CT images [76], a noise-smoothing filter is typically applied as a first step. Smoothing of images not only suppresses localised deviations in brightness, which could be noise, but also sharpens peaks in the histogram, which helps with image segmentation [77]. Due to low computational costs, and wide

implementation in image processing software, many authors apply simple median or Gaussian filters [23,24,32]. However, as those filters tend to blur edges, other researchers have employed bilateral [46] or non-local means filters [51,55], which have become more usable for large datasets with increasing computer performance. Instead of using an image-smoothing filter, some authors prefer to set a minimum voxel or volume cut-off limit to remove the smallest artefacts before quantification [52,58].

2.4. Step 4: Image binarisation and segmentation

Before quantification of particle size and shape is possible, the borders of each particle in the dataset must be identified and the particle given an individual number in a process called segmentation or labelling. The process usually begins with binarising the image into particles and background (which might be air or a surrounding medium such as epoxy), followed by separation and labelling of individual particles. For binarisation, typically a simple greyscale threshold is set or found with an algorithm such as Otsu's method [78]. Thresholding can be difficult if there is a strong variation in brightness across the image or between particles, in which case a machine learning tool such as the trainable WEKA segmentation tool implemented in ImageJ [79] might provide better results [22]. If the particles are physically separate, such as when intentionally spaced apart, or separated by another medium such as epoxy, they can be labelled directly from the binary image by cluster detection [29]. However, in cases where particles are touching, such as when loose particles have been scanned in a capillary, particle boundaries fall below the resolution limit, and the particles may appear to be merged. An underlying assumption must be made that the particles are indeed separate and are not fused or cemented together. In these cases, additional image processing methods need to be employed to separate them into individual particles. The challenge is to find particle boundaries that preserve the actual shape of the particles, without breaking single particles into multiple ones, or merging multiple particles together. A common approach is to use a distance transform-based

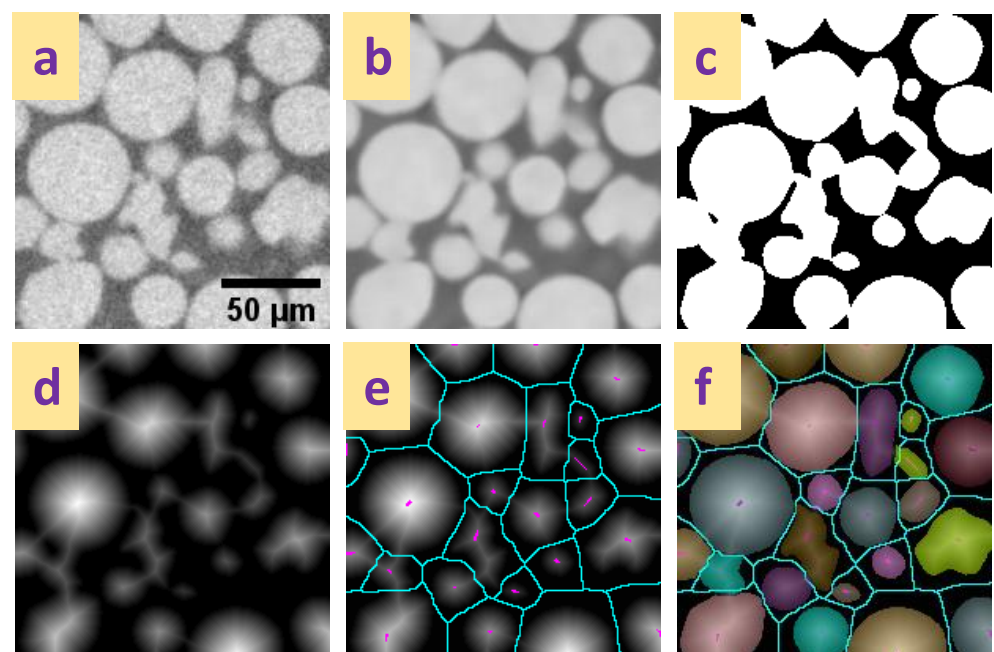


Figure 6. Particle separation process with a distance-transform watershed method. (a) Unprocessed image, (b) smoothed image (non-local means filter), and (c) binarised image, (d) distance-transform of the binary image shown in Figure 6c, (e) distance transform with the extended maxima markers (purple) and watershed lines (blue) shown, (f) segmented particles resulting from re-flooding the image from the markers to the boundaries of the binary mask image and the watershed lines.

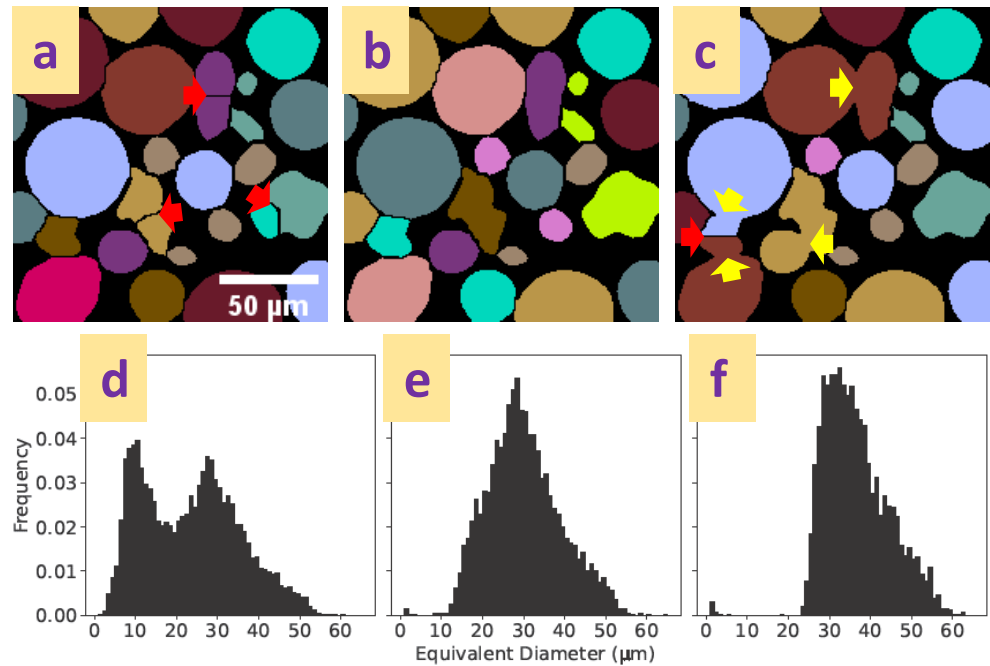


Figure 7. Segmentation errors and their effect on the particle size distribution of a copper powder with a manufacturer’s size range of 15–45 μm . Top row: (a) over-segmentation with increased splitting of particles (red arrows), (b) visually correct segmentation, (c) under-segmentation with increased merging of particles (yellow arrows). Segmentation differences are a result of varying the extrema marker extend (Figure 6e) during the watershed process. Segmentation with the open-source ImageJ plugin MorphoLibJ [82]. Bottom row: Particle size distributions for the full datasets: (d) 8800 particles (e) 5700 particles, (f) 3300 particles) resulting from the segmentations shown in top row a, b, and c.

watershed to separate particles, illustrated in Figure 6. A distance map of the particle phase is calculated by successive erosion of the border of particles, the centres of the particles identified and labelled as markers, and the final label image created by re-flooding the binary image by a watershed process [77,80]. While this approach works very well for spherical, equant particles, complex particle shapes present additional challenges. For example, the erosion process of complex particle shapes often leads to multiple central spots, which, if uncorrected, result in over-segmentation by splitting whole irregular particles into multiple parts. A range of approaches exist to correct the marker image, for example by eliminating weak markers with an h-extrema filter [81] or by stopping the erosion early [60]. Removing too many markers results in under-segmentation and the artificial merging of separate particles. Figure 7 illustrates over- and under-segmentation, and the resulting particle size distributions. As can be seen, care must be taken to choose appropriate watershed parameters, and human supervision of the process is recommended. Unsupervised algorithms can be used to evaluate the segmentation if a particular particle shape is expected and can be used as a quality marker [39].

2.5. Step 5: Measurements and quantification

Once particles have been separated in a satisfactory way, each particle can be measured. Table 1 presents an overview of the most commonly employed size and shape parameters to describe particles.

While each particle is originally represented by a cluster of voxels in the segmented 3D data set, it can be advantageous for data storage demands and processing speeds to approximate the particle surface with either a triangular surface mesh [83] or with a series of spherical harmonics (SH) functions [2,27]. Approximating the particle surface in either of those ways

also introduces a degree of surface smoothing, which can help deal with unrealistic effects of surface voxelisation. However, it is difficult to use SH functions to describe particles with more complex shapes, for example, when the centre of gravity lies outside of the particle [52]. Most morphological parameters can be calculated directly from the voxelised representation, though it can be faster to calculate them from the mesh or SH approximation of the particle. Table 1 list the alternative approaches to calculate each measure. Currently, no agreement over the best approach exists, and various software solutions implement one or more of the methods. While, in general, results from different approaches should be similar, small deviations of results exist due to the different approximations employed, which might limit the usefulness of specific approaches [46]. This especially affects surface area measurements. Simply counting the faces of the surface voxels usually leads to over-estimation of the surface area, and approximation approaches with surfaces meshes, SH functions, or algebraic estimation [84,85] give more realistic results [86].

The 3D data allows the measurement of the length (L), width (W), and breadth (B), also called depth or thickness, of each particle, which again can be found in multiple ways, but most commonly by determining the principal axes of the inertia tensor and computing the moments of inertia (with mass represented by voxel intensity) [87]. Knowing the three dimensions L, W, and B, can improve the comparison with other particle measurement methods; for example, one study found that the width of a particle correlated well with sieve analysis data, while the length correlated well with laser diffraction data [7]. The dimensions also allow calculation of the aspect ratios, which can be used to classify the particles, for example by the four Zingg classes [66] of discs, spheres, blades, and rods (Figure 2b).

Apart from the morphological parameters mentioned in Table 1, many other parameters can be calculated; for example, particle projections at different angles [52] can be directly compared with 2D measurements, e.g., from microscopy images. Careful analysis of the surface curvature allows for determination of particle roundness in 3D [26,42,75], which is more difficult than in 2D [88], and thus not commonly implemented in analysis software. In addition to measuring each particle, properties of the granular assembly, such as the packing density or bulk porosity can also be quantified, if the sample was prepared in a bulk state (and not diluted by, for example, epoxy).

Resulting measurement data is usually presented in tabular form or summarised statistically. However, it is often also possible to visualise results by combining them graphically with image data, for example as colour coding of the original 3D data (Figure 2).

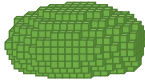

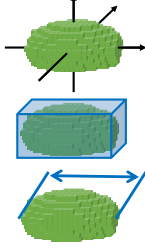
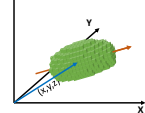
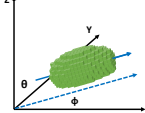


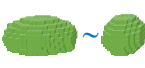
3. Outlook and limits of the method

After here summarising the range of work already undertaken, two research questions with regards to the limits of particle characterisation by X-ray CT will be subsequently discussed. Following the development of sub-micrometre commercial X-ray CT systems, the first question concerns the smallest particle size that can be successfully characterised using laboratory equipment. The second question concerns the types of materials that can be used for powder analysis using X-ray CT, especially regarding highly X-ray attenuating materials.

3.1. Limits of particle size and resolution

Currently the highest resolving commercial X-ray CT systems advertise a sub-micrometre resolution, as small as 0.5 micrometres. This limit results from hardware parameters, such as the the source spot size and the physical detector resolution [68]. The definition of 3D spatial resolution in X-ray CT is complicated, and a topic of current debate [96]. The 2D resolution of each projection can be measured with resolution targets such as the JIMA (Japan Inspection Instruments Manufacturers' Association) chart [97] or by evaluation of the modulation transfer function [98]. However, the true 3D resolution can vary from scan to scan due to additional factors such as the number of projections, the reconstruction

Table 1. Overview of common particle size measures, and their methods of calculation from the digital image data. The same measure can often be calculated in multiple ways, as listed in the right-hand column. SH refers to approximating the particle surface with spherical harmonics functions.

Sketch	Measure	Methods of calculation
	Volume	Counting of all voxels belonging to a particle [89], integral over SH functions [87], integral over the surface covered by a mesh [90].
	Surface Area	Counting all faces of surface voxels, estimation of the surface area [84,85], measuring a surface mesh (marching cubes [90]), or calculate from the SH functions [87].
	Three dimensions of the particle – length (L), width (W), and breadth (B) (also called depth or thickness). These are mutually orthogonal and $L \geq W \geq B$	Derived from the moments of inertia (with mass represented by voxel intensity) [52,87], edge length of the smallest box that contains the particle [91,92], searching the SH parameters [52], or by calculating length as the maximum Feret [93] or caliper diameter, the maximum distance between two tangential planes of the particle surface and finding W and B orthogonally [94].
	Position of the particle within the data set	Centroid (centre of mass) position [89], as the origin of a square box containing the particle, or as the first point of the particle encountered in searching direction.
	Orientation of principal axes, ϕ , θ	Principal axis orientation derived from moments of inertia (or volume) tensor [87].
	Local Thickness	The diameter of the largest sphere that fits inside the particle at a local point. [95]. The local thickness differs from the total thickness especially in cases of porous or cup-shaped particles.
	Equivalent Diameter of a sphere of the same volume as the particle	Derived measure from volume (V): Equivalent diameter $= \sqrt[3]{6V/\pi}$
	Sphericity measures between 0 and 1, and shows how closely the shape matches a perfect sphere	Derived measure from volume (V) and surface area (A): Sphericity $= \sqrt[3]{(36\pi V^2)/A}$

algorithm, the complex energy spectrum and the sample shape relationship. Standardised measurement test samples (phantoms) and defining standards for 3D resolution are under active development [96]. In the following section, it is assumed that the approximate highest resolution is $0.5 \mu\text{m}$. It should be noted that in most X-ray CT systems the pixel size (and resulting voxel size) does not equal the spatial resolution of the system at the current conditions. Firstly, it is often possible to decrease the pixel size significantly to below the current spatial resolution by increasing the magnification (oversampling). Secondly, according to the Nyquist-Shannon sampling theorem, the sampling rate must be at least twice as high as the signal, which means at least two pixels are needed to detect a feature. For example, to achieve a spatial resolution of $0.5 \mu\text{m}$, a pixel size of at least $0.25 \mu\text{m}$ should be used.

To characterise loose particles, three conditions must be met: the particle must be observable over the resolution limit, it must be separate from neighbouring particles, and it must be made up of enough voxels to describe its size and shape.

Fewer voxels are needed if the absorption contrast to the surrounding medium is high and only the general position needs to be determined. In the case of spaced-apart particles, two voxels are enough to identify a particle. With more densely packed particles, this identification is more difficult, because the size of gaps between the particles typically becomes the limiting factor. This is especially true in case of spherical particles, where the convex shape reduces the gap between particles to less than the resolution limit. In such cases, enough of the particle must be without surface contact to be able to separate it from its neighbours by e.g., a watershed process (section 2.4). Broad particle size distributions (e.g., in poorly sorted samples), where smaller particles fill the gap between larger ones, make this separation even more challenging.

It is easily understandable that more voxels per particle result in a more accurate shape description, but the question is how few voxels could be considered to be enough? In practice, often a voxel, or volume, cut-off limit is defined, under which particles are not further evaluated, even though this can affect the resulting particle size distribution. 512 voxels are commonly used for particles separated in epoxy [52], which is an $8 \times 8 \times 8$ cube, or a sphere with a diameter of 10 voxels. Other studies have used a much lower limit, such as 8 or 10 voxels [37,45]. Assuming a sub-micrometre resolution X-ray CT system, an approximate smallest voxel size at the highest resolution is approximately 0.2 to $0.3 \mu\text{m}$. Using the 512 voxel cut-off limit, this means the smallest characterisable particle size is approximately 2 to $3 \mu\text{m}$. However, calculating the average amount of voxels across the smallest particles, in our survey of published research [1–61], has revealed that typically approximately 25 voxels are used, which equates to the smallest characterisable particle size being $5 \mu\text{m}$. A small voxel size necessitates a similarly small field of view (of e.g., $500 \times 500 \mu\text{m}$ for a $0.25 \mu\text{m}$ voxel size with a 2000×2000 pixel detector), and very high-resolution scans might not be feasible if the sample size cannot be sufficiently reduced, or if insufficient numbers of larger particles can fit into the field of view. Many commercial X-ray CT systems also cannot achieve their highest resolution at high power [68], mainly due to source point spread with increasing power [99] and increased detector blurring [100], which limits the materials that can be analysed at high resolution.

3.2. Limits of material suitability

While X-ray CT analysis has been applied successfully to characterise particles made from a wide range of materials, a limiting factor is the requirement for X-ray transmission through the sample, given that X-ray transmission reduces with increasing atomic number. The higher the atomic number, the thinner a sample has to be for sufficient X-ray transmission, assuming constant energy of the beam (Figure 8). In the following, we will establish the approximate thickness of single-element samples that are possible to scan with a typical

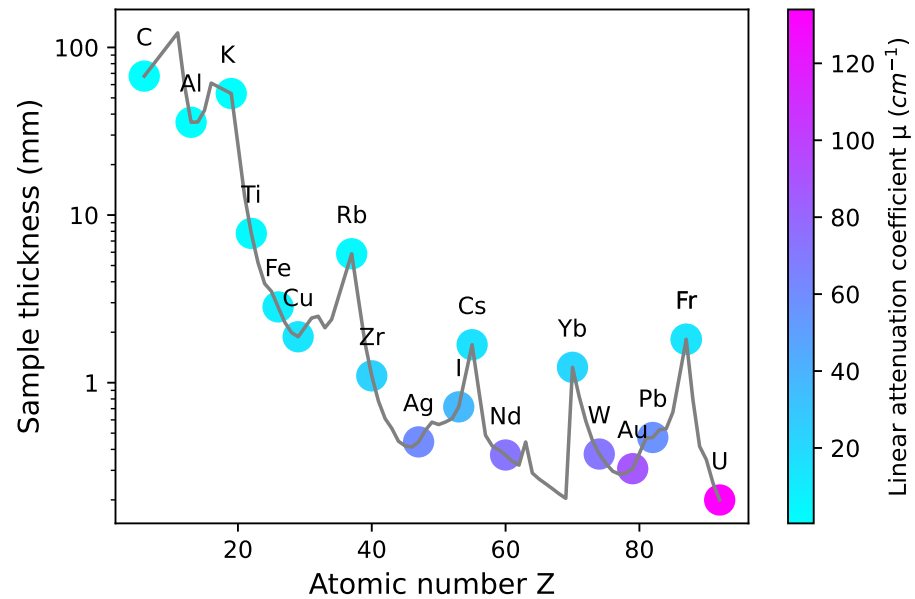


Figure 8. Estimation of sample thickness for a loose particle sample in a capillary for a material with atomic number Z . Calculations assume a packing density of 60%, an X-ray transmission of 20% and an effective energy of 60 keV [101], for which mass attenuation coefficients μ/ρ have been taken from in the National Institute of Standards and Technology's (NIST, USA) X-ray Mass Attenuation Coefficients database [102]. The grey line shows estimated sample thickness for all elements ($Z=8$ to $Z=92$, excluding gases), while the coloured dots highlight selected elements. The colour represents the linear attenuation coefficient, μ , calculated from the mass attenuation coefficient μ/ρ and the density ρ .

laboratory X-ray CT instruments. In principle, the thickness t for a given transmission I/I_0 356
can be calculated by re-arranging the Lambert-Beer equation: 357

$$I = I_0 e^{-\frac{\mu}{\rho} \cdot \rho t} \Leftrightarrow t = 1/\mu \cdot \ln(I_0/I) \quad (1)$$

with I intensity, I_0 initial intensity, ρ density, and μ/ρ mass attenuation coefficient. The 358
Lambert-Beer equation assumes a monochromatic, parallel beam and single-material sam- 359
ple of constant thickness. Those assumptions are not met in the reality of laboratory X-ray 360
sources with polychromatic and divergent beams, detectors with unknown energy response 361
functions, and multi-material, irregularly shaped samples. However, an approximation of 362
the sample thickness can still be made to understand the limits of the current methodology. 363
Most modern laboratory X-ray CT systems operate with a polychromatic source, often with 364
a tuneable accelerating voltage up to 160 kV or 225 kV. However, because of the nature of 365
the bremsstrahlung spectrum, the proportion of high-energy photons within the spectrum 366
is very small. As a first step in simplifying the problem, the polychromatic spectrum can 367
be approximated by a single effective energy [101]. This energy is typically considerably 368
lower than the maximum possible energy for the system, for example the effective energy 369
of a 225 kV tungsten target source has been calculated to be between 40 kV and 80 kV, 370
depending on accelerating voltage [101]. Once a suitable energy has been estimated, the 371
mass attenuation coefficient and the density for a given material for that energy can be 372
found from tabulated values [102,103]. Further assuming a collimated X-ray beam and 373
a flat sample (or the centre of a cylinder), the thickness t for a given transmission can be 374
calculated with the Lambert-Beer equation above (Eq. 1). To derive Figure 8, an effective 375
energy of 60 keV has been assumed, along with a transmission of 20%. Additionally, it 376

has been assumed that the sample is a granular material with a packing density of 60%. Samples made of materials with atomic numbers higher than 40 (zirconium) would have to be thinner than <1 mm to achieve sufficient transmission. As samples under 1 mm become difficult to handle in practice, an alternative way of dealing with particles of high-Z materials is to disperse them in epoxy resin to achieve a reduced packing density. This in turn allows for thicker samples of an equivalent X-ray transmission.

3.3. Outlook and future developments

As this review has shown, particle analysis with X-ray CT has become an often-used methodology. However, there is scope for the method to become more widely used, as thus far, the majority of publications citing the use of this technique stem from additive manufacturing, with only a few examples from other disciplines, such as geological studies or pharmaceutical development. Particle size, if over a few micrometres, and material composition are not necessarily limiting factors, as long as the samples are adequately prepared. The non-destructive nature of X-ray imaging, along with the potential to prepare samples without the need to embed them in resin, makes the method especially suitable for substances that might react with epoxy, or have a similar composition to epoxy, which would decrease contrast.

Although considerable increases in spatial resolution of laboratory X-ray CT instruments seems to be unlikely in the near future, improvements might be possible with regards to the field of view. The development of larger detectors, or of projection image stitching methods, would allow for a larger FoV with a similar voxel size. Especially for spaced-apart particles, a larger FoV would enable scans to simultaneously cover a larger quantity of particles. Currently, a limiting factor with regards to image size, is the size of the resulting data files. However, with increasing computer memory capacity, this limitation is likely to be overcome. Further improvements are also likely with regards to noise and other image artifact reduction, through improved image filters and machine learning routines. This would enable clearer segmentation, especially of closely packed particles, which is currently a limiting factor for loose particle samples.

4. Conclusions

1. Particle characterisation with X-ray CT has become a widely used method over the last 20 years.
2. The advantages of X-ray CT are the ease of sample preparation, and the available measures of the 3D size and morphology of the particles, as well as internal features such as intra-particle porosity.
3. Since each X-ray CT scan typically encompasses tens of thousands of particles, it is easy to achieve statistically significant results.
4. Modern sub-micrometre X-ray CT systems are able to scan particles as small as 5 μm , or potentially as small as 2 to 3 μm , if the particles are spaced apart.
5. Using theoretical approximations, we have shown that X-ray CT is suitable for characterising materials with atomic numbers up to $Z = 40$ when the sample is prepared in form of loose particles in a capillary.
6. Materials with an atomic number greater than 40 need special sample preparation methods such as diluting in epoxy to achieve enough X-ray transmission from a typical laboratory source.

Author Contributions: Conceptualization, J. Behnsen; methodology, J. Behnsen, J. Houghton, writing—original draft preparation, J. Behnsen; writing—review and editing: K. Black, R. Worden, funding acquisition: K. Black, R. Worden. All authors have read and agreed to the published version of the manuscript.

Funding: The Zeiss Xradia Versa 620 at the University of Liverpool was funded under the EPSRC strategic equipment grant number EP/V007610/1.

Data Availability Statement: Not applicable.

Acknowledgments: The help of R. Finch for the preparation of the copper samples shown in 6, and 7 is much appreciated.

Conflicts of Interest: The authors declare no conflict of interest.

References

1. Seidler, G.T.; Martinez, G.; Seeley, L.H.; Kim, K.H.; Behne, E.A.; Zaranek, S.; Chapman, B.D.; Heald, S.M.; Brewster, D.L. Granule-by-granule reconstruction of a sandpile from x-ray microtomography data. *Physical review. E, Statistical physics, plasmas, fluids, and related interdisciplinary topics* **2000**, *62*, 8175–81.
2. Garboczi, E. Three-dimensional mathematical analysis of particle shape using X-ray tomography and spherical harmonics: Application to aggregates used in concrete. *Cement and Concrete Research* **2002**, *32*, 1621–1638. [https://doi.org/10.1016/S0008-8846\(02\)00836-0](https://doi.org/10.1016/S0008-8846(02)00836-0).
3. Lame, O.; Bellet, D.; Michiel, M.D.; Bouvard, D. In situ microtomography investigation of metal powder compacts during sintering. *Nuclear Instruments and Methods in Physics Research Section B: Beam Interactions with Materials and Atoms* **2003**, *200*, 287–294. Proceedings of the E-MRS 2002 Symposium I on Synchrotron Radiation and Materials Science, [https://doi.org/10.1016/S0168-583X\(02\)01690-7](https://doi.org/10.1016/S0168-583X(02)01690-7).
4. Miller, J.D.; Lin, C.L. Three-dimensional analysis of particulates in mineral processing systems by cone beam X-ray microtomography. *Mining, Metallurgy & Exploration* **2004**, *21*, 113–124. <https://doi.org/10.1007/BF03403313>.
5. Aste, T.; Saadatfar, M.; Senden, T.J. Geometrical structure of disordered sphere packings. *Phys. Rev. E* **2005**, *71*, 061302. <https://doi.org/10.1103/PhysRevE.71.061302>.
6. Thompson, K.E.; Willson, C.S.; Zhang, W. Quantitative computer reconstruction of particulate materials from microtomography images. *Powder Technology* **2006**, *163*, 169–182. <https://doi.org/10.1016/j.powtec.2005.12.016>.
7. Erdoğan, S.; Garboczi, E.; Fowler, D. Shape and size of microfine aggregates: X-ray microcomputed tomography vs. laser diffraction. *Powder Technology* **2007**, *177*, 53–63. <https://doi.org/10.1016/j.powtec.2007.02.016>.
8. Ahsan, M.N.; Pinkerton, A.J.; Moat, R.J.; Shackleton, J. A comparative study of laser direct metal deposition characteristics using gas and plasma-atomized Ti–6Al–4V powders. *Materials Science and Engineering: A* **2011**, *528*, 7648–7657. <https://doi.org/10.1016/j.msea.2011.06.074>.
9. Dann, R.; Turner, M.; Close, M.; Knackstedt, M. Multi-scale characterisation of coastal sand aquifer media for contaminant transport using X-ray computed tomography. *Environmental Earth Sciences* **2011**, *63*, 1125–1137. <https://doi.org/10.1007/s12665-010-0788-8>.
10. Redenbach, C.; Ohser-Wiedemann, R.; Löffler, R.; Bernthaler, T.; Nagel, A. Characterization of Powders using Micro Computed Tomography. *Particle & Particle Systems Characterization* **2011**, *28*, 3–12. <https://doi.org/10.1002/ppsc.200900088>.
11. Andò, E.; Hall, S.A.; Viggiani, G.; Desrues, J.; Bésuelle, P. Grain-scale experimental investigation of localised deformation in sand: a discrete particle tracking approach. *Acta Geotechnica* **2012**, *7*, 1–13. <https://doi.org/10.1007/s11440-011-0151-6>.
12. Chawanji, A.; Baldwin, A.; Brisson, G.; Webster, E. Use of X-ray micro tomography to study the microstructure of loose-packed and compacted milk powders. *Journal of Microscopy* **2012**, *248*, 49–57. <https://doi.org/10.1111/j.1365-2818.2012.03649.x>.
13. Fonseca, J.; O’Sullivan, C.; Coop, M.; Lee, P. Non-invasive characterization of particle morphology of natural sands. *Soils and Foundations* **2012**, *52*, 712–722. <https://doi.org/10.1016/j.sandf.2012.07.011>.
14. Willson, C.S.; Lu, N.; Likos, W.J. Quantification of Grain, Pore, and Fluid Microstructure of Unsaturated Sand from X-Ray Computed Tomography Images. *Geotechnical Testing Journal* **2012**, *35*.
15. Andò, E.; Viggiani, G.; Hall, S.A.; Desrues, J. Experimental micro-mechanics of granular media studied by x-ray tomography: recent results and challenges. *Géotechnique Letters* **2013**, *3*, 142–146. <https://doi.org/10.1680/geolett.13.00036>.
16. Cottrino, S.; Jorand, Y.; Maire, E.; Adrien, J. Characterization by X-ray tomography of granulated alumina powder during in situ die compaction. *Materials Characterization* **2013**, *81*, 111–123. <https://doi.org/10.1016/j.matchar.2013.04.004>.
17. Schaller, F.M.; Neudecker, M.; Saadatfar, M.; Delaney, G.; Mecke, K.; Schröder-Turk, G.E.; Schröter, M. Tomographic analysis of jammed ellipsoid packings. *AIP Conference Proceedings* **2013**, *1542*, 377–380. <https://doi.org/10.1063/1.4811946>.
18. Fonseca, J.; Sim, W.; Shire, T.; O’Sullivan, C. Microstructural analysis of sands with varying degrees of internal stability. *Géotechnique* **2014**, *64*, 405–411. <https://doi.org/10.1680/geot.13.T.014>.
19. Slotwinski, J.A.; Garboczi, E.J.; Stutzman, P.E.; Ferraris, C.F.; Watson, S.S.; Peltz, M.A. Characterization of Metal Powders Used for Additive Manufacturing. *Journal of Research of the National Institute of Standards and Technology* **2014**, *119*, 460. <https://doi.org/10.6028/jres.119.018>.
20. Devarrewaere, W.; Foqué, D.; Heimbach, U.; Cantre, D.; Nicolai, B.; Nuyttens, D.; Verboven, P. Quantitative 3D Shape Description of Dust Particles from Treated Seeds by Means of X-ray Micro-CT. *Environmental Science & Technology* **2015**, *49*, 7310–7318. PMID: 26023822, <https://doi.org/10.1021/acs.est.5b02250>.
21. Tammis-Williams, S.; Zhao, H.; Léonard, F.; Derguti, F.; Todd, I.; Prangnell, P. XCT analysis of the influence of melt strategies on defect population in Ti–6Al–4V components manufactured by Selective Electron Beam Melting. *Materials Characterization* **2015**, *102*, 47–61. <https://doi.org/10.1016/j.matchar.2015.02.008>.
22. Wang, Y.; Lin, C.; Miller, J. Improved 3D image segmentation for X-ray tomographic analysis of packed particle beds. *Minerals Engineering* **2015**, *83*, 185–191. <https://doi.org/10.1016/j.mineng.2015.09.007>.

23. Heim, K.; Bernier, F.; Pelletier, R.; Lefebvre, L.P. High resolution pore size analysis in metallic powders by X-ray tomography. *Case Studies in Nondestructive Testing and Evaluation* **2016**, *6*, 45–52. <https://doi.org/10.1016/j.csnedt.2016.09.002>. 485
24. Pashminehazar, R.; Kharaghani, A.; Tsotsas, E. Three dimensional characterization of morphology and internal structure of soft material agglomerates produced in spray fluidized bed by X-ray tomography. *Powder Technology* **2016**, *300*, 46–60. 7th International Granulation Workshop 2015: Granulation across the length scales, <https://doi.org/10.1016/j.powtec.2016.03.053>. 487
25. Wang, Y.; Lin, C.; Miller, J. 3D image segmentation for analysis of multisize particles in a packed particle bed. *Powder Technology* **2016**, *301*, 160–168. <https://doi.org/10.1016/j.powtec.2016.05.012>. 488
26. Zhao, B.; Wang, J. 3D quantitative shape analysis on form, roundness, and compactness with μ CT. *Powder Technology* **2016**, *291*, 262–275. <https://doi.org/10.1016/j.powtec.2015.12.029>. 489
27. Zhou, B.; Wang, J. Generation of a realistic 3D sand assembly using X-ray micro-computed tomography and spherical harmonic-based principal component analysis. *International Journal for Numerical and Analytical Methods in Geomechanics* **2017**, *41*, 93–109. <https://doi.org/10.1002/nag.2548>. 490
28. Cunningham, R.; Narra, S.P.; Montgomery, C.; Beuth, J.; Rollett, A.D. Synchrotron-Based X-ray Microtomography Characterization of the Effect of Processing Variables on Porosity Formation in Laser Power-Bed Additive Manufacturing of Ti-6Al-4V. *JOM* **2017**, *69*, 479–484. <https://doi.org/10.1007/s11837-016-2234-1>. 491
29. Garboczi, E.; Bullard, J. 3D analytical mathematical models of random star-shape particles via a combination of X-ray computed microtomography and spherical harmonic analysis. *Advanced Powder Technology* **2017**, *28*, 325–339. <https://doi.org/10.1016/j.apt.2016.10.014>. 492
30. Garboczi, E.; Riding, K.; Mirzahosseini, M. Particle shape effects on particle size measurement for crushed waste glass. *Advanced Powder Technology* **2017**, *28*, 648–657. <https://doi.org/10.1016/j.apt.2016.12.002>. 493
31. Grell, W.; Solis-Ramos, E.; Clark, E.; Lucon, E.; Garboczi, E.; Predecki, P.; Loftus, Z.; Kumosa, M. Effect of powder oxidation on the impact toughness of electron beam melting Ti-6Al-4V. *Additive Manufacturing* **2017**, *17*, 123–134. <https://doi.org/10.1016/j.addma.2017.08.002>. 494
32. Bernier, F.; Tahara, R.; Gendron, M. Additive manufacturing powder feedstock characterization using X-ray tomography. *Metal Powder Report* **2018**, *73*, 158–162. <https://doi.org/10.1016/j.mprp.2018.01.002>. 495
33. Chen, G.; Zhou, Q.; Zhao, S.; Yin, J.; Tan, P.; Li, Z.; Ge, Y.; Wang, J.; Tang, H. A pore morphological study of gas-atomized Ti-6Al-4V powders by scanning electron microscopy and synchrotron X-ray computed tomography. *Powder Technology* **2018**, *330*, 425–430. <https://doi.org/10.1016/j.powtec.2018.02.053>. 496
34. Chen, G.; Zhao, S.; Tan, P.; Wang, J.; Xiang, C.; Tang, H. A comparative study of Ti-6Al-4V powders for additive manufacturing by gas atomization, plasma rotating electrode process and plasma atomization. *Powder Technology* **2018**, *333*, 38–46. <https://doi.org/10.1016/j.powtec.2018.04.013>. 497
35. du Plessis, A.; Sperling, P.; Beerlink, A.; du Preez, W.B.; le Roux, S.G. Standard method for microCT-based additive manufacturing quality control 4: Metal powder analysis. *MethodsX* **2018**, *5*, 1336–1345. <https://doi.org/10.1016/j.mex.2018.10.021>. 498
36. Karatza, Z.; Andò, E.; Papanicolopoulos, S.A.; Ooi, J.Y.; Viggiani, G. Evolution of deformation and breakage in sand studied using X-ray tomography. *Géotechnique* **2018**, *68*, 107–117, [<https://doi.org/10.1680/jgeot.16.P.208>]. <https://doi.org/10.1680/jgeot.16.P.208>. 499
37. Mostafaei, A.; Hilla, C.; Stevens, E.L.; Nandwana, P.; Elliott, A.M.; Chmielus, M. Comparison of characterization methods for differently atomized nickel-based alloy 625 powders. *Powder Technology* **2018**, *333*, 180–192. <https://doi.org/10.1016/j.powtec.2018.04.014>. 500
38. Rozendaal, A.; Le Roux, S.; du Plessis, A.; Philander, C. Grade and product quality control by microCT scanning of the world class Namakwa Sands Ti-Zr placer deposit West Coast, South Africa: An orientation study. *Minerals Engineering* **2018**, *116*, 152–162. <https://doi.org/10.1016/j.mineng.2017.09.001>. 501
39. Safonov, I.; Yakimchuk, I.; Abashkin, V. Algorithms for 3D Particles Characterization Using X-Ray Microtomography in Proppant Crush Test. *Journal of Imaging* **2018**, *4*. <https://doi.org/10.3390/jimaging4110134>. 502
40. Sinico, M.; Ametova, E.; Witvrouw, A.; Dewulf, W. Characterization of AM Metal Powder with an Industrial Microfocus CT: Potential and Limitations. American Society for Precision Engineering, 2018, Vol. 69. 503
41. Su, D.; Yan, W. 3D characterization of general-shape sand particles using microfocus X-ray computed tomography and spherical harmonic functions, and particle regeneration using multivariate random vector. *Powder Technology* **2018**, *323*, 8–23. <https://doi.org/10.1016/j.powtec.2017.09.030>. 504
42. Zhou, B.; Wang, J.; Wang, H. Three-dimensional sphericity, roundness and fractal dimension of sand particles. *Géotechnique* **2018**, *68*, 18–30. <https://doi.org/10.1680/jgeot.16.P.207>. 505
43. Heiden, M.J.; Deibler, L.A.; Rodelas, J.M.; Koepke, J.R.; Tung, D.J.; Saiz, D.J.; Jared, B.H. Evolution of 316L stainless steel feedstock due to laser powder bed fusion process. *Additive Manufacturing* **2019**, *25*, 84–103. <https://doi.org/10.1016/j.addma.2018.10.019>. 506
44. Karatza, Z.; Andò, E.; Papanicolopoulos, S.A.; Viggiani, G.; Ooi, J.Y. Effect of particle morphology and contacts on particle breakage in a granular assembly studied using X-ray tomography. *Granular Matter* **2019**, *21*, 44. <https://doi.org/10.1007/s10035-019-0898-2>. 507
45. Pelletier, R.; Bernier, F.; Charbonneau, C. Quantification of contaminants in 3D printing metal powders using microfocus x-ray tomography. In Proceedings of the International Conference on Powder metallurgy and Particulate Materials (POWDERMET2019). APMI International, 2019, International Conference on Powder metallurgy and Particulate Materials (POWDERMET2019), Additive Manufacturing with Powder Metallurgy (AMPA2019), June 23-26, 2019, Phoenix, AR, USA. 508

46. Thiede, T.; Mishurova, T.; Evsevlev, S.; Serrano-Munoz, I.; Gollwitzer, C.; Bruno, G. 3D Shape Analysis of Powder for Laser Beam Melting by Synchrotron X-ray CT. *Quantum Beam Science* **2019**, *3*. <https://doi.org/10.3390/qubs3010003>. 544
47. Wang, P.; Karatza, Z.; Arson, C. DEM modelling of sequential fragmentation of zeolite granules under oedometric compression based on XCT observations. *Powder Technology* **2019**, *347*, 66–75. <https://doi.org/10.1016/j.powtec.2019.02.050>. 545
48. Zheng, K.H.; Qiu, B.J.; Li, J.P.; Gao, K.D. 3D XCT Mesostructure Characterization and Image-Based Discrete Element (DE) Modelling of Failure Patterns in Coal Gangue Particles (CGPs). *Complexity* **2019**, *2019*, 4021368. <https://doi.org/10.1155/2019/4021368>. 546
49. Cuesta Cano, A.; Van Stappen, J.F.; Wolterbeek, T.K.; Hangx, S.J. Uniaxial compaction of sand using 4D X-ray tomography: The effect of mineralogy on grain-scale compaction mechanisms. *Materials Today Communications* **2021**, *26*, 101881. <https://doi.org/10.1016/j.mtcomm.2020.101881>. 547
50. Feng, Z.K.; Xu, W.J.; Lubbe, R. Three-dimensional morphological characteristics of particles in nature and its application for DEM simulation. *Powder Technology* **2020**, *364*, 635–646. <https://doi.org/10.1016/j.powtec.2020.02.022>. 548
51. Gajjar, P.; Styliari, I.; Nguyen, T.; Carr, J.; Chen, X.; Elliott, J.; Hammond, R.; Burnett, T.; Roberts, K.; Withers, P.; et al. 3D characterisation of dry powder inhaler formulations: Developing X-ray micro computed tomography approaches. *European Journal of Pharmaceutics and Biopharmaceutics* **2020**, *151*, 32–44. <https://doi.org/10.1016/j.ejpb.2020.02.013>. 549
52. Garboczi, E.; Hrabec, N. Particle shape and size analysis for metal powders used for additive manufacturing: Technique description and application to two gas-atomized and plasma-atomized Ti64 powders. *Additive Manufacturing* **2020**, *31*, 100965. <https://doi.org/10.1016/j.addma.2019.100965>. 550
53. Leibner, T.; Diener, A.; Löwer, E.; Ditscherlein, R.; Krüger, K.; Kwade, A.; Peuker, U. 3D ex-situ and in-situ X-ray CT process studies in particle technology – A perspective. *Advanced Powder Technology* **2020**, *31*, 78–86. <https://doi.org/10.1016/j.apt.2019.09.038>. 551
54. Nie, J.Y.; Li, D.Q.; Cao, Z.J.; Zhou, B.; Zhang, A.J. Probabilistic characterization and simulation of realistic particle shape based on sphere harmonic representation and Nataf transformation. *Powder Technology* **2020**, *360*, 209–220. <https://doi.org/10.1016/j.powtec.2019.10.007>. 552
55. Turner, T.D.; Gajjar, P.; Fragkopoulos, I.S.; Carr, J.; Nguyen, T.T.H.; Hooper, D.; Clarke, F.; Dawson, N.; Withers, P.J.; Roberts, K.J. Measuring the Particle Packing of L-Glutamic Acid Crystals through X-ray Computed Tomography for Understanding Powder Flow and Consolidation Behavior. *Crystal Growth & Design* **2020**, *20*, 4252–4263, [<https://doi.org/10.1021/acs.cgd.9b01515>]. <https://doi.org/10.1021/acs.cgd.9b01515>. 553
56. Fei, W.; Narsilio, G.; van der Linden, J.; Disfani, M.; Miao, X.; Yang, B.; Afshar, T. X-ray computed tomography images and network data of sands under compression. *Data in Brief* **2021**, *36*, 107122. <https://doi.org/10.1016/j.dib.2021.107122>. 554
57. Gajjar, P.; Nguyen, T.T.H.; Sun, J.; Styliari, I.D.; Bale, H.; McDonald, S.A.; Burnett, T.L.; Tordoff, B.; Lauridsen, E.; Hammond, R.B.; et al. Crystallographic tomography and molecular modelling of structured organic polycrystalline powders. *CrystEngComm* **2021**, *23*, 2520–2531. <https://doi.org/10.1039/D0CE01712D>. 555
58. Hebert, R.J.; Sun, Y.; Aindow, M.; Garboczi, E.J. Three-dimensional particle size, shape, and internal porosity characterization: Application to five similar titanium alloy (Ti–6Al–4V) powders and comparison to two-dimensional measurements. *Additive Manufacturing* **2021**, *44*, 102060. <https://doi.org/10.1016/j.addma.2021.102060>. 556
59. Zhang, C.; Zhao, S.; Zhao, J.; Zhou, X. Three-dimensional Voronoi analysis of realistic grain packing: An XCT assisted set Voronoi tessellation framework. *Powder Technology* **2021**, *379*, 251–264. <https://doi.org/10.1016/j.powtec.2020.10.054>. 557
60. Zhou, X.; Dai, N.; Cheng, X.; Thompson, A.; Leach, R. Three-dimensional characterization of powder particles using X-ray computed tomography. *Additive Manufacturing* **2021**, *40*, 101913. <https://doi.org/10.1016/j.addma.2021.101913>. 558
61. Whiting, J.G.; Garboczi, E.J.; Tondare, V.N.; Scott, J.H.J.; Donmez, M.A.; Moylan, S.P. A comparison of particle size distribution and morphology data acquired using lab-based and commercially available techniques: Application to stainless steel powder. *Powder Technology* **2022**, *396*, 648–662. <https://doi.org/10.1016/j.powtec.2021.10.063>. 559
62. Weis, S.; Schröter, M. Analyzing X-ray tomographies of granular packings. *Review of Scientific Instruments* **2017**, *88*, 051809. <https://doi.org/10.1063/1.4983051>. 560
63. Withers, P.J.; Bouman, C.; Carmignato, S.; Cnudde, V.; Grimaldi, D.; Hagen, C.K.; Maire, E.; Manley, M.; Du Plessis, A.; Stock, S.R. X-ray computed tomography. *Nature Reviews Methods Primers* **2021**, *1*, 18. <https://doi.org/10.1038/s43586-021-00015-4>. 561
64. du Plessis, A.; Yadroitsev, I.; Yadroitsava, I.; Le Roux, S.G. X-Ray Microcomputed Tomography in Additive Manufacturing: A Review of the Current Technology and Applications. *3D Printing and Additive Manufacturing* **2018**, *5*, 227–247. <https://doi.org/10.1089/3dp.2018.0060>. 562
65. Thompson, A.; Maskery, I.; Leach, R.K. X-ray computed tomography for additive manufacturing: a review. *Measurement Science and Technology* **2016**, *27*, 072001. <https://doi.org/10.1088/0957-0233/27/7/072001>. 563
66. Zingg, T. *Beitrag Zur Schotteranalyse*; Leemann: Zurich, 1935. 564
67. Hounsfield, G.N. Computerized transverse axial scanning (tomography). 1. Description of system. *The British journal of radiology* **1973**, *46*, 1016–22. 565
68. Carmignato, S.; Dewulf, W.; Leach, R.K. Industrial X-Ray Computed Tomography. *Industrial X-Ray Computed Tomography* **2018**. 566
69. Stock, S.R. Recent advances in X-ray microtomography applied to materials. *null* **2008**, *53*, 129–181. <https://doi.org/10.1179/174328008X277803>. 567
70. Maire, E.; Withers, P.J. Quantitative X-ray tomography. *International Materials Reviews* **2014**, *59*, 1–43. <https://doi.org/10.1179/1743280413Y.0000000023>. 568

71. Buzug, T. *Computed Tomography*; Springer: Berlin, Germany, 2008. 603
72. Feldkamp, L.A.; Davis, L.C.; Kress, J.W. Practical cone-beam algorithm. *Journal of the Optical Society of America A* **1984**, pp. 612–619. 604
73. Kennedy, S.K.; Dalley, A.M.; Kotyk, G.J. Additive Manufacturing: Assessing Metal Powder Quality Through Characterizing Feedstock and Contaminants. *Journal of Materials Engineering and Performance* **2019**, *28*, 728–740. <https://doi.org/10.1007/s11665-018-3841-5>. 605
74. Kantzos, P.T.; Bonacuse, P.J.; Telesman, J.; Gabb, T.P.; Barrie, R.L.; Banik, A. Effect of powder cleanliness on the fatigue behaviour of powder metallurgy Ni-disk alloy UDIMET 720. *Superalloys* **2004**, pp. 409–417. 606
75. Zheng, J.; Sun, Q.; Zheng, H.; Wei, D.; Li, Z.; Gao, L. Three-dimensional particle shape characterizations from half particle geometries. *Powder Technology* **2020**, *367*, 122–132. <https://doi.org/10.1016/j.powtec.2020.03.046>. 607
76. Rodríguez-Sánchez, A.; Thompson, A.; Körner, L.; Brierley, N.; Leach, R. Review of the influence of noise in X-ray computed tomography measurement uncertainty. *Precision Engineering* **2020**, *66*, 382–391. <https://doi.org/10.1016/j.precisioneng.2020.08.004>. 608
77. Russ, J.C.; Neal, F.B. *The Image Processing Handbook*, 7th ed.; CRC Press: Boca Raton, FL, USA, 2018. 609
78. Otsu, N. A Threshold Selection Method from Gray-Level Histograms. *IEEE Transactions on Systems, Man, and Cybernetics* **1979**, *9*, 62–66. <https://doi.org/10.1109/TSMC.1979.4310076>. 610
79. Arganda-Carreras, I.; Kaynig, V.; Rueden, C.; Eliceiri, K.W.; Schindelin, J.; Cardona, A.; Sebastian Seung, H. Trainable Weka Segmentation: a machine learning tool for microscopy pixel classification. *Bioinformatics* **2017**, *33*, 2424–2426. <https://doi.org/10.1093/bioinformatics/btx180>. 611
80. Soille, P. *Morphological Image Analysis: Principles and Applications*; Springer Berlin Heidelberg: Berlin, Heidelberg, 2004; chapter 9, pp. 267–292. https://doi.org/10.1007/978-3-662-05088-0_9. 612
81. Jung, C.; Kim, C. Segmenting Clustered Nuclei Using H-minima Transform-Based Marker Extraction and Contour Parameterization. *IEEE Transactions on Biomedical Engineering* **2010**, *57*, 2600–2604. <https://doi.org/10.1109/TBME.2010.2060336>. 613
82. Legland, D.; Arganda-Carreras, I.; Andrey, P. MorphoLibJ: integrated library and plugins for mathematical morphology with ImageJ. *Bioinformatics* **2016**, *32*, 3532–3534. <https://doi.org/10.1093/bioinformatics/btw413>. 614
83. Lorensen, W.E.; Cline, H.E. Marching Cubes: A High Resolution 3D Surface Construction Algorithm. *SIGGRAPH Comput. Graph.* **1987**, *21*, 163–169. <https://doi.org/10.1145/37402.37422>. 615
84. Lindblad, J. Surface area estimation of digitized 3D objects using weighted local configurations. *Image and Vision Computing* **2005**, *23*, 111–122. <https://doi.org/10.1016/j.imavis.2004.06.012>. 616
85. Lehmann, G.G.; Legland, D. Efficient N-Dimensional surface estimation using Crofton formula and run-length encoding, 2012. 617
86. Legland, D.; Kiêu, K.; Devaux, M.F. Computation of Minkowski Measures on 2D and 3D Binary Images. *Image Analysis and Stereology* **2011**, *26*, 83–92. <https://doi.org/10.5566/ias.v26.p83-92>. 618
87. Taylor, M.A.; Garboczi, E.J.; Erdogan, S.T.; Fowler, D.W. Some properties of irregular 3-D particles. *Powder Technology* **2006**, *162*, 1–15. <https://doi.org/10.1016/j.powtec.2005.10.013>. 619
88. Wadell, H. Volume, Shape, and Roundness of Quartz Particles. *The Journal of Geology* **1935**, *43*, 250–280. <https://doi.org/10.1086/624298>. 620
89. Taylor, M.A. Quantitative measures for shape and size of particles. *Powder Technology* **2002**, *124*, 94–100. [https://doi.org/10.1016/S0032-5910\(01\)00476-4](https://doi.org/10.1016/S0032-5910(01)00476-4). 621
90. Doube, M.; Klosowski, M.M.; Arganda-Carreras, I.; Cordelières, F.P.; Dougherty, R.P.; Jackson, J.S.; Schmid, B.; Hutchinson, J.R.; Shefelbine, S.J. BoneJ: Free and extensible bone image analysis in ImageJ. *Bone* **2010**, *47*, 1076–9. 622
91. O'Rourke, J. Finding minimal enclosing boxes. *International Journal of Computer and Information Sciences* **1985**, *14*, 183–199. <https://doi.org/10.1007/BF00991005>. 623
92. Chelishchev, P.; Sørby, K. Estimation of minimum volume of bounding box for geometrical metrology. *International Journal of Metrology and Quality Engineering* **2020**, *11*. <https://doi.org/10.1051/ijmqe/2020007>. 624
93. Feret, L.R. La grosseur des grains des matières pulvérulentes. *Premières Communications de la Nouvelle Association Internationale pour l'Essai des Matériaux, Groupe D* **1930**, p. 428–443. 625
94. Merkus, H.G. *Particle Size Measurements*; Springer Netherlands, 2009. 626
95. Dougherty, R.; Kunzelmann, K.H. Computing Local Thickness of 3D Structures with ImageJ. *Microscopy and Microanalysis* **2007**, *13*, 1678–1679. <https://doi.org/10.1017/S1431927607074430>. 627
96. Villarraga-Gómez, H.; Herazo, E.L.; Smith, S.T. X-ray computed tomography: from medical imaging to dimensional metrology. *Precision Engineering* **2019**, *60*, 544–569. <https://doi.org/10.1016/j.precisioneng.2019.06.007>. 628
97. Japan Inspection Instruments Manufacturers' Association. Available online. Accessed 8. August 2022. 629
98. Rueckel, J.; Stockmar, M.; Pfeiffer, F.; Herzen, J. Spatial resolution characterization of a X-ray microCT system. *Applied Radiation and Isotopes* **2014**, *94*, 230–234. <https://doi.org/10.1016/j.apradiso.2014.08.014>. 630
99. Hiller, J.; Maisl, M.; Reindl, L.M. Physical characterization and performance evaluation of an x-ray micro-computed tomography system for dimensional metrology applications. *Measurement Science and Technology* **2012**, *23*, 085404. <https://doi.org/10.1088/0957-0233/23/8/085404>. 631
100. Bub, A.; Gondrom, S.; Maisl, M.; Uhlmann, N.; Arnold, W. Image blur in a flat-panel detector due to Compton scattering at its internal mountings. *Measurement Science and Technology* **2007**, *18*, 1270. <https://doi.org/10.1088/0957-0233/18/5/013>. 632

-
101. Bam, L.C.; Miller, J.A.; Becker, M. A Mineral X-ray Linear Attenuation Coefficient Tool (MXLAC) to Assess Mineralogical Differentiation for X-ray Computed Tomography Scanning. *Minerals* **2020**, *10*. <https://doi.org/10.3390/min10050441>. 662
 102. J. H. Hubbell, S.M.S. X-Ray Mass Attenuation Coefficients: NIST Standard Reference Database 126. 2004. Available online. Accessed 2. December 2022, <https://doi.org/10.18434/T4D01F>. 663
 103. Rumble, J., Ed. *CRC Handbook of Chemistry and Physics*, 103 ed.; CRC Press, 2022. 664