

MICROPROCESSOR-BASED AGRICULTURAL

DIGGER CONTROL

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of the University of Liverpool for the degree of
Doctor in Philosophy

by

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SUMMARY

This thesis describes the design, construction, and evaluation of a closed loop microprocessor based control system for a tractor mounted type PA6 agricultural digger as manufactured by F.W. McConnel, Ltd., Ludlow. After a description and analysis of the principal operations for which the digger is used a set of functional objectives is defined. As agricultural diggers are used intermittently and mainly for annual maintenance it was decided to develop a system to reduce the level of skill to be maintained or acquired to use the machine efficiently and effectively.

To reduce the degree of coordination required of the operator the microprocessor system was designed to make straight cuts at any specified pitch by the deflection of a single control lever. To facilitate repetitive difficult cuts a learn and repeat facility was included to repeat a learned path from any given starting point.

To minimise the cost of the system single stage proportional electrohydraulic valves were used and were evaluated in a simple proportional controller built to operate in a fashion similar to the conventional mechanical control system. Having demonstrated that satisfactory manual control may be achieved using these valves the microprocessor system was built, based on an Intel 8085 with an AMD 9511 Arithmetic Processor Unit.

For closed loop control mechanically robust and water

resistant transducers were designed to mount on the machine pivots and measure arm positions. The valves were interfaced to the computer by an eight bit pulse width modulator circuit and an eight bit multiplexed analogue to digital converter was used to input transducer signals and control inputs from the portable control unit. The computer is based on an Intel SDK-85 development kit and power for the system is derived from the tractor battery.

The system software was written in assembly language for speed of execution and stored in EPROM. The program reads the control inputs and machine outputs, inverts the machine geometry to calculate the required output positions and assigns the valve settings according to the positional errors. The sampling and execution frequency of the control software is 30 Hz.

Evaluation trials were carried out with both skilled and novice users. The principal results were that the system assisted with levelling and trench cutting, but overall did not provide any significant consistent increases in work rate for either group of users. Finally, further areas for research are discussed, with reference to both diggers and electrohydraulic hedge cutters.

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4.5 Learn & Repeat	54
4.6 Transducer Resolution	56
4.7 Dynamics	57
4.8 Hydraulics	57
4.9 Mechanics	59
4.10 Control Algorithm	61
V. TRANSDUCERS	68
5.1 Design Constraints	69
5.2 Selection Possibilities	70
5.3 Construction	71
VI. HARDWARE I: SYSTEM STRUCTURE & PROCESSOR BOARD	76
6.1 System Structure	77
6.2 Processor Board	80
6.3 Memory Expansion	82
6.4 Arithmetic Processor Unit	85
6.5 Board Layout	88
6.6 Memory & I/O Maps	89
VII. HARDWARE II: INTERFACE CARDS, POWER SUPPLIES & RACK CONNECTIONS	91
7.1 Analogue Interface Unit	92
7.2 Valve Driver Card	100
7.3 Power Supplies	104
7.4 Rack Layout & Interconnection Tables	107
VIII. HARDWARE III: CONTROL UNIT, TRANSDUCER WIRING, & POWER SWITCHING UNIT	113
8.1 Control Unit	114
8.2 Transducer Wiring	120
8.3 Power Switching Unit	120

IX. SOFTWARE I: GENERAL PURPOSE APU	
SUBROUTINES & MACROS	128
9.1 Arithmetic Processor Unit	129
9.2 Subroutines for APU Stack Data Transfer	130
9.3 Subroutines for APU Operations	133
9.4 Macros for Conditional Jumps	134
X. SOFTWARE II: PROGRAM MANCON	137
10.1 Introduction	138
10.2 Algorithm	138
10.3 Memory Utilisation	140
10.4 Code Documentation	141
XI. SOFTWARE III: PROGRAM DIG	149
11.1 Functional Description & Algorithms	150
11.2 Memory Utilisation	156
11.3 Code Documentation	157
XII. FIELDWORK & SYSTEM EVALUATION	181
12.1 Introduction	182
12.2 Tuning of Control Parameters	182
12.3 Kinematic Evaluation	183
12.4 System Reliability	185
12.5 Functional Evaluation	186
12.6 Learn & Repeat Facility	190
12.7 Estimation of Cost	191
XIII. DISCUSSION	192
13.1 Hardware	193
13.2 Software	195
13.3 Safety	196
13.4 Hydraulics	197
13.5 Functional Aspects	198

13.6 Commercial Considerations	199
XIV. CONCLUSIONS & FURTHER WORK	201
14.1 Conclusions	202
14.2 Further Work	203
REFERENCES	205
APPENDIX A: LISTING OF PROGRAM MANCON	209
APPENDIX B: LISTING OF PROGRAM DIG	228

CHAPTER ONE

INTRODUCTION

- 1.1 Microprocessors in Agriculture
- 1.2 Record Keeping
- 1.3 Modelling
- 1.4 Instrumentation
- 1.5 Control of Machinery & Equipment

1.1 Microprocessors in Agriculture

Over the past few years microprocessors have been used in an increasing number of applications in agriculture to help make optimal use of the resources of energy, materials, money, and manpower. The first area in which they were applied is that of record keeping; subsequently they have been used in modelling, instrumentation, and the control of farm equipment and field machinery. The subject of this work is the application of microprocessors to the control of a tractor mounted hydraulic digger. It is useful, however, to start by putting the work in context and examining how the potential of microcomputers has so far been exploited by the agricultural industry, and what the future developments are likely to be.

1.2 Record Keeping

In 1982 it was estimated that about four hundred microcomputers were being used in farm offices in the UK for accounting, handling payrolls, livestock ration formulation and performance monitoring¹. This number will have greatly increased with decreasing system cost and availability. One particular area for which a number of systems have been developed is that of dairy herd monitoring. In discussing this application Speicher² states

"The ultimate goal is for the computerised data acquisition system to be fully informed on the production, nutrition, reproduction, health, and economic status of all animals at all times and to notify the manager of any appropriate action to be taken."

In some installations this goal is effectively attained, and in addition the monitoring system is used in conjunction with automatic feeding machinery. The data acquisition is automated by the use of cow identifiers, either implanted or worn around the neck, which allow detectors at the milking parlour and feeding points to recognise individual animals³.

The US Department of Agriculture (USDA) is developing a minicomputer system for maintaining record of feed consumption, milk production, temperature, and condition on individual animals to improve the performance of the livestock producer⁴. The computer system facilitates the management of larger herds and enables changes in performance and health problems to be more easily detected by giving data on both the herd and individual animals. It will be a short time before such systems are implemented on microcomputers and come into more widespread use. In a scheme run in Scotland a number of farms use microcomputers to monitor health and, by linking individual micros to a mainframe, large scale statistical studies may be carried out for disease control and studies on optimum herd management strategies⁵.

Another area where microcomputers are used for record keeping is that of plant breeding where conventionally card index systems are used. The USDA have produced a program to be run on a desk microcomputer for use by plant breeders and horticulturalists for maintaining records on plant pedigrees⁶. The program stores, searches, lists, corrects, appends, and duplicates plant pedigree records using magnetic tape for backing store.

1.3 Modelling

A number of programs have been developed for modelling and evaluation of the efficacy of different farming strategies. With for example arable farming, given data on the cropping history of the fields involved, soil analysis, and fertiliser input, the gross profit margin and cash flow for different crops may be calculated. The Ministry of Agriculture, in conjunction with the National Institute for Agricultural Engineering have developed a program for glass house crops and field vegetables where soil analysis data is used to provide information on the fertiliser requirements of each crop. Work has also been done on the optimisation of grassland usage. A number of detailed modelling programs have been written to run on mainframes, not directly accessible to the farmer⁷. With the low cost and versatility of desk top machines such programs should become increasingly available for use on microcomputers.

1.4 Instrumentation

Certain diseases affecting fruit and vegetables may be accurately predicted, and preventive action taken, by close monitoring of such environmental factors as temperature and humidity. Microcomputer systems may be used to continuously monitor these variables and alert the grower when dangerous conditions arise. One such system is being developed for the prediction of apple scab fungus which affects orchards; the processor monitors temperature, leaf wetness, and relative humidity in the orchard, checking for dangerous conditions⁸. The system gives on the spot warning as well as keeping record of the variables monitored for later reference.

Another system for predicting potato blight (the fungus *Phytophthora infestans*) is now commercially available and collects data every ten minutes on temperature, relative humidity, and rainfall⁹. When "blight weather" is detected a display indicates that preventive spraying is required.

An ingenious system has been made for the weighing of poultry whereby a perch is fitted with a load cell and linked to a microcomputer¹⁰. The mean flock weight is thus monitored as random birds alight on the perch. This saves time otherwise spent weighing manually, enables future weight prediction to be made, allows feed conversion measurement, avoids stress to the birds, and facilitates diet control to maximise the number of fertile eggs for breeding flocks.

An automatic system for weighing the different defect categories of fruits and vegetables has been made to facilitate grading operations¹¹. The micro controls the weighing of the contents of each compartment of a mechanical grading table and records the data for the batch on a grade certificate. Microcomputer technology is also used for measuring grain moisture¹², which must be carefully monitored when drying and storing grain, and the quantity of grain harvested on a combine harvester¹³. On the combine harvester it is grain volume that is measured and the system must be first calibrated with the appropriate mass/volume setting. Acreage harvested, average yield, work rate, ground speed, and running yield are also measured and displayed.

1.5 Control of Machinery and Equipment

A major growth area in computerised farming equipment is that of automated animal feeding systems. As early as 1976 a microprocessor based system was developed for cattle recognition and feeding as well as for recording milk production³. It is also possible to mix rations automatically to suit individual animals. A pig feeding system described by Fuller¹⁴ weighs and mixes skim milk and meal and pumps a controlled amount to each pen. Feed can be programmed to be given several times a day using up to four solid and two liquid feed ingredients. In principle each animal may be identified, weighed at the feeding point, have high and low density feeds mixed, and be fed in relation to cost and appetite. The ventilation and heating may also be kept under computer control and an adaptive model used to increase feeding when temperature drops¹⁵.

In the Netherlands micros are used extensively for greenhouse climate control and sophisticated adaptive control schemes are employed using on-line identification¹⁶. Potato sorting has been automated using a microcomputer and a TV camera to sort the potatoes according to size¹⁷. Systems also exist for the control and monitoring of the drying and storage conditions of grain¹⁸.

In the area of field machinery the use of microprocessor for control and monitoring functions is now well established. On combine harvesters the grain loss varies with the harvesting speed. As the machine is driven faster the grain loss increases, however to reduce the loss almost to nil the speed is

prohibitively low so a compromise must be found. On a commercially available system produced by RDS Farm Electronics Ltd. an acceptable level of grain loss is selected and the grain loss monitor is used to control the forward speed of the machine, using another sensor at the front to give advance information about cropping levels¹⁹.

When spraying crops the amount of chemical applied per unit area must be very closely controlled; if too little is applied the spraying may be ineffective and the cost of the chemicals wasted, if too much is applied the crop may be damaged. On the sprayer produced by RDS the operator keys in data on the number of nozzles in use, target speed, flow rate, pressure limits, etc. and by measuring forward speed and nozzle pressure the flow is closely controlled. The system compensates for the square law relation between speed and pressure. The unit displays speed, application rate, pressure, area, trip area as well as the preprogrammed target values. Also, commercially available from Evrard, is a microcomputer based spray system using sonic sensors to measure boom height and keep it constant by controlling the tractor hydraulics²⁰.

A tractor safety system has been developed using a microprocessor to sense p.t.o. engagement, throttle setting, brakes, hydraulics, operator's seat and brake. If, for example the driver leaves his seat with the p.t.o. engaged it will automatically be stopped. The equipment may also be connected up to equipment such as harvesters drawn by the tractor²¹.

These examples show that the use of microprocessors is well established in the agricultural industry and that there is a growing number of applications both in the farm office and in the harsher environment of equipment and field machinery. In view of the rapid growth in the use of these devices in agriculture generally, and their low cost and flexibility, it was decided to investigate their applicability to tractor mounted diggers.

Considerable skill is required to operate these machines efficiently and effectively and a computer assisted control system presents the possibility of facilitating their use. The availability of proportional solenoid valves makes it possible to interface a computer to the machine without the high cost of two stage servo valves. The scope of this work is the development and evaluation, both functional and economic, of a computer based control system for a tractor mounted hydraulic digger. To the knowledge of the author there is not any other computer assisted digger in operation.

CHAPTER TWO

OBJECTIVES

- 2.1 Description of Conventional Machine
- 2.2 Machine Usage
- 2.3 Potential Functions & Limitations of
Computer Control
- 2.4 Objectives & Functional Specification
- 2.5 Design Constraints
- 2.6 Method of Approach

2.1 Description of Conventional Machine

The machine used in this study was a "Power Arm 6" tractor mounted digger manufactured by F.W. McConnell Ltd., Ludlow. A side view of the machine is shown in Fig. 2-1; the main features are two arms and a bucket pivoted as shown and the machine may also slew about a vertical axis. The movement about each of the pivots is effected by double-acting hydraulic rams, shown shaded; for slewing there are two rams, one on each side of the machine.

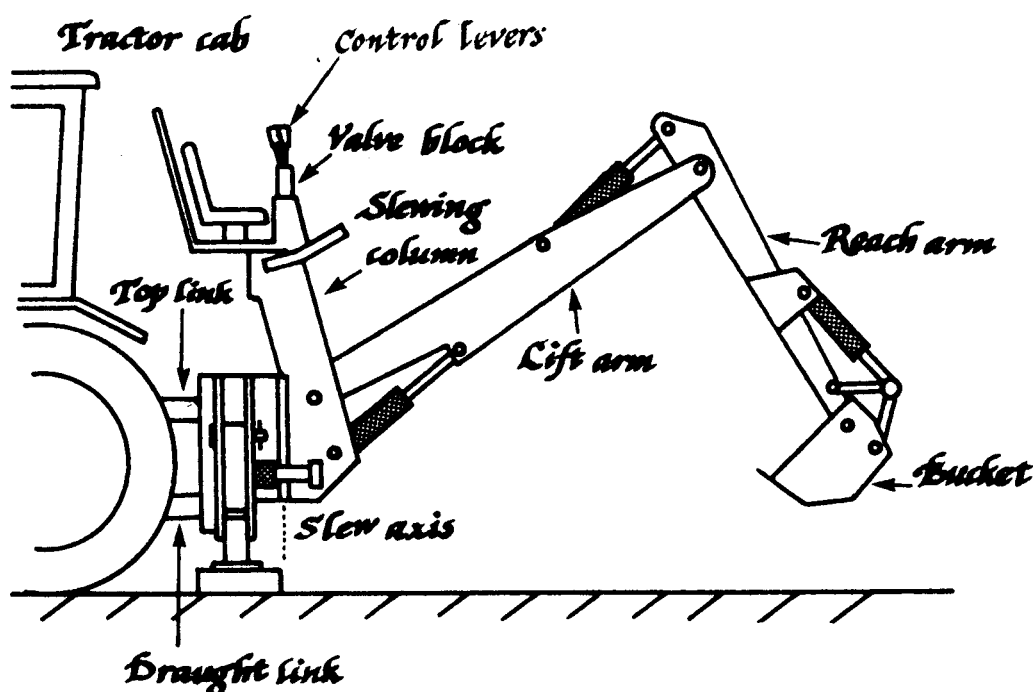


Fig. 2-1: Side View of Machine

Dimensions and masses of the arms and the bucket are as follows:

<u>Main Arm:</u>	Pivot to pivot length	2.28 m
	Mass	68 kg
<u>Dipper Arm:</u>	Pivot to pivot length	1.57 m
	Mass	53 kg
<u>Bucket:</u>	Pivot to blade length	0.4 m
	Mass	60 kg

The operator's seat is situated on the slewing column on the machine and he operates the proportional valves by levers on the valve block. The layout of the control joysticks is shown in Fig. 2-2: the Lift or Main Arm moves Up and Down, the Reach or Dipper Arm moves In and Out. The Open and Close functions operate the Bucket, and Right and Left the Slew. Alternatively he may sit in the tractor cab with mechanical cables linking the control levers to the valve block. The digger is primarily intended for use as a farm maintenance tool and is attached to the three point linkage of an agricultural tractor and powered by the tractor engine.

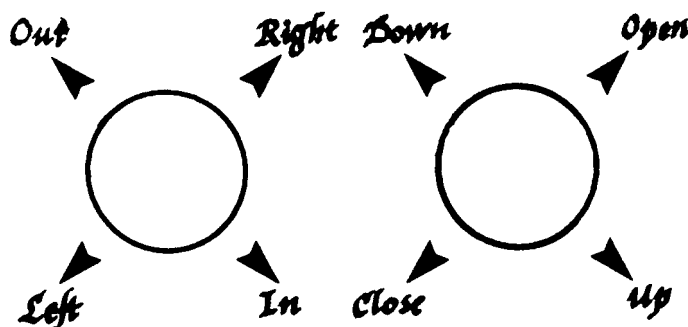


Fig. 2-2: Layout of Joystick Control Functions

Three links attach the digger to the tractor: two draught links and an adjustable top link. Associated with each draught link is an additional 'Instant Weight Transfer' (IWT) ram which, when activated by the operator, exerts a lifting force against the tractor via the draught links and presses the feet of the machine onto the ground and increasing the machine's rigidity. The slewing axis may be set vertically by adjusting the top link

and the feet at the side of the machine; on later models the top link is hydraulically adjustable as is the sideways tilt.

The power for the machine is derived from the tractor Power Take Off (PTO) shaft, which through a gearbox drives a

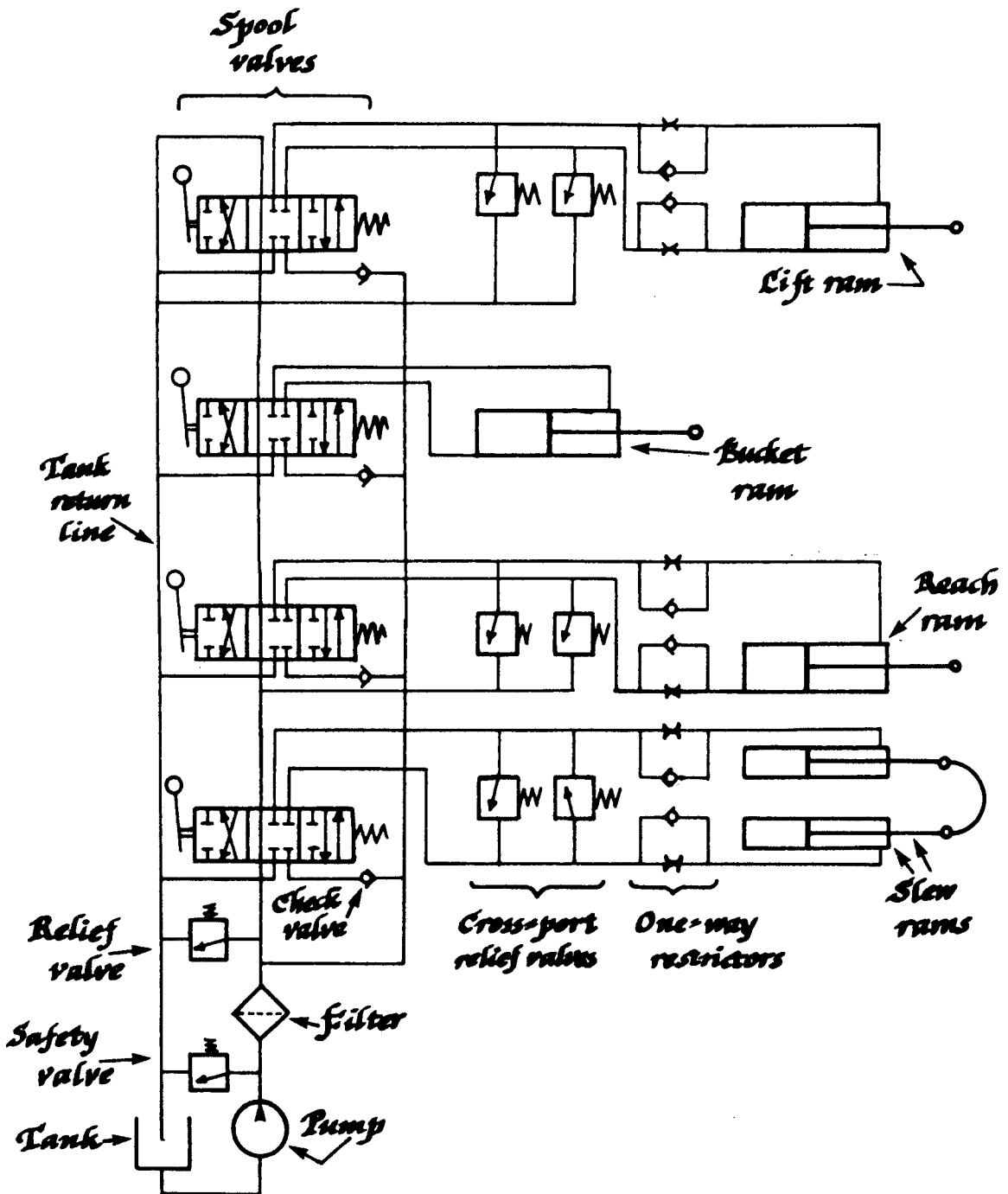


Fig. 2-3: Hydraulic Circuit

constant displacement pump. The basic hydraulic circuit is shown in Fig. 2-3²². The PTO shaft is set to rotate at approximately 540 rev/min which gives a pump flow rate of 0.25 l/s (4 g.p.m.). The safety valve connects the pump output back to the tank and opens in the event of a blockage in the output line. The relief valve is set to 1.7×10^7 Pa (2500 p.s.i.) and limits the supply pressure to the system. When none of the services (Slew, Lift, Reach, or Bucket) is selected, the spool valves are in the position shown and the output from the pump is fed straight back to the tank.

When any of the services is selected the tank return line is closed and oil passes through the check valve to one port of the corresponding ram. The other port of the ram is simultaneously connected to the tank via a one-way restrictor which restricts oil flow from the ram to prevent cavitation. The check valves between the pump and the spool valve prevent any back flow from the ram if the supply pressure should be reduced because of high demand from more than one service or if a high load is applied. The IWT is not shown in this diagram.

In normal operation the supply pressure is lower than the relief valve pressure and there is hydraulic interaction between the services. As more than one service is selected the supply flow will divide depending on the valve opening, restrictors and load forces on the rams.

2.2 Machine Usage

The digger is a versatile machine and for different operations a range of buckets and implements may be fitted in place of the bucket shown above. These include auto-eject trenching buckets, wide and narrow digging and ditch cleaning buckets, a grab, and pick tine. Also the machine configuration (i.e. pivot positions) may be changed to suit the task in hand.

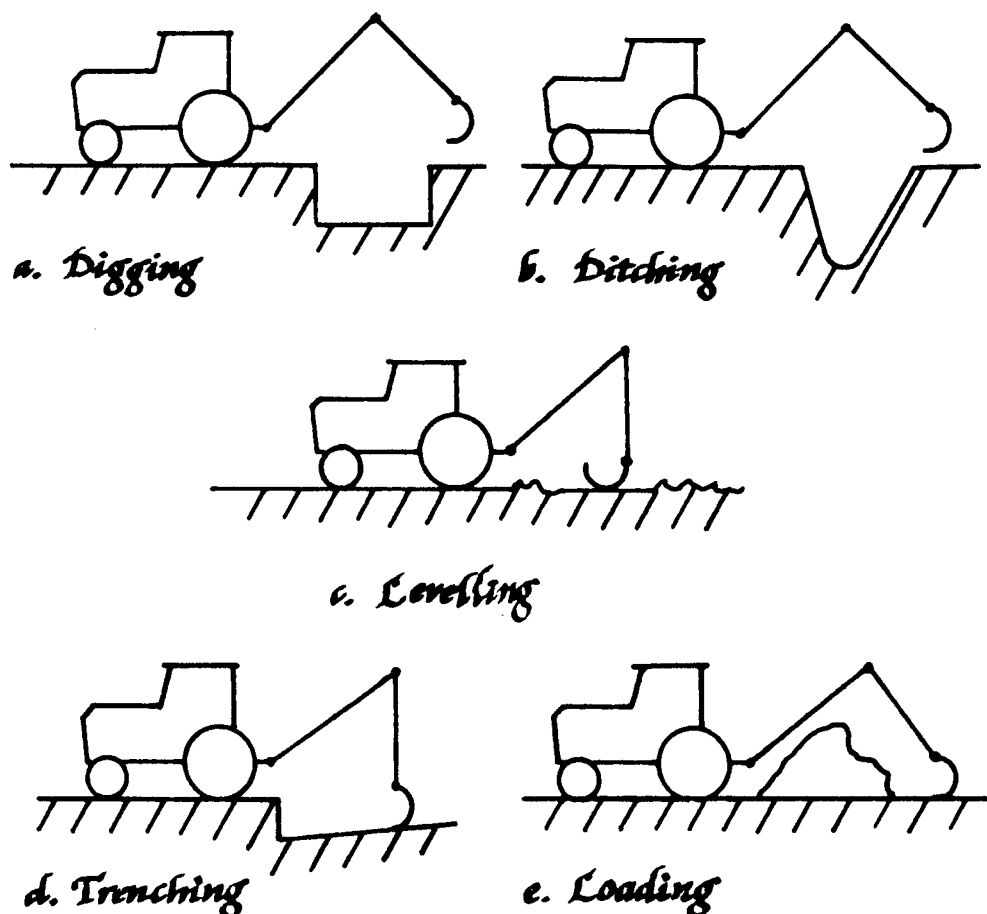


Fig. 2-4: Principal Operations

The principal operations for which the digger is used are digging, ditching, trenching, levelling, and loading (see Fig. 2-4). However considerable practice is required to do work accurately and rapidly. There are five main aspects to the skill developed by an operator over a period of time:

1. Relating the control joystick axes to the corresponding rams.
2. Combining ram movements and valve settings to give the desired bucket blade movement given the mechanical and hydraulic interaction between the services.
3. Judging the inclination of planes to be cut.
4. Positioning the arms and bucket to bring maximum cutting force to bear against an obstruction.
5. Judging the behaviour of the material being handled

When an operator has acquired a "feel" for the machine and the task, these five aspects of the skill are developed and there is no need for him to stop and think to operate the machine once the task is defined. Whereas for an inexperienced operator considerable mental effort is required, and pauses and errors are made. The main users of the machines tend to be farmers who do not run the machines all the year round but only intermittently for maintenance tasks. Therefore they do not develop and maintain the level of proficiency of, for example, a full time operator employed on a larger machine. Let us now look in more detail at the tasks for which the machine is used.

For digging it is often required to cut holes with flat bottoms or sides and in rough, uneven ground it is not always easy to

judge vertical and horizontal planes by eye. Having filled the bucket in making a cut, care must be taken not to allow material to tip from the bucket by closing or opening it too far in moving it to the point where the spoil is to be dumped.

In ditching there are two cases to be considered: the cutting of new ditches and the cleaning out of existing ones. For new ditches it is desirable to keep the sides straight and smooth and to maintain a constant profile along the length of the ditch, moving the tractor along from one cut to the next. For clearing existing ditches the process is more one of piecemeal attention to local obstructions.

Trenching involves the cutting of a channel in line with the direction of travel of the tractor and at a constant pitch. This tends to be a very repetitive process and care must be taken to maintain a constant slope on the trench bottom.

The levelling of ground is effected in two stages: firstly using the bucket blade to shift peaks of ground into troughs, then a smoothing process using the bottom of the bucket to flatten the ground. For the inexperienced operator there are two main difficulties: the very precise combined control of the valves to obtain linear bucket movement and the judging of the location of the level plane to be achieved.

When loading the operator is often picking up material from level ground and the need then arises to move the blade in the plane of the floor. Having filled the bucket, it is necessary to

adjust the bucket angle as the machine moves so that material does not spill out through its being too far open or closed.

2.3 Potential Functions, Advantages & Limitations of Computer

Control

The first question which must be asked is whether the operator could be replaced by a computer controlled system. There are strong technical, economic, and social arguments against trying to do so. The control system would have to have a visual sensing system and very sophisticated intelligent software to interpret and execute instructions for anything other than a repetitive task without obstructions or irregularities to accommodate. In addition an interface to the tractor would be required adding to the cost and introducing considerable safety problems. It is socially undesirable to increase unemployment, particularly if there are no economic benefits in automation.

Potential gains in learning time, accuracy, and speed of completion many tasks may be made if the process of combining control functions in order to effect linear movements of the bucket blade is automated. In addition similar gains may be made in automatic compensation for the hydraulic and mechanical coupling of the arms tending to deflect the blade of the bucket from the intended path. So rather than have control lever axis correspond to particular ram speeds they correspond to particular directions of bucket blade travel. For cutting the sides of ditches, sloping ground, and the bottoms of trenches a calibrated control of the inclination or pitch of bucket blade movement is desirable. The blade may then be set to cut at any desired angle relative to the machine.

For repetitive tasks, e.g. trenching, an automated digging cycle would allow the operator to concentrate on driving the tractor once the cutting cycle had been "taught" to the machine manually. The mechanical constraints of the machine are unaffected by the control system, for example the maximum cutting force i.e. the load which will stall the machine. In automated digging cycles the machine is unable to correct automatically for the problem of earth falling back into the cut ditch, or to respond to the particular form of obstructions encountered.

2.4 Objectives and Functional Specification

With the availability of cheap microprocessors and electrohydraulic valves the general objective of the study was defined to develop and evaluate a microprocessor-based digger controller to assist the operator with many of the difficulties mentioned above.

From the discussion of machine usage the main areas which emerge where computer assisted control may be of value are:

1. Simultaneously controlling ram speeds to produce linear bucket movement.
2. Accurately gauging the pitch of sloping cuts.
3. Automatic repetition of taught cutting profiles.

A general advantage of electronic controls is that they enable

the operator to work the machine remotely as the control panel need only be connected to the machine by an electric cable. Thus an electronic unit is easier to install in the cab than conventional cable controls and may be used off the machine for better visibility and comfort provided appropriate safety precautions are taken. Control lever loads may also be considerably reduced from those required on a cable operated system or a system with levers mounted on the valve block, making the machine easier to operate.

The objectives then are:

1. To develop and evaluate a control system to provide these functions using the lowest level of technology suitable for the task to minimise cost.
2. To evaluate the functional benefits to experienced and inexperienced operators in terms of learning time reduction and work throughput.
3. To determine the economic viability of the system as a product.

The specification for the system is to achieve linear bucket blade movement by using the computer to create lift and reach functions which move the bucket blade in nominally horizontal and vertical, H and V, directions. The conventional machine gives to operator control of α , β , and γ (see Fig. 2-5(a)) whereas the computer system gives control of x , y , and θ . The

slew control is the same on both systems. The bucket angle is kept constant relative to these axes as the blade moves. To cut slopes at defined pitches one may rotate the axes in Fig. 2-5(b) through a pitch angle variable from $+45^\circ$ to -45° using a calibrated dial on the control panel.

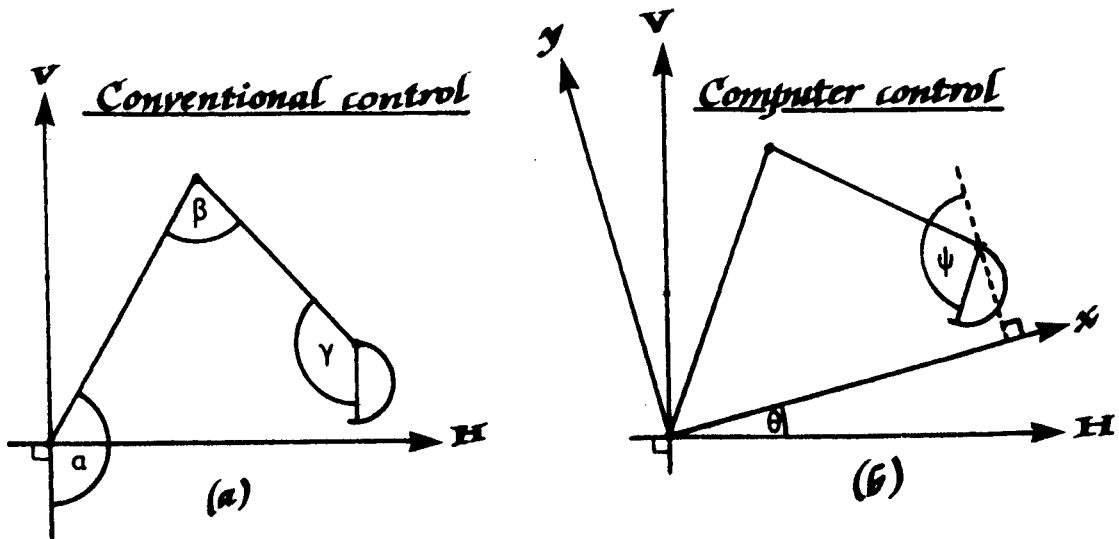


Fig. 2-5: (a) Conventional and (b) Computer Control Coordinates

For the automation of repetitive tasks it was decided to implement a learn and repeat facility operating in such a way that in Learn Mode the movements of the bucket blade from its initial position are recorded. When one of the repeat modes, Repeat Fast or Repeat Slow, is selected the stored path is executed from the new starting point (see Fig. 2-6).

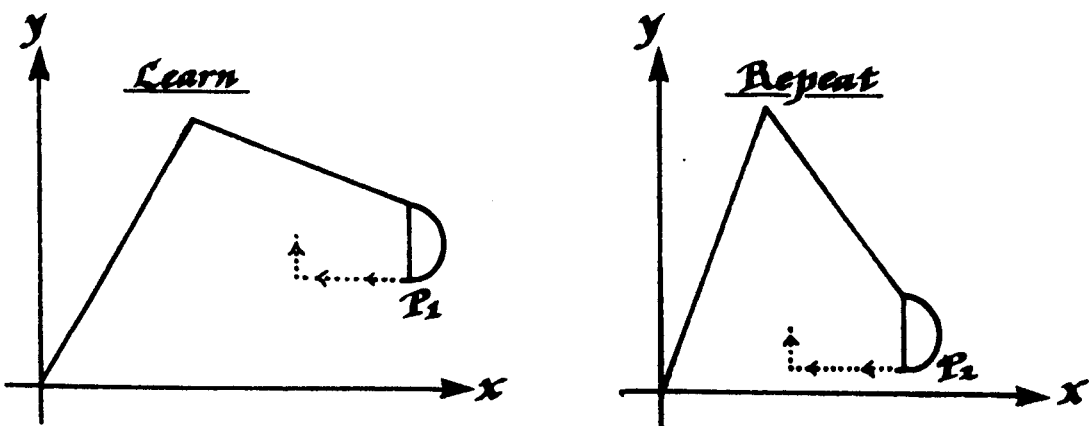


Fig. 2-6: Learn and Repeat Operations

2.5 Design Constraints

From a commercial viewpoint, manufacturing and components costs are major factors in considering the viability of a product. In order that the cost of any commercially produced electronic control system be minimised it is important that mechanical changes to the machine be kept as few and as minor as possible: the control system should be an optional fitting to an otherwise standard machine. It was decided to design the system keeping the cost of components to a minimum with the limits of the functional specification and the other design constraints with the overall view of having a working system which, with very little development or experimental work, could be put into production. Where possible in the design, standard, readily available parts should be used to minimise cost and availability problems in manufacture.

Typical agricultural working environments for electronic equipment are extremely harsh, and that of field machinery is the most demanding. As the system operates outside, protection must be given against water and damp to all parts of the system not mounted in the tractor cab. The entire machine is subject to continuous vibration from the tractor engine and the pump while the machine is in operation and there are additional shocks to the machine from the bucket when digging which must not affect the system operation.

All transducers must be weatherproof, damp-proof, unaffected by the vibration, protected from damage if they are

immersed as happens when cleaning ditches, and must be sufficiently mechanically robust to withstand contact with earth, stones, branches, and any other material encountered as the digger is used. The machine must be able to withstand wide range of operating temperature as the diggers may be used in all climates. The system must function in the range -10°C to $+35^{\circ}\text{C}$. The sealing and corrosion-proofing of the controller and transducers must be such that when the machine is stored for long periods no deterioration or corrosion occurs: it must work first time when switched on.

The power for the system is derived from the 12 V tractor supply and must be immune to drift in the supply voltage of ± 2 V according to the state of the battery. Spikes on the supply line from inductive loads must be filtered out and the system protected against the "load dump" phenomenon when the battery is accidentally disconnected from the alternator and a high current surge is applied to the 12 V line. The circuit must be able to withstand indefinite reverse polarity connection of the supply, have minimum current consumption, and be free from interference and electromagnetic noise.

The diggers are frequently attached to and detached from the tractor and the control system must be built to withstand rough handling and have reliable connectors. The control system must also be easy to service so that faults can easily be found and the construction such that system modules can be replaced when faulty by the operator. This necessitates some self-diagnostics to assist in detecting the faulty module. An important

ergonomic consideration is that the layout of the controls must be such as not to create difficulties for an operator already familiar with the conventional mechanical control system. This is achieved by having the x, y, bucket, and slew axes on the joysticks correspond to the reach, lift, bucket, and slew axes of the conventional machine.

As the system is experimental, the facility must be provided for altering the control software as well as having the facility for altering control parameters in the field without having to reprogram EPROM's for example. A production machine must be able to accommodate changes in the machine geometry arising from the use of different pivot positions, digging implements and rams. Also it should not be difficult to modify the system to accommodate future design changes in the mechanics of the digger.

As well as providing proportional control of the bucket blade cutting speed, the maximum speed available should correspond to zero relief valve oil flow so that machine power is not wasted. The dynamic characteristics of the machine should not be critically dependent upon the PTO speed which may not be well regulated by the tractor.

2.6 Method of Approach

As a first stage in the development of the microprocessor system it was decided to first construct a simple electric proportional control circuit functionally similar to the conventional mechanical control system. The construction of an electronic control unit for the machine involves the selection of

appropriate valves and a hydraulic circuit which can then be used as the basis of the microprocessor system interface. It was also considered to be of potential value by F.W. McConnel, Ltd. as such a system has advantages of reduced lever loads, ease of installation, and electronic simplicity. This preliminary system is the subject of the next chapter.

CHAPTER THREE

DEVELOPMENT OF MANUAL PROPORTIONAL CONTROLLER

- 3.1 Introduction
- 3.2 Selection of Electrohydraulic Valves
- 3.3 Hydraulic Circuit
- 3.4 Control Circuit
- 3.5 Performance Evaluation
- 3.6 Discussion

3.1 Introduction

The function of the manual or open loop controller is essentially to simulate conventional mechanical cable controls for the digger, but using electrohydraulic valves, giving a valve spool deflection and hence speed of arm movement varying with control joystick deflection. This forms a valuable basis for the microprocessor system as, having selected appropriate valves and developed a satisfactory hydraulic circuit for manual control, the valves may then be interfaced to the microprocessor in conjunction with appropriate feedback transducers to obtain the desired control functions described in Chapter Two.

3.2 Selection of Electrohydraulic Valves

There have recently been a number of developments in low cost electrohydraulic valves, particularly for use in computer based control systems. The standard valve to use for proportional flow control from a computer is a two stage electrohydraulic valve using a digital to analogue converter to drive the valve control input. The main spool position is controlled by a flapper valve, the position of the flapper being set by the actuating current. These valves are very fast, having a bandwidth over 100 Hz, and can pass high flow rates but they are also very expensive²³.

The Japanese manufacture digital hydraulic flow control valves with pressure compensators; the position of the flapper is controlled by a stepper motor and the main spool follows the flapper²⁴. The use of the stepper motor simplifies the interfacing of the valve to a computer. Another type of digital

valve which has been produced has a rotary spool positioned by a stepper motor. There are also being developed low cost spool valves with d.c. motor drives but these were not on the market at the time the work was carried out²⁵.

The cost of two stage valves suitable for use on the digger, with a flow rating of 0.3 l/s (4 g.p.m.) and pressure rating of 17 MPa (2500 p.s.i.) is in the order of £200 each. As the basic machine sells for approximately £3500 it was decided that the total cost to manufacture the microcomputer control system should be around £1000 maximum. Two stage valves were thus ruled out on a cost basis.

Experimentation using bang-bang solenoid operated valves showed that they are not suitable, as variable speed control is required and when bang-bang valves are used high acceleration changes occur in starting and stopping which could only be overcome by reducing the maximum speed to a prohibitively low level. The possibility was also explored of pulsing bang-bang valves on and off with a view to getting proportional control by varying the mark-space ratio. This did not work however: at low frequencies the pulsing caused the machine to oscillate and at high frequencies the valve latched on or off.

In view of the high cost or lack of availability of the types of valve discussed above it was decided to initially use proportional solenoid valves as supplied by A & D Fluid Power Ltd. which cost £50 each. A section through the valve is shown in Fig. 3-1²⁶.

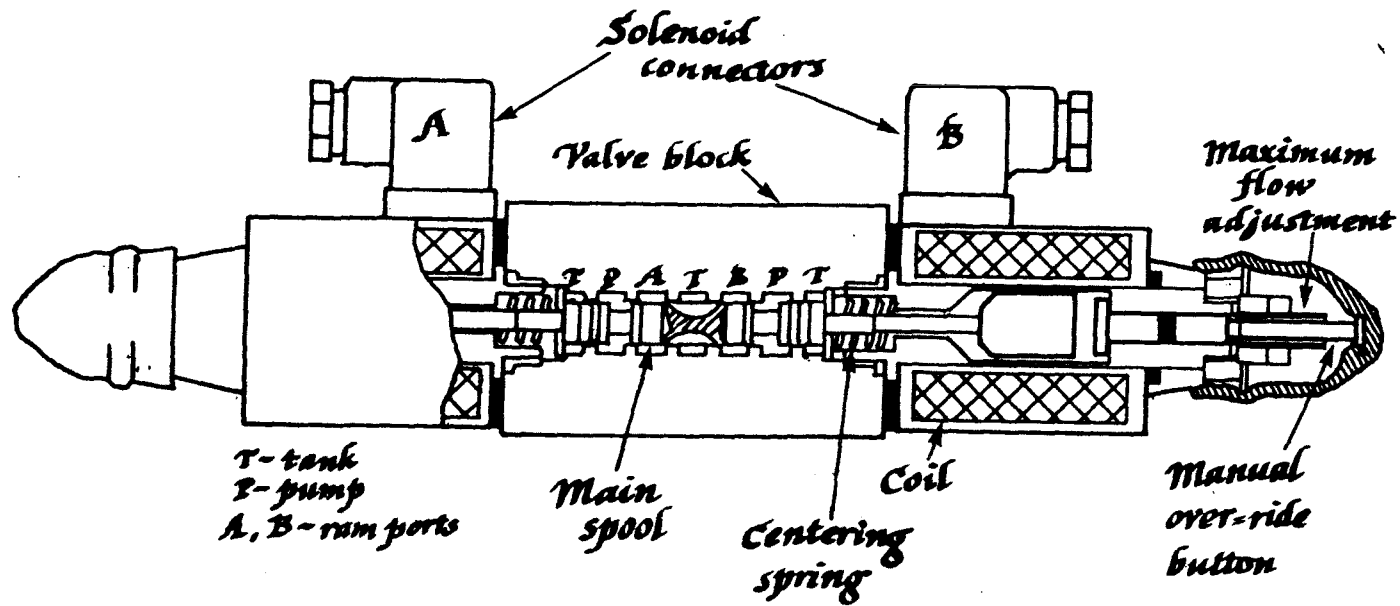


Fig. 3-1: Section through Proportional Solenoid Valve
 (Redrawn from data sheet with kind permission
 of A & D Fluid Power Ltd.)

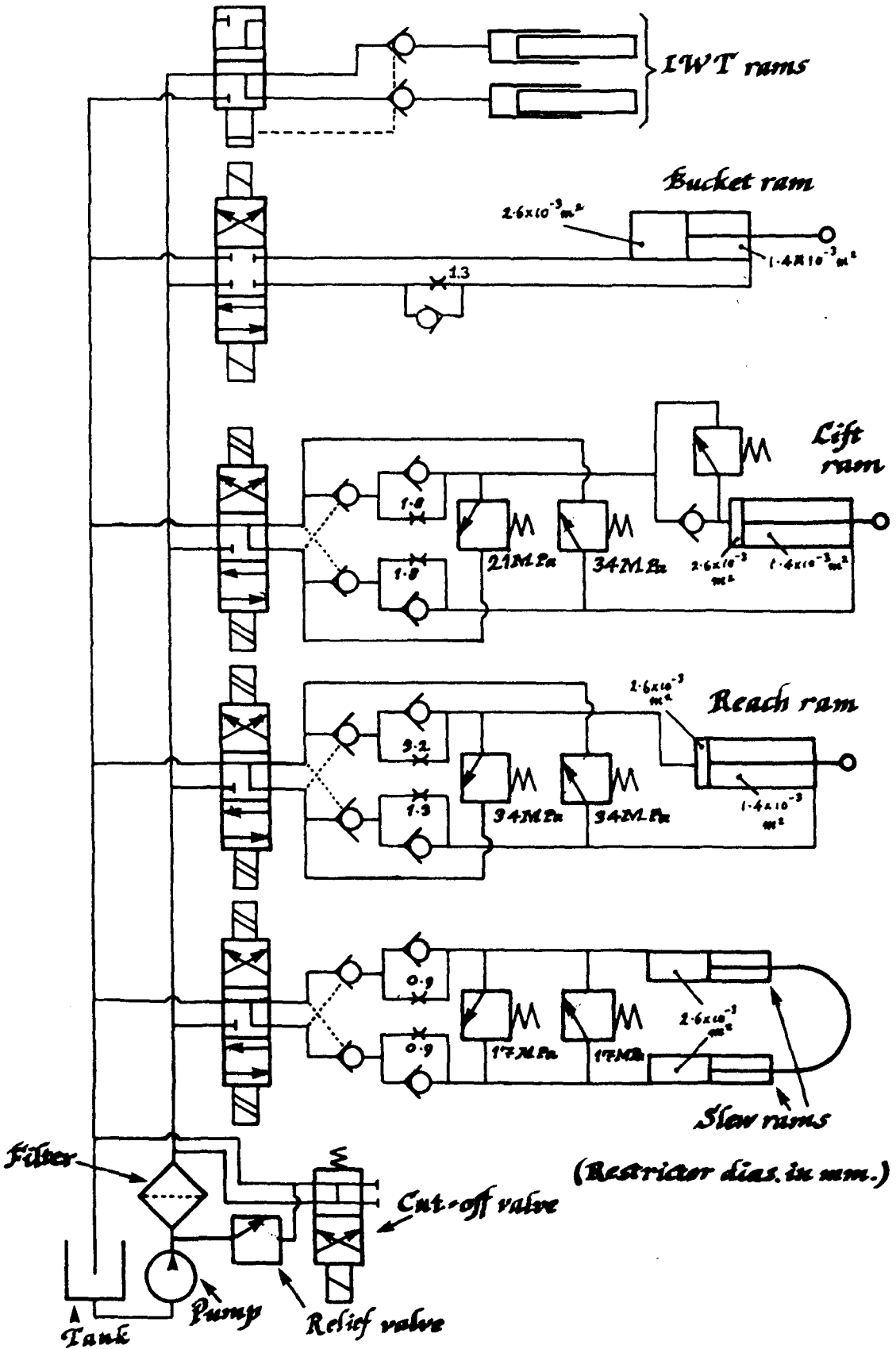
The valve comprises a valve block with a sliding spring centred spool which can be moved either way by a pair of solenoids. By controlling the mean solenoid current and hence the solenoid force, the spool position is continuously variable. In the past this type of valve, which has a bandwidth from 0 to between 10 and 20Hz, has not been used a great deal. The reason being that flow reaction forces and stiction effects tend to give the device high hysteresis and poor repeatability. These can be overcome by the use of stronger springs and more powerful solenoids but this increases the power consumption and heating effects.

An alternative means of improving the valve performance, employed in the A & D valves, is to drive the solenoids from a pulse width modulator circuit which pulses the current through the coils and gives variable spool deflection by varying the mark-space ratio. The frequency of the pulse train is set to vibrate the spool about a mean position determined by the mark-space ratio so as to minimise stiction effects. The solenoids are rated at a nominal 8 V, 28 W and were run at a frequency of 50 Hz. Also the spool is machined so as to be balanced and to minimise flow reaction forces at the orifices.

3.3 Hydraulic Circuit

The hydraulic circuit²⁷ for the digger employing the electric valves is given in Fig. 3-2. When none of the services is selected, the cut-off valve is open allowing oil from the pump to flow straight back to the tank. When any of the services is selected the cut-off valve is closed, the supply pressure rises

Valve actuators: Manual
 Pilot operation..... Bang-bang
 Coupling..... Proportional



(Restrictor dias. in mm.)

Fig. 3-2: Hydraulic Circuit for Electric Proportional Control

and fluid flows through the valve from the supply line and through the two check valves to one port of the selected ram. Simultaneously the output from the ram flows through the corresponding restrictor and the pilot operated check valve which is unseated by the supply pressure.

The valve metering occurs on the oil inlet side to the ram, i.e. the valve spool is of the "meter in" type. The bucket is operated using a bang-bang valve in conjunction with the one way restrictor which restricts flow into the gland end of the ram as the required maximum speed of bucket movement is relatively slow. The use of the bang-bang valve instead of a proportional valve introduces a cost saving and simplifies the control circuitry. On the lift service the one way relief valve which has an adjustable pressure setting, is connected to the base end of the ram to prevent cavitation as the arm moves down assisted by the strong gravitational force acting upon it. Without this relief valve, at low flows from the control valve, the arm was found to move down in a series of jerks as the pilot operated check valve between the base end of the ram and the return line opened and shut.

3.4 Control Circuit

A simplified schematic for the electronic circuit, just showing the control of the lift service and the cut-off is given in Fig. 3-3. The control voltage from the joystick potentiometer is subtracted from the output from the triangle wave oscillator by the summing amplifier. The output from the summing amplifier is fed to a pair of comparators, with threshold voltages V_{T1} and

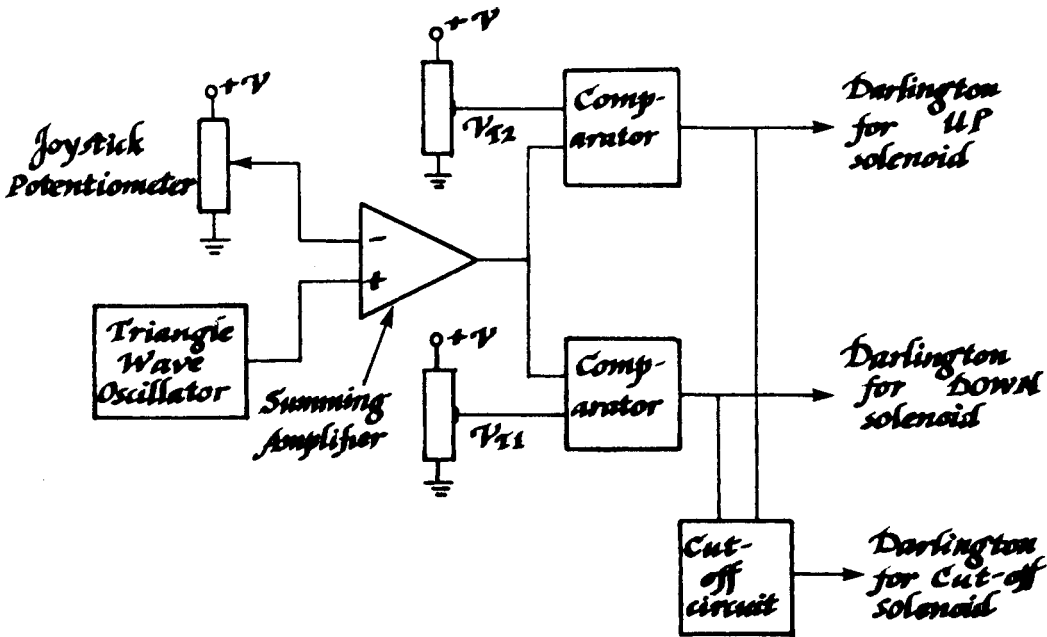


Fig. 3-3: Schematic of Control Circuit for Lift Service

V_{T2} , which switch the power transistors driving the proportional valve solenoids. As the joystick is deflected in one direction or the other from its central position the mark-space ratio of the

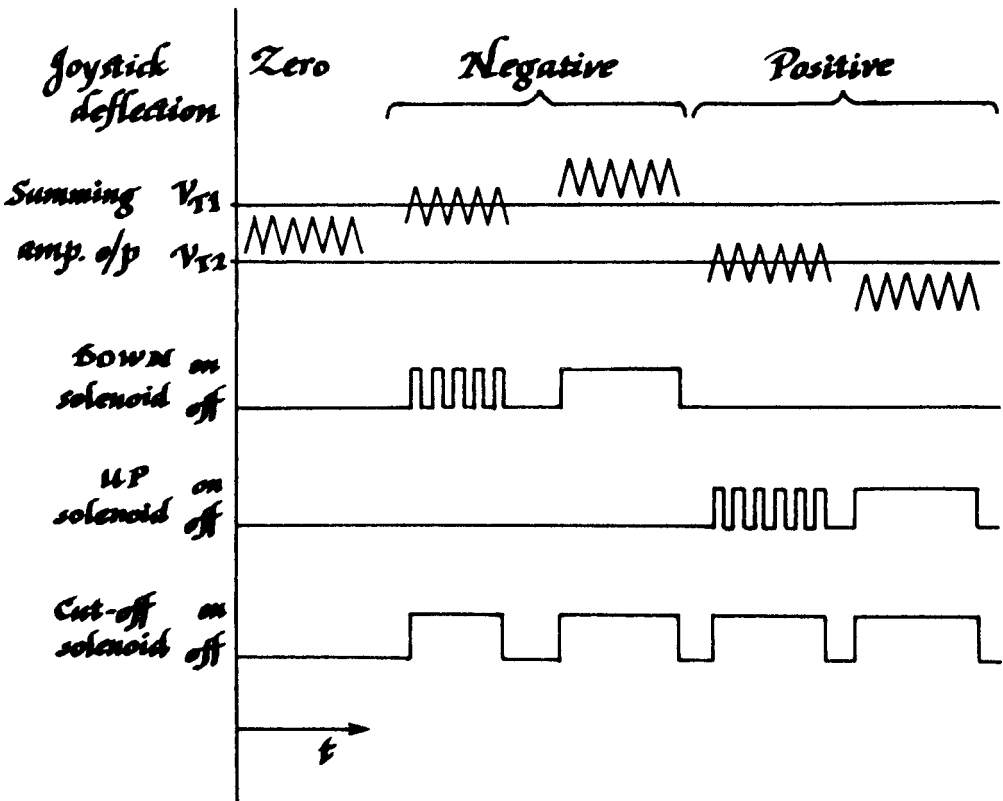


Fig. 3-4: Timing Diagram for Lift Service

current through the corresponding solenoid valve varies accordingly. When a solenoid is activated, this is sensed by the cut-off circuit which activates the cut-off solenoid closing the cut-off valve which is of the bang-bang type. The circuit operation is shown in Fig. 3-4; this shows the waveforms produced and the resulting solenoid switching for different joystick deflections.

The full circuit diagram is shown in Fig. 3-5 and the component values and specifications are given in Table 3-1. The power source for the circuit is the tractor battery, nominally 12 V, but which may vary between 10 V and 16 V. To provide a stable supply for the pulse width modulators and switching circuitry, a semiconductor regulator RG1 is used with feedback resistors R1 and VR1 to provide a stable supply (V+) of 8.2 V. Capacitors C1 and C2 provide smoothing for the regulator. Resistor R2 and Zener diode Z1 provide a 4.2 V reference for the triangle wave oscillator.

The oscillator is of relaxation type and comprises operational amplifier A1, potentiometer VR2, variable resistor VR3 and capacitor C3. VR2 and VR3 set the amplitude and frequency of the output waveform, taken from capacitor C3. The output is not a perfect triangle wave, as the capacitor voltage rises and falls exponentially, but it is a satisfactory approximation. The single oscillator circuit is used to drive all three pulse width modulators for the slew, lift, and reach services. The oscillator is set to give an output of 0.25 V peak to peak at 50 Hz.

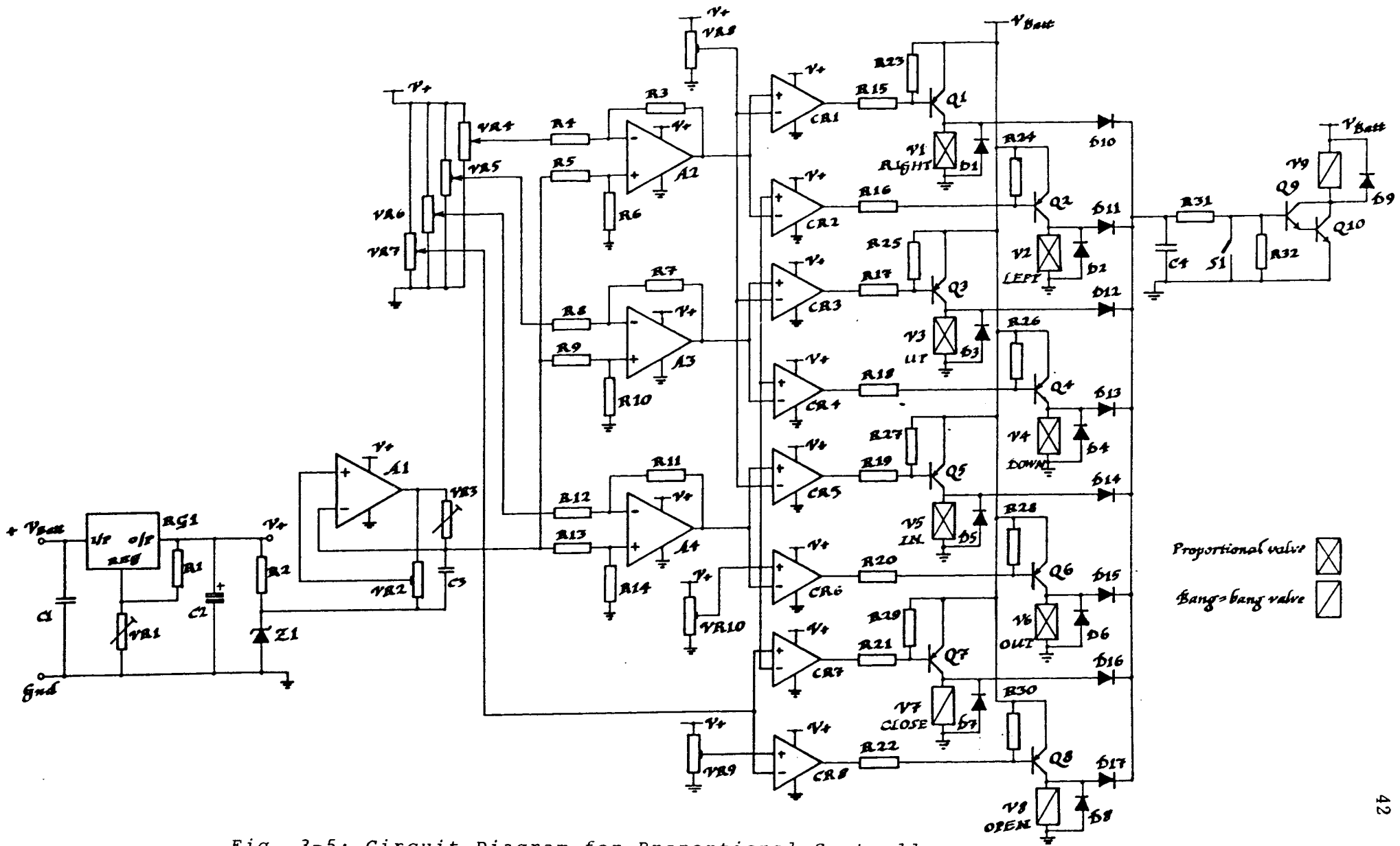


Fig. 3-5: Circuit Diagram for Proportional Controller

C1	100 nF		
C2	1 μ F Electrolytic		
C3	22 μ F		
C4	20 μ F		
VR1	5 k Ω 10 turn Cermet		
VR2	10 k Ω " " "		
VR3	2 k Ω " " "		
VR4-7	Type JS4 joystick from Flight Link, Alton, Hants.		Dropper resistors for pro- portional valves: 1 Ω 17 W
VR8-10	10 k Ω 10 turn Cermet		
R1	240 Ω 0.25 W Carbon	RG1	317K regulator
R2	120 Ω " "	A1-4	324 Quad op-amp
R3-14	68 k Ω " "	CR1-7	LM319
R15-22	460 Ω " "	Q1-8	BDX54C
R23-30	220 Ω " "	Q9	BFX85
R31	270 Ω " "	Q10	2N3055
R32	220 Ω " "	Z1	4.3 V 1.3 W
		D1-17	1N4001

Table 3-1: Components for Proportional Control Circuit

The joystick potentiometers VR4 to VR7 are in fact inductive devices manufactured by Flight Link Controls Ltd., and have an equivalent circuit of a potentiometer, with a 1.8 k Ω resistor in series with the wiper. The devices have no sliding parts to wear out, they are linear, noise free, mechanically robust, and very low priced at £15 for each dual axis unit. The devices give a 3V output for zero mechanical deflection and 0.8 V swing (10% of supply) each way.

The three unity gain summing amplifiers using operational amplifiers A2, A3, and A4 have the oscillator output connected to their non-inverting input and the slew, lift and reach control voltages to their respective inverting inputs. The output from each amplifier is fed to a pair of comparators, which detect when the control voltage crosses the threshold voltages for opening

and closing. The threshold voltages are provided by VR10 and VR9.

Comparators CR1 to CR8 have open collector outputs. Devices Q1 to Q8 are PNP Darlington pairs, drawn here for simplicity as single PNP transistors. R15 to R22 limit the base currents and R23 to R30 ensure that their corresponding transistors turn off. Diodes D1 to D9 connected across the solenoid coils suppress the inductive transients occurring when the current through the coils is turned off. In series with each of the proportional solenoid coils is a 1Ω resistor, between each coil and ground (not shown) to limit the current through the coils operating from the 12 V supply.

The cut-off valve V9 requires a continuous current to activate it as it is operated by a simple bang-bang solenoid. When any of the valves V1 to V8 is turned on, capacitor C4 charges through the base of Q9 via R31, turning on the Darlington pair between successive pulses of current through any of the proportional valves. R32 ensures that Q9 and Q10 do not conduct due to any leakage currents. Switch S1 is a safety switch mounted on the control box which prevents activation of the cut-off solenoid when thrown hence rendering the machine immobile.

The physical layout of the different sections of the circuit is shown in Fig. 3-6. The control cable, linking the control box to the junction box, only carries signal currents and the supply to the control circuit; the cable is also screened to

minimise electromagnetic pick-up. The heavy valve current switching takes place in the junction box to avoid interference with the control circuitry. The joystick axes and functions are aligned as on a conventional, mechanically controlled digger so that a direct comparison of performance could be made by experienced operators without their having to learn a new control configuration.

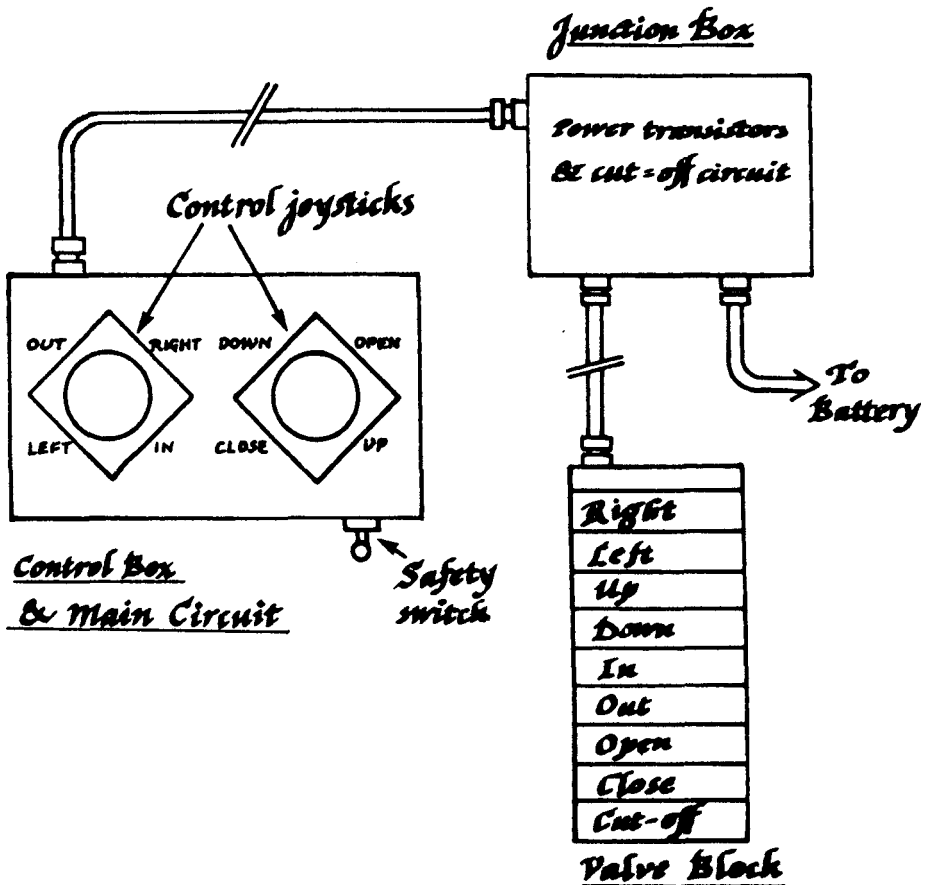


Fig. 3-6: Constructional Schematic of Proportional Controller

3.5 Performance Evaluation

The proportional manual control system was tested by the author and two experienced digger operators who performed machine evaluation trials for F.W. McConnel Ltd. The system was found to give controllability equivalent to that of a direct mechanical link from joystick to spool. Hysteresis effects in the

valve were not noticeable and the unloaded speed range of arm movement was the same as that on a conventional system ($\dot{\alpha} : 0 - 0.3 \text{ rad s}^{-1}$, $\dot{\beta} : 0 - 0.4 \text{ rad s}^{-1}$).

The operator lever loads were lighter which was an advantage and greater operator mobility was available as the control box is portable. A further advantage is that the control box may easily be installed in a tractor cab as it is only necessary to accommodate a single electric cable leading into the cab as against a set of heavy mechanical cables. The only disadvantage of the system was that the control box was difficult to support when used off the machine; a problem readily overcome by attaching a strap to each side of the box so that it may be worn around the neck.

3.6 Discussion

The proportional valves selected and hydraulic circuit, used in conjunction with the control circuitry described were found to give perfectly satisfactory control of the digger. This implies that, used in conjunction with appropriate feedback transducers and control algorithm the valves may be used satisfactorily for the microprocessor system to provide X-Y movement and a learn/repeat facility. The cost of parts for making the prototype circuit was £160 which is quite acceptable from a potential production viewpoint.

There are improvements to be made to the circuit, however. The proportional valves should be supplied from regulators deriving a steady 8 V supply from the battery. Also the power

switching, effected in the above prototype by the battery connectors, should be done using a relay in the junction box switched from the control box; this would add to the safety of the system.

The circuit has been redesigned to incorporate these features as well as modifications for the control of a type PA8 digger, a later machine, the king post of which may also be tilted level under electrohydraulic control.

CHAPTER FOUR

CONTROL SCHEME

- 4.1 Introduction
- 4.2 Kinematics
- 4.3 Generation of Target Point
- 4.4 Bucket Kinematics
- 4.5 Learn & Repeat
- 4.6 Transducer Resolution
- 4.7 Dynamics
- 4.8 Hydraulics
- 4.9 Mechanics
- 4.10 Control Algorithm

4.1 Introduction

The development of a control algorithm for a manipulator system falls into two main parts: kinematics and dynamics. The first concerns the derivation of the joint coordinates, and their necessary derivatives, in real time to execute the motion of the tool as demanded by the operator. The second, a potentially much more difficult problem, is that of implementing a control system to apply the necessary torques at the pivots to make the linkage follow the desired trajectory. With the growth in the use of industrial robots, a great deal of work has been done on the development of both kinematic and dynamic algorithms for manipulators.

4.2 Kinematics

There are two ways in which the input velocity command from the joysticks (x_i, y_i) may be used to derive the path to define the machine coordinate trajectory. By the first method, at each sampling instant the input velocities x_i and y_i are read and the equations relating the joint velocities to the input velocities are solved to provide inputs to joint rate servos:

$$\dot{a} = \frac{a}{x} \dot{x}_i + \frac{a}{y} \dot{y}_i$$

$$\dot{\beta} = \frac{\beta}{x} \dot{x}_i + \frac{\beta}{y} \dot{y}_i$$

This method, however, produces a trajectory subject to cumulative error as illustrated in Fig. 4-1. The machine starts at point S with the horizontal input vector shown. When the machine encounters an obstacle (shown shaded), a small positional error d arises which the system does not correct.

The desired trajectory is shown dashed with the maximum value of d as small as practicable so that the feedback system operates so as to maintain the machine on the original path.

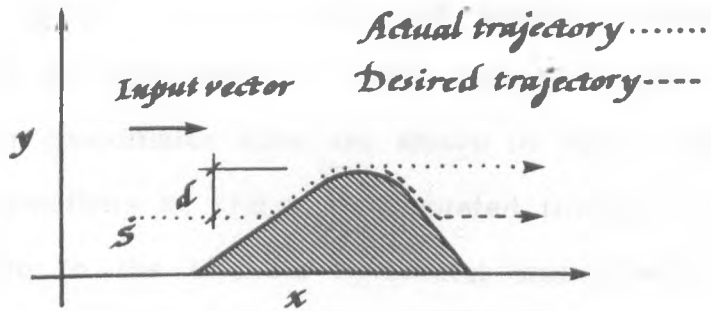


Fig. 4-1: Simple control scheme allowing cumulative error

The alternative method which overcomes the drift problem is to generate a 'Target Point' in software which follows the desired trajectory and to have a position control servo system to make the machine track the Target Point. This may be done, as here, by directly inverting the machine geometry (i.e. converting user coordinates to machine coordinates) or by Resolved Rate Motion control, particularly useful for reducing the computational load for complex linkages²⁸.

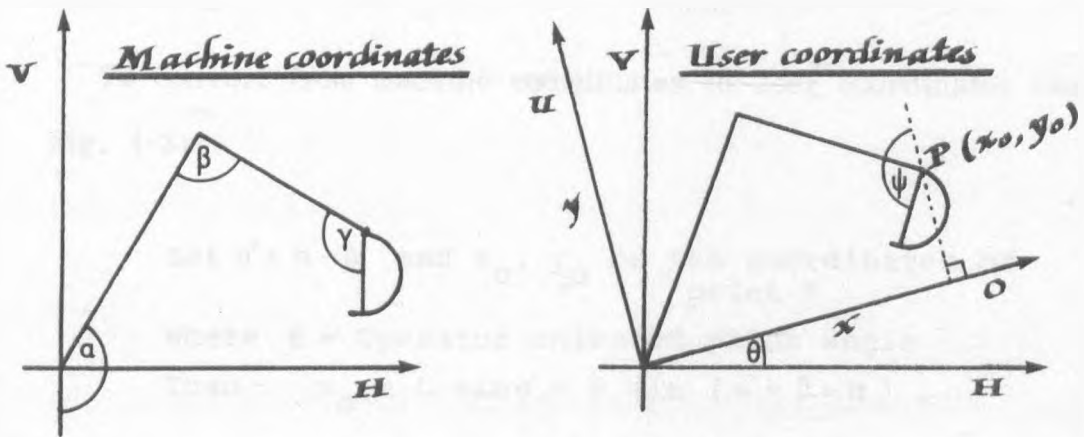


Fig. 4-2: Machine and User Coordinate Systems

To implement the control of horizontal and vertical bucket blade movement it is necessary to be able to convert machine

coordinates (i.e. angles measured at the pivots) to Cartesian user coordinates and to convert user coordinates to machine coordinates. The machine coordinates are shown in Fig. 4-2(a); H and V designate the horizontal and vertical directions in relation to the machine body, V being parallel to the slewing axis. The user coordinates axes are shown in Fig. 4-2(b); the Out and Up directions x, and y, are rotated through the pitch angle θ relative to the machine horizontal and vertical. The machine configuration is described by the x and y coordinates of the bucket pivot P and the bucket angle ψ , measured from the user vertical.

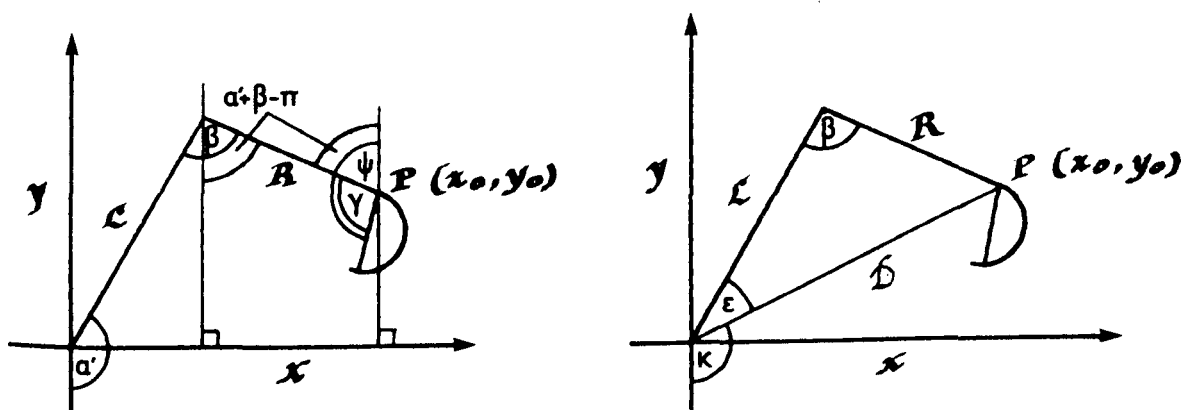


Fig. 4-3: Conversion between coordinate systems

To convert from machine coordinates to user coordinates (see Fig. 4-3):

Let $\alpha' = \alpha - \theta$ and x_0, y_0 be the coordinates of point P

Where θ = Operator selected pitch angle

Then $x_0 = L \sin \alpha' + R \sin (\alpha' + \beta - \pi)$

$y_0 = -L \cos \alpha' - R \cos (\alpha' + \beta - \pi)$

$\psi = \alpha' + \beta + \gamma - \pi$

To convert from user coordinates to machine coordinates:

$$D = \sqrt{x_o^2 + y_o^2}$$

$$\text{Let } A_1 = \cos^{-1} \left[\frac{L^2 + D^2 - R^2}{2 L D} \right]$$

$$\text{and } A_2 = \cos^{-1} (-y_o / D)$$

$$\alpha = A_1 + A_2 + \theta$$

$$\beta = \cos^{-1} \left[\frac{L^2 + R^2 - D^2}{2 L R} \right]$$

$$\gamma = (\psi + \pi) - (\alpha + \beta)$$

4.3 Generation of Target Point

If the machine is static and the joysticks are deflected to select x and y velocities \dot{x} , and \dot{y} , then the Target Point onto which the bucket pivot is servoed should move from the current output position at the selected velocity. When the input velocity is changed by the operator the Target Point should begin a new trajectory from the position of the machine at the time of the input change. It is necessary therefore to threshold a 'significant' change of joystick input otherwise the target point may be reset by the slightest unsteadiness of the operator's hand or by signal noise.

An additional consideration in determining the movement of the Target Point is what should happen if the machine is stalled by an immovable obstacle. It is necessary to stop the movement of the Target Point when the positional error exceeds a critical value determined by the characteristics of the control scheme.

4.4 Bucket Kinematics

In moving the bucket pivot in the x and y directions the control system must act in such a way as to maintain a constant bucket angle ψ . To do this it is necessary to feedback the angle γ by means of an appropriate transducer. Rather than mount a transducer on the bucket pivot where it may be vulnerable to physical damage it was decided to mount it so as to measure the angle δ and from this to derive γ .

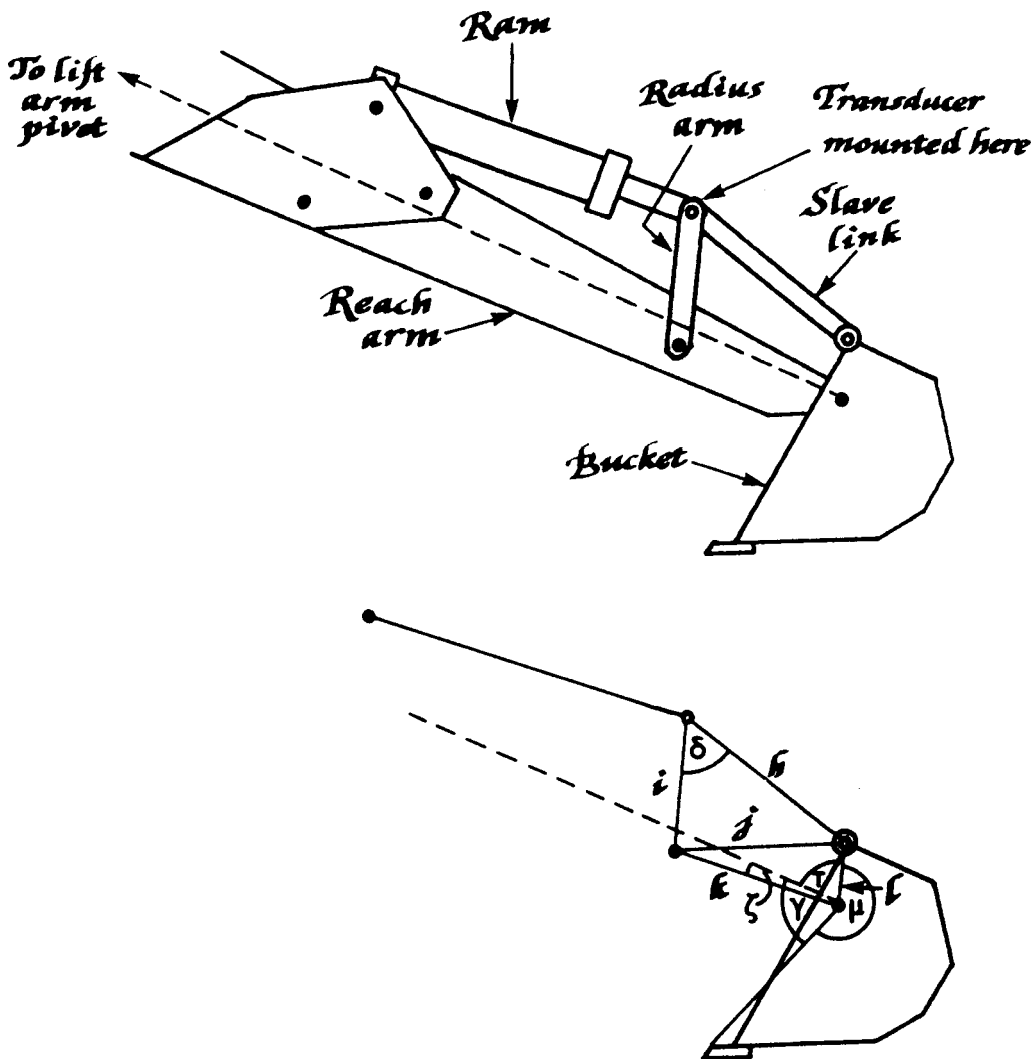


Fig. 4-4: Bucket Linkage and Geometry

The relationship between γ and δ may be derived as follows
(See Fig. 4-4):

$$j^2 = (h^2 + i^2 - 2 h i \cos \delta)$$

$$\tau = \cos^{-1} \left[\frac{k^2 + l^2 - j^2}{2 k l} \right]$$

$$\gamma = 2\pi + \xi - (\tau + \mu)$$

The dimensions of the bucket linkage are as follows:

$$i = 0.228\text{m} \quad \xi = 2.83^\circ = 0.049 \text{ rad}$$

$$h = 0.335\text{m} \quad \mu = 136^\circ = 2.37 \text{ rad}$$

$$l = 0.164\text{m}$$

Hence:

$$j^2 = 0.164 - 0.153 \cos \delta$$

$$\tau = \cos^{-1} \left[\frac{0.104 - j^2}{0.091} \right]$$

$$\gamma = 3.96 - \tau$$

$$\therefore \gamma = 3.96 - \cos^{-1} (-0.660 - 0.153 \cos \delta)$$

4.5 Learn and Repeat

The function of the Learn facility is to record the movements of the bucket blade from the starting position when the Learn mode is selected to the moment it is deselected. In Repeat mode, the blade cuts the same path as executed in Learn mode relative to the x and y axes but offset to the new starting point, being the position of the machine when repeat mode is selected.

There are two basic ways in which the Learn process may be executed: one method is to record points of the path at regular intervals in time and the other is to record points at even spacing. The first method retains information on the velocity of the blade whilst the second does not. However to record the speed of movement as the path was taught is not particularly useful as an operator may deliberately slow down certain parts of the learned operation to perform them accurately whilst such speed reduction in Repeat mode may be undesirable.

The method of recording a path at regular spacing has other advantages. The method is more economic in terms of memory usage i.e. a longer path may be stored in a finite memory space. With a constant sampling frequency and finite memory space there would be a time constraint on the operator in executing the path in Learn mode which is obviated by regularly spaced sampling. Having equispaced points in memory facilitates speed control in Repeat mode as the repeat speed may be determined by the rate at which data is sequentially retrieved from the list of input points. It was decided to allow the operator a choice of two repeat speeds selected by switches on the control panel.

When Repeat mode is selected the offset to be added to the path points in memory is calculated by subtracting the x,y coordinates of the starting point on the path in memory from the current output position of the machine. The trajectory for the Target Point is then generated by accessing and offsetting the successive points in memory at a rate corresponding to the

selected repeat speed. The bucket angle at the successive points is unaffected by the change in starting point of the path and requires no offset.

Let successive points on the learned path be represented by vectors

$$\underline{L}_i = (x_{L_i}, y_{L_i}, \psi_{L_i}) \quad i = 1, \dots, n$$

Let the starting point for the repeat be

$$\underline{S} = (x_S, y_S, \psi_S)$$

Then Offset $\underline{O} = (x_S - x_{L_1}, y_S - y_{L_1}, 0)$

and repeat path points $\underline{R}_i = \underline{L}_i + \underline{O} \quad i = 1, \dots, n$

4.6 Transducer Resolution

A major factor in determining the minimum resolution required of the transducers for measuring α , β , and δ angles is the maximum acceptable positional error at the bucket blade. A worst case configuration for error in calculating the y coordinate of the bucket pivot arises when the machine is in the position shown in Fig. 4-5. The reach arm is fully extended, $\beta = 142.0^\circ$, and $\alpha = 105.4^\circ$ then $\frac{\partial y}{\partial \alpha}$ and $\frac{\partial y}{\partial \beta}$ are at maxima and $y = 0$. For eight bit resolution of α and β the worst case error in y is 15 mm.

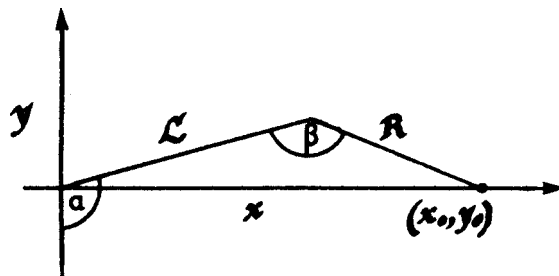


Fig. 4-5: Position for worst case error in determination of y coordinate

Thus positional resolution of eight bits is quite sufficient for digging purposes; the additional error introduced by quantisation of the bucket angle may be neglected as the bucket pivot to blade distance is relatively small.

4.7 Dynamics

Having established the kinematic requirements of the system and solved the machine geometry, a control scheme of minimum cost and complexity was sought which would give satisfactory performance. For the purpose of analysis the machine to be controlled may be divided into the sections of hydraulics and mechanics, including load.

4.8 Hydraulics

The complete hydraulic circuit for the control of digger using A & D Hydraulics' proportional valves is given in Fig. 3-3. The sections for the supply and the Lift service are shown in Fig. 4-6. The accumulators C_A and C_B represent the compliances of the hoses supplying the ram. This example of the Lift service is taken as it is the most complex individual service in the circuit. Given the valve setting V_L and the ram velocity \dot{X}_L , the ram force F_L and the flow Q_L may be found computationally as follows. Consider the case where the valve deflection is negative:

$$P_{RB_n} = P_{RB_{n-1}} + \frac{1}{C} Q_{CB_{n-1}} \Delta t$$

Where subscripts $n-1$, n denote successive samples at interval Δt

$$Q_L = K_V V_L \sqrt{P_S - P_{RB_n}}$$

$$Q_{CB_n} = Q_L - A_A \dot{x}_{L_n}$$

$$P_{x_n} = \frac{1}{C} Q_{CA_{n-1}} \Delta t + P_{x_{n-1}}$$

$$Q_{CA_n} = -A_A \dot{x} - R_A \sqrt{P_{x_n}}$$

$$P_{RA} = P_{RV} + R_A \sqrt{P_{x_n}}$$

$$F_L = P_{RA} A_A - P_{RB} A_B$$

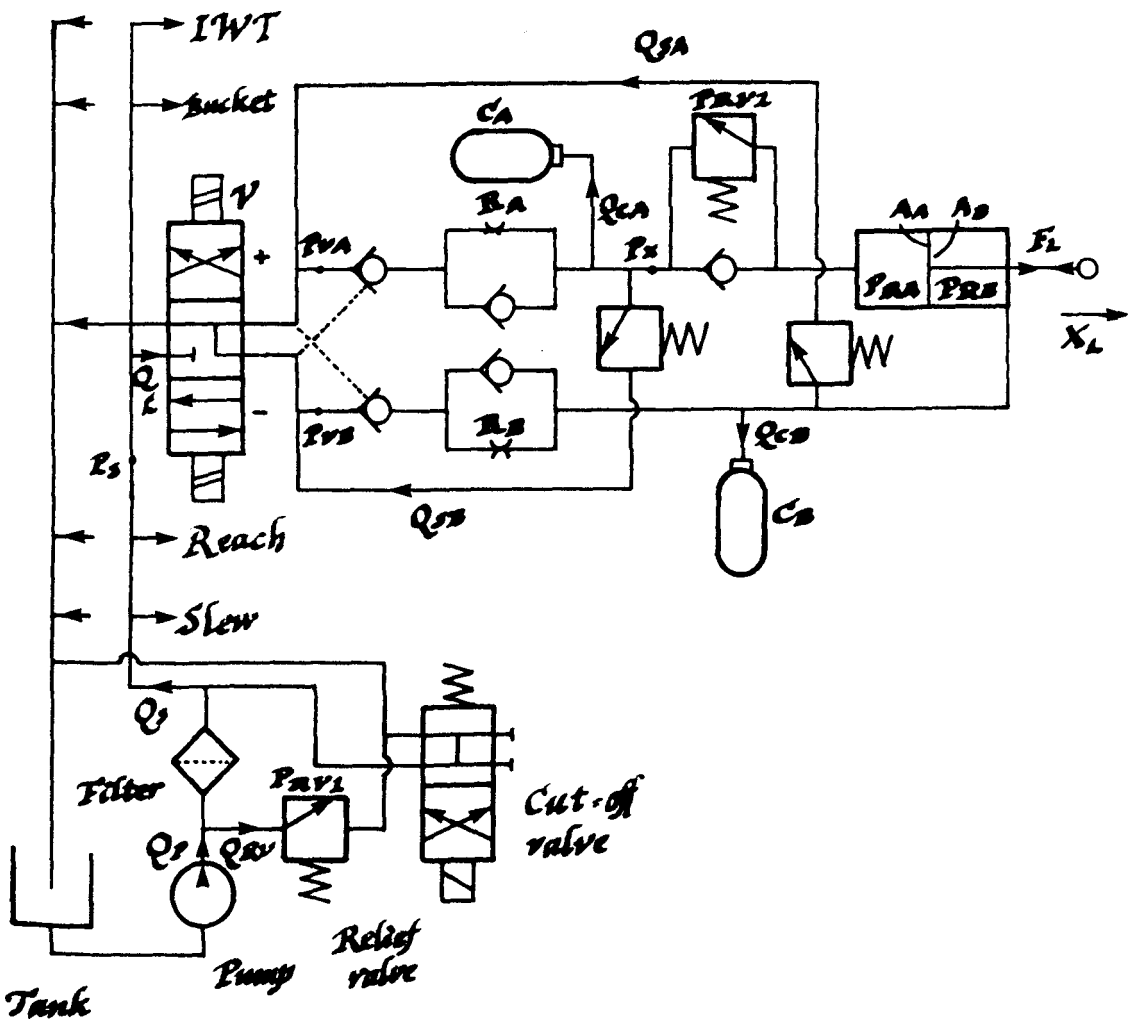


Fig. 4-6: Hydraulic Circuit for Supply and Lift Service

Similar sets of equations may be drawn up for each of the other services. The supply, comprising the pump and the relief valve, is governed by the following equations:

$$Q_P = Q_S + Q_{RV}$$

$$Q_{RV} = 0 \quad \left| \quad P_S < P_{RV1}$$

The value of P_S may be found at each sampling instant by performing an interval bisection type iteration varying P_S from 0 to P_{RV1} until the flow continuity constraint is satisfied:

$$Q_S = Q_{SLEW} + Q_{LIFT} + Q_{REACH}$$

$$+ Q_{BUCKET} + Q_{IWT}$$

It may be seen from the above that the hydraulic circuit is highly non-linear with saturation effects and interaction between the services. In addition there is the offset, hysteresis, leakage and dynamics of the valves to accommodate. The pump rate is subject to variation due to mis-setting and tractor governor imperfections. The oil viscosity changes significantly with temperature (changing effective restrictor and valve constants) becoming lower as the oil heats up and making the machine move noticeably faster.

4.9 Mechanics

In modelling the mechanics of the digger, in general, the following forces and corresponding torques must be considered:

1. Accelerational
2. Gravitational
3. Centrifugal
4. Frictional
5. Stictional
6. Coriolis

For very complex robotic systems Lagrangian dynamics provides a systematic and efficient method for solving the equations of motion. For a digger with a relatively simple geometry, the equations may be written and solved applying Newton's Laws directly. For slow moving manipulators the inertial forces may be negligible and the device may be treated purely kinematically²⁸. Slow moving in this context means about 1 m/s or less and the maximum speed of motion of the bucket blade of the digger in a horizontal cut at mid reach is 0.5 m/s.

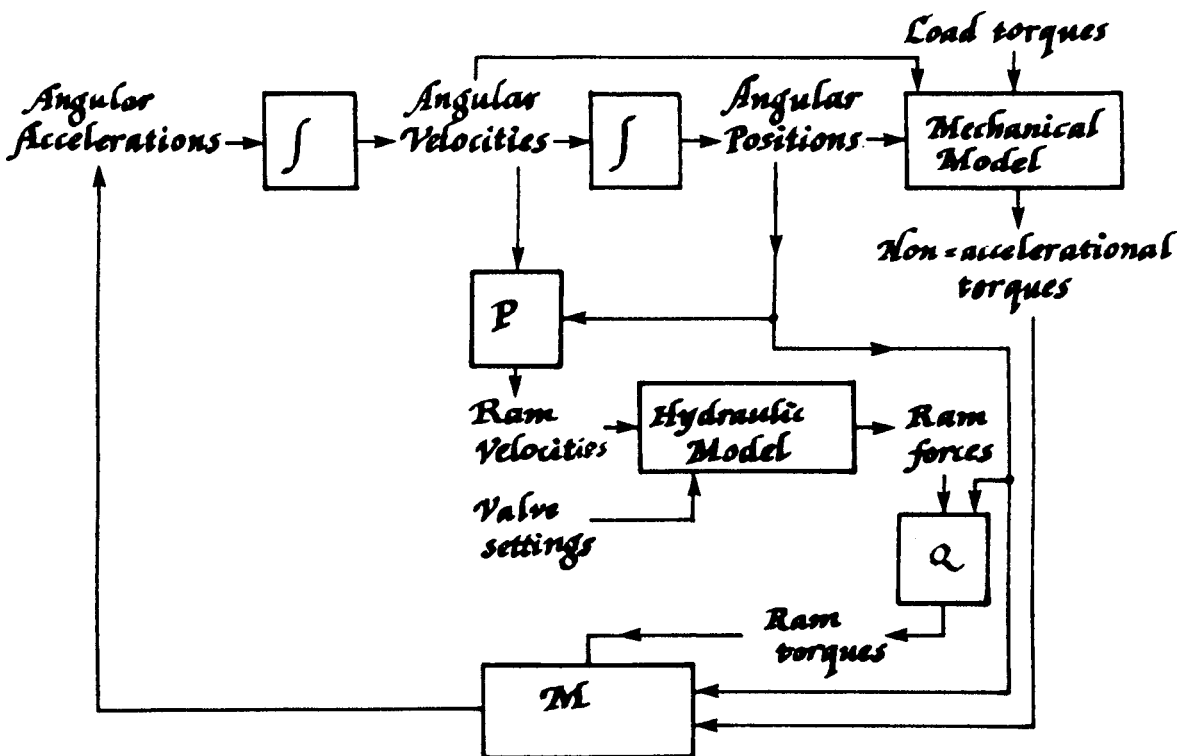


Fig. 4-7: Schematic of System Model

The overall structure of a complete model of the machine is shown in Fig. 4-7. The model operates by integrating the angular acceleration at each sampling instant to give velocities and positions; this data in conjunction with the load torques and valve settings enables the net acceleration torque to be calculated for the next sampling instant. Block P solves the geometry associated with each ram to convert the angular velocities at the pivots to ram velocities. This data is fed into the hydraulic model constructed as described above along with the valve setting to give the ram forces. Block Q converts the ram forces into angular torques at the corresponding pivots. The Mechanical Model M calculates the direct and induced torques listed above and hence the total non-accelerational torques using the basic laws of mechanics.

The derivation of the equations of motion is a lengthy but straightforward piece of mechanical analysis. The load forces acting on the bucket may change with position from that of a pure mass in the bucket to frictional forces as the blade cuts ground. To simulate a microprocessor controlled system care must be taken to include the effects of quantisation and finite word length arithmetic. It can readily be seen that the mechanics constitute a highly non-linear time-varying coupled system.

4.10 Control Algorithm

Two control schemes particularly suited to non-linear interacting robotic system are sliding mode^{29,30} control and invariant control²⁸. Both of the schemes require minimal information of the system to be controlled in terms of modelling.

Sliding mode control operates by switching between two control schemes which may be individually unstable chosen so as to keep the system in the region of a chosen switching line in phase space. Invariant control uses measurement of acceleration to eliminate the disturbances caused by the mechanical interaction of the joints to be controlled. Both these systems require additional transducers for measurement of velocity or acceleration in addition to sensing position, or a sufficiently well resolved position measurement to permit sufficiently accurate differentiation.

In view of the complexity of modelling it was decided to initially adopt an empirical approach to the development of a suitable control scheme. The most important question about the control scheme so far as the hardware specification is concerned is the number and type of feedback transducers required. Position, velocity, acceleration, and ram pressure are all variables required by different robotic control systems.

Early crude experimental work was carried out using a valve driver supplied by A & D Fluid Power, realising the scheme shown in Fig. 4.8 (a) using the apparatus shown schematically in Fig. 4.8 (b). Experiments were done using the lift arm as the linkage for this service has the highest moment of inertia about the pivot. An SDK-85 microcomputer was used to run a program to give proportional feedback using 8-bit integer arithmetic. An 8-bit digital to analogue converter was used to drive the analogue voltage controlled pulse width modulator supplied by A & D Fluid Power. This device was found to have

a varying frequency with control voltage.

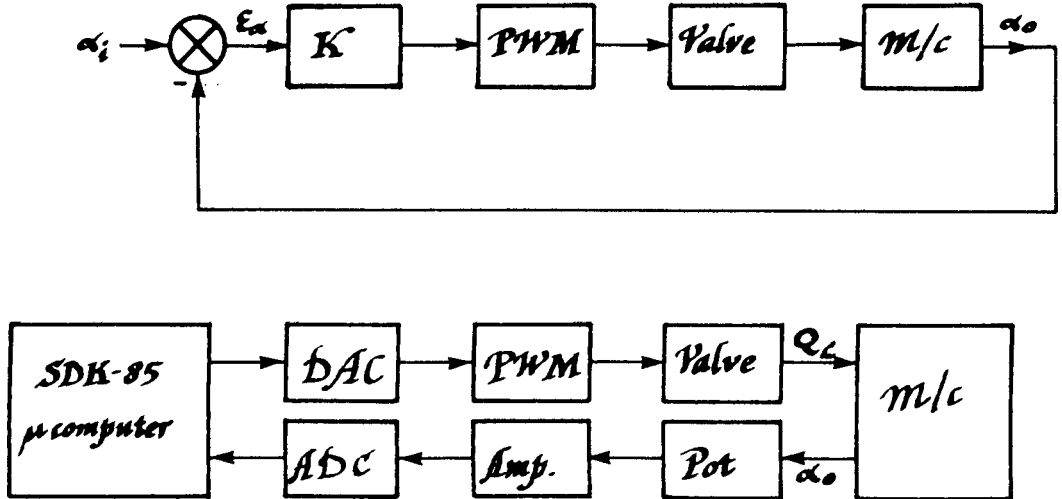


Fig. 4-8: Control Loop (a) and Hardware Schematic (b) for experimental system

A carbon potentiometer mounted on the spindle of the pivot was used to measure the output angle giving a voltage fed through a gain and offset stage to an 8-bit analogue converter. The resulting step response, by adjusting the gain K was fast and without overshoot similar to that of a first order system but had a small erratic residual error due possibly to non-repeatability of the valves.

It was decided therefore to start by building a system with more precise hardware to implement proportional control, adjusting the gains to obtain the fastest possible response without overshoot. The main effect of the hydraulic interactions is to reduce the gain of the services individually so if a gain is selected which gives a stable response for a service in isolation it will remain stable in conjunction with the other services. The faster the step response of the system, the better tracking is obtained to a ramp input.

Fig 4-9 shows a simplified schematic for control of the lift and reach (α and β) pivots to give x-y control of the bucket pivot. The control voltages V_x and V_y from the joysticks (J/S) are fed into the analogue to digital converter (ADC) to the computer. The corresponding velocities \dot{x}_i and \dot{y}_i are integrated to give x_i and y_i , the coordinates of the Target Point, onto which the bucket pivot is servoed. Code segment G calculates the corresponding coordinates α_i and β_i ; the corresponding errors are multiplied by the gain constants A_α and A_β and the results output to the pulse width modulators which drive the valves. It is necessary to prevent excessive errors accumulating if the machine encounters an obstacle that stalls it i.e. causes the relief valve to blow. This is detected by thresholding the x and y errors (ϵ_x and ϵ_y) and disconnecting the x_i and y_i inputs to the integrators when a critical error magnitude arises.

The controller for the bucket angle is shown in Fig. 4-10 (a). The overall effect of the system is to maintain the bucket angle constant in the user coordinate system as the bucket pivot is moved, this function being over-ridden by control signals from the bucket control joystick. With zero joystick deflection the Sample and Hold outputs the angle to be maintained to summing point S_1 which calculates the error signal which is used to switch the bucket valve. When the joystick is deflected the sample and hold is put in sample mode and becomes zero and the value of the joystick voltage is fed to the valve controller. When the joystick is released the sample and hold holds the value of the bucket angle at release which then becomes the new input to the regulator.

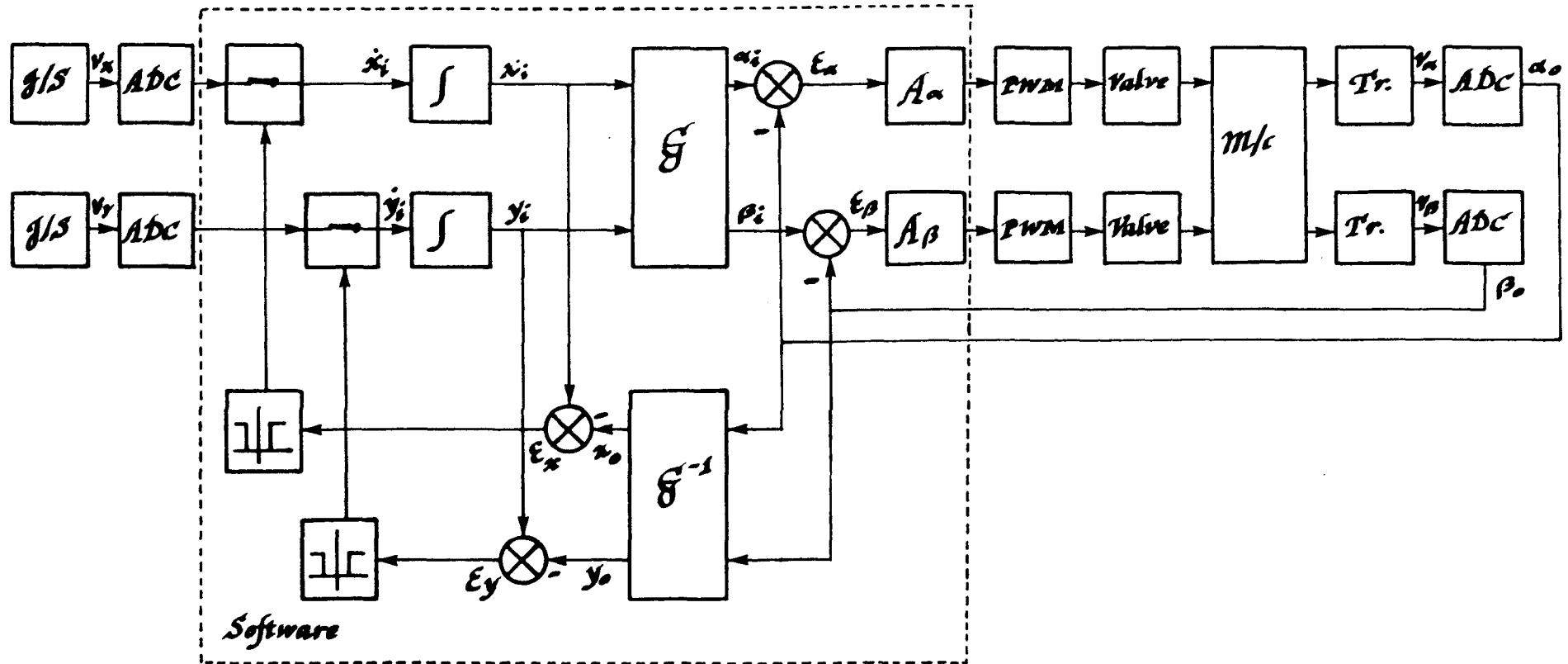


Fig. 4-9: Control System for Lift (α_0) and Reach (β_0)

The slew controller (see Fig. 4.10 (b)) is functionally equivalent to that of the proportional electric control system but implemented through the computer. The control joystick voltage V_s is fed to the ADC, multiplied by a gain constant A_Ω and output to the PWM to drive the valve.

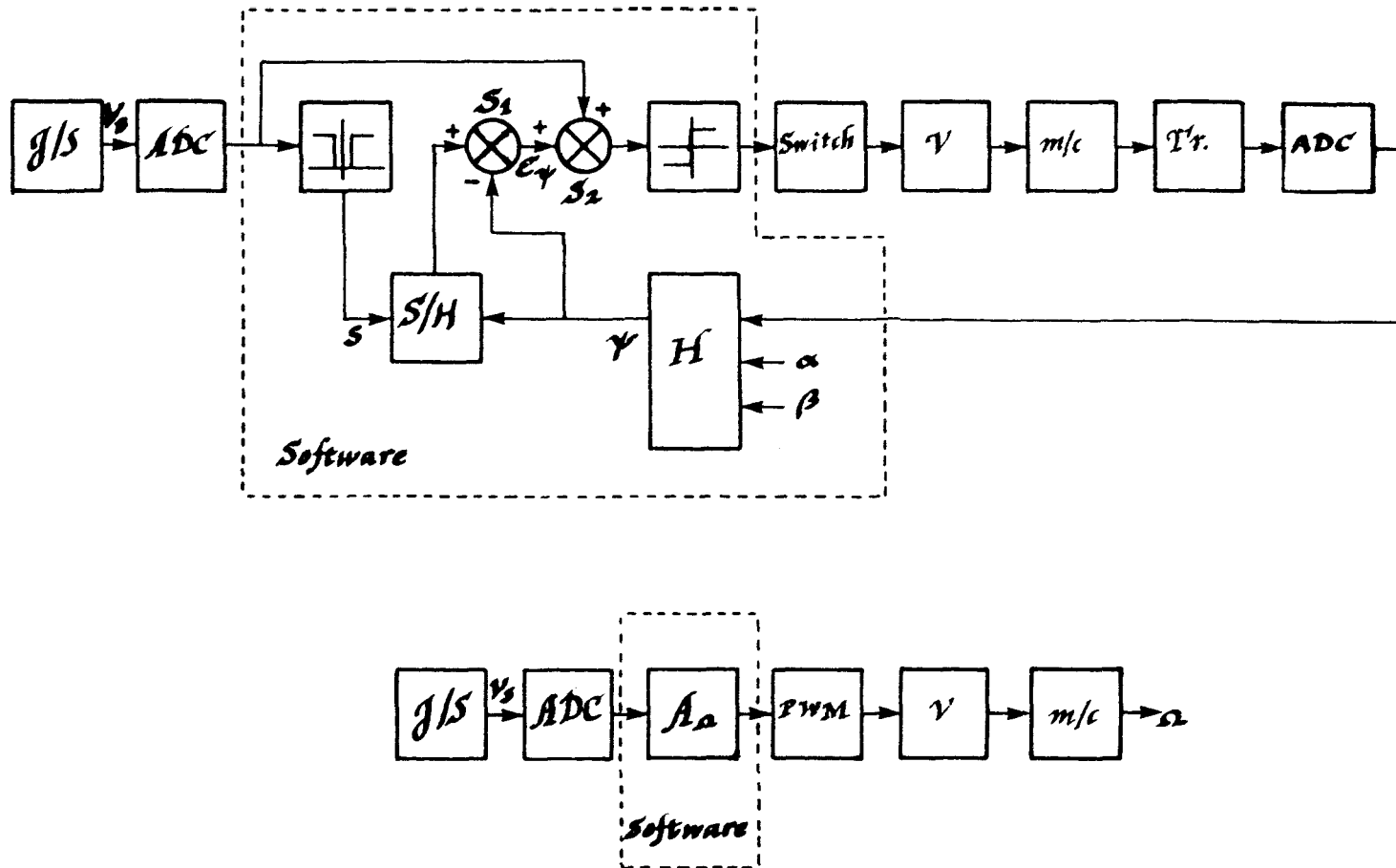


Fig. 4-10: Bucket Control Loop (a) and Slew Control Schematic (b)

CHAPTER FIVE

TRANSDUCERS

- 5.1 Design Constraints
- 5.2 Selection Possibilities
- 5.3 Construction

5.1 Design Constraints

With the availability of cheap microprocessors, a major part of the total hardware cost of a computer-based control system can lie in the feedback transducers. As the cost of the diggers is relatively low, the cost of the output transducers must be kept as low as possible.

The transducers must be able to give eight bit resolution over the measured angle of travel and must be repeatable to less than half a least significant bit. The devices used must also be mechanically robust: vibration is transmitted to the transducers from the tractor engine and from the pump. They are also subject to mechanical shocks from the bucket when digging. The transducers must be made waterproof to withstand weathering and mud splashes; the bucket transducer may even be immersed if the machine is being used for clearing waterlogged ditches.

They must be easy to fit to a standard machine in the sense that no significant mechanical modifications have to be made. They must also be able to withstand the rough handling of the agricultural environment as well as any impact in use if the machine hits an obstacle. All electrical connections must be well screened to prevent electromagnetic interference from other circuits on the machine (e.g. solenoid valves) or from nearby.

Easy access to the workings of the transducers is desirable for ease of servicing. Also it should be possible to replace any one independently of the others if a fault should arise.

5.2 Selection Possibilities

There exists a number of types of transducer commercially available for angular position measurement. The most simple to interface to a computer is an absolute encoder which gives a bit parallel output in binary or Gray code corresponding to the measured angle. The objections to using this type of encoder are cost and the number of wires to be connected to the computer. Connectors capable of withstanding the working environment of field machinery are expensive and the cost increases with the number of ways that are connected.

Incremental encoders overcome the problem of a large number of connectors but they are still relatively expensive and they must be re-datumed if the machine is switched off. Hydraulic rams exist which have capacitive transducers built in; they are well protected but have the disadvantage again of cost. The possibility was considered of using an ultrasonic pulse-echo technique to measure ram extension with the transducers mounted inside the ram. This was not pursued however, owing to the difficulty in finding a suitable piezo-electric material, the complexity of the driving circuitry, and the necessity for temperature compensation.

In view of the drawbacks with various other measurement systems it was decided to design a transducer using a high quality plastic film potentiometer. These devices have 0.5% linearity and virtually infinite resolution giving a calculated total worst case positional error of ± 26 mm.

5.3 Construction

The set of three transducers may then be interfaced to the computer using an analogue multiplexer and an analogue to digital converter. An exploded section through the device is shown in Fig. 5-1. The potentiometer is mounted on a steel ring attached by a brass strip to the transducer body; the strip is flexible to accommodate any mis-alignment of the potentiometer spindle relative to the spindle block.

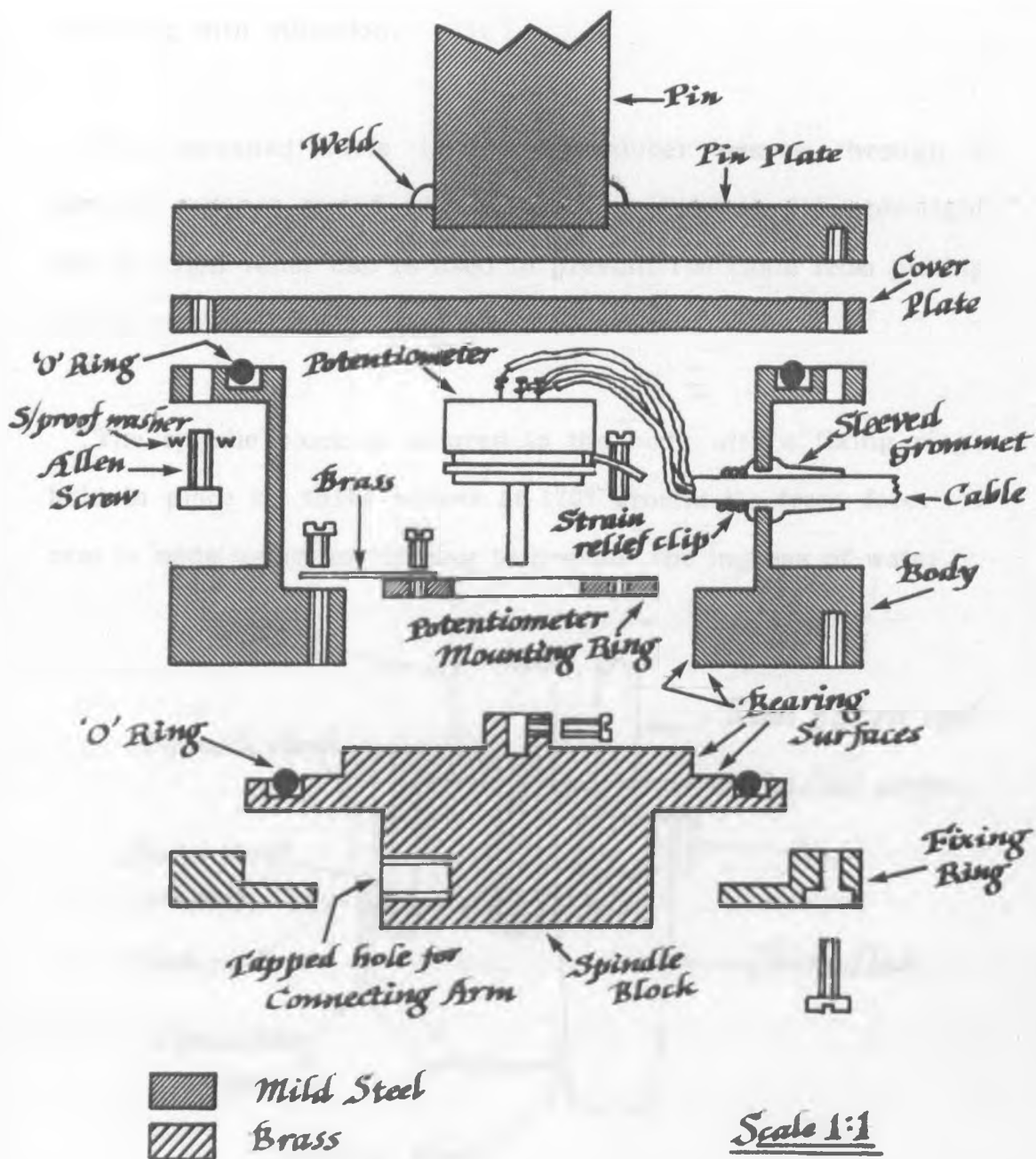


Fig. 5-1: Exploded Section through Transducer

The pin at the top of the diagram acts as the pivot for the two arms, the angle between which is being measured. The pin or pin plate is secured to one or other of the arms by a cotter pin or by a weld. The cover plate serves to protect the interior of the transducer if it is removed from the machine and there is a water-tight 'O' ring seal between the plate and the transducer body. The plate is secured to the body using an allen screw fitted with a shakeproof washer to prevent it from loosening with vibration.

The screened cable to the transducer passes through a sleeved grommet sealed with plastic glue to make it water-tight and a strain relief clip is used to prevent the cable from pulling out or stressing the potentiometer connections.

The spindle block is secured to the body with a fixing ring, held in place by three screws at 120° around its front face. A seal is made using an 'O' ring to prevent the ingress of water.

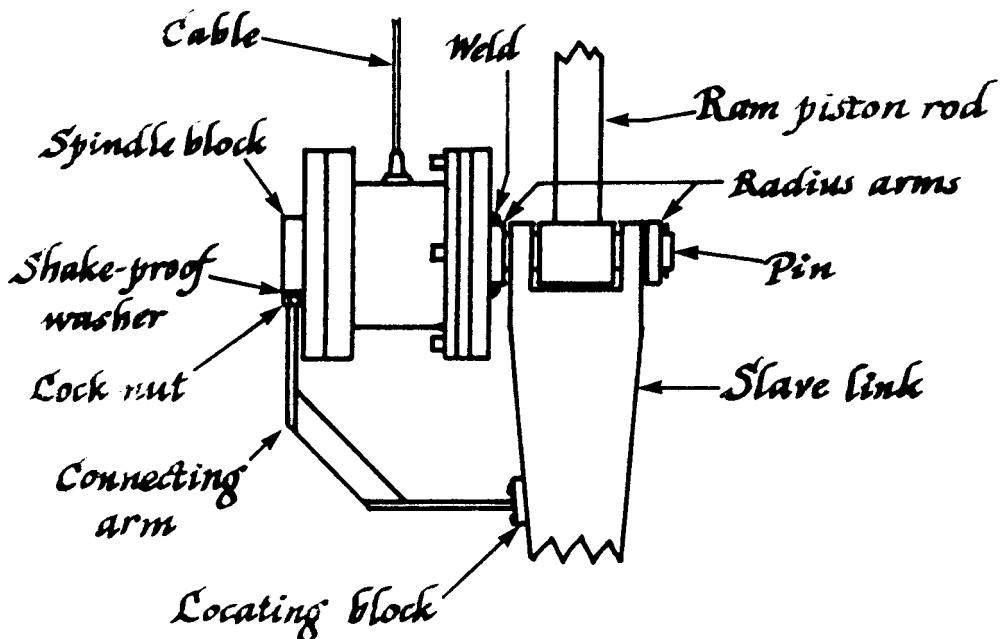


Fig. 5-2: Mounting of Bucket Angle Transducer

Fig. 5-2 shows a side view of the assembled transducer attached to the bucket linkage (see also Plate I). The pin plate is welded onto the radius arm of the bucket linkage to prevent the transducer body from rotating. The connecting arm engages in the slot in the locating block. The locating block is shown in detail in Fig. 5-3.

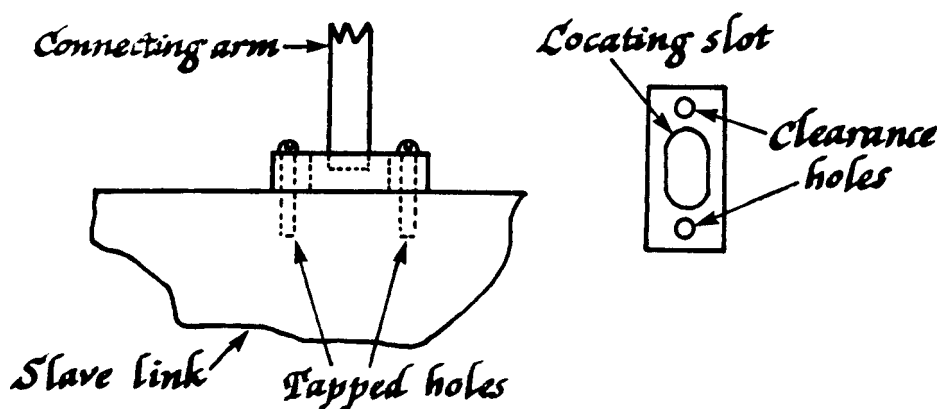


Fig. 5-3: Detail of Locating Block

The elongation of the slot serves to accommodate any movement of the transducer in the plane of the connecting arm due to pin wear. The space between the connecting arm and the slave link accommodates any movement axially along the pin. Plates II and III show the transducers fitted on the machine for measuring angles α and β respectively.

The locating pin shown in Plate II above the transducer prevents it from rotating; the junction box for the transducer connections can also be seen on the machine body. The pin for the transducer measuring angle β is fixed by a cotter pin to the lift arm.



Plate I: Bucket Transducer



Plate II: Lift Transducer showing Junction Box



Plate III: Reach Transducer

CHAPTER SIX

HARDWARE I:

SYSTEM STRUCTURE & PROCESSOR BOARD

- 6.1 System Structure
- 6.2 Processor Board
- 6.3 Memory Expansion
- 6.4 Arithmetic Processor Unit
- 6.5 Board Layout
- 6.6 Memory & I/O Maps

6.1 System Structure

A block diagram of the control system hardware is shown in Fig. 6-1. The system is based upon an Intel SDK-85 single board microcomputer. It uses an Intel 8085A microprocessor and the unit includes a hexadecimal keyboard, display, a monitor, and in its most basic form 2K of ROM and 256 bytes of RAM. The processor has an eight bit word length and is run on a 6 MHz crystal. The system is compatible with the Intel "Intellec" development system in the departmental microprocessor laboratory allowing the use of an in-circuit emulator for debugging hardware and for software development. The 8085A is also a widely available industry standard device.

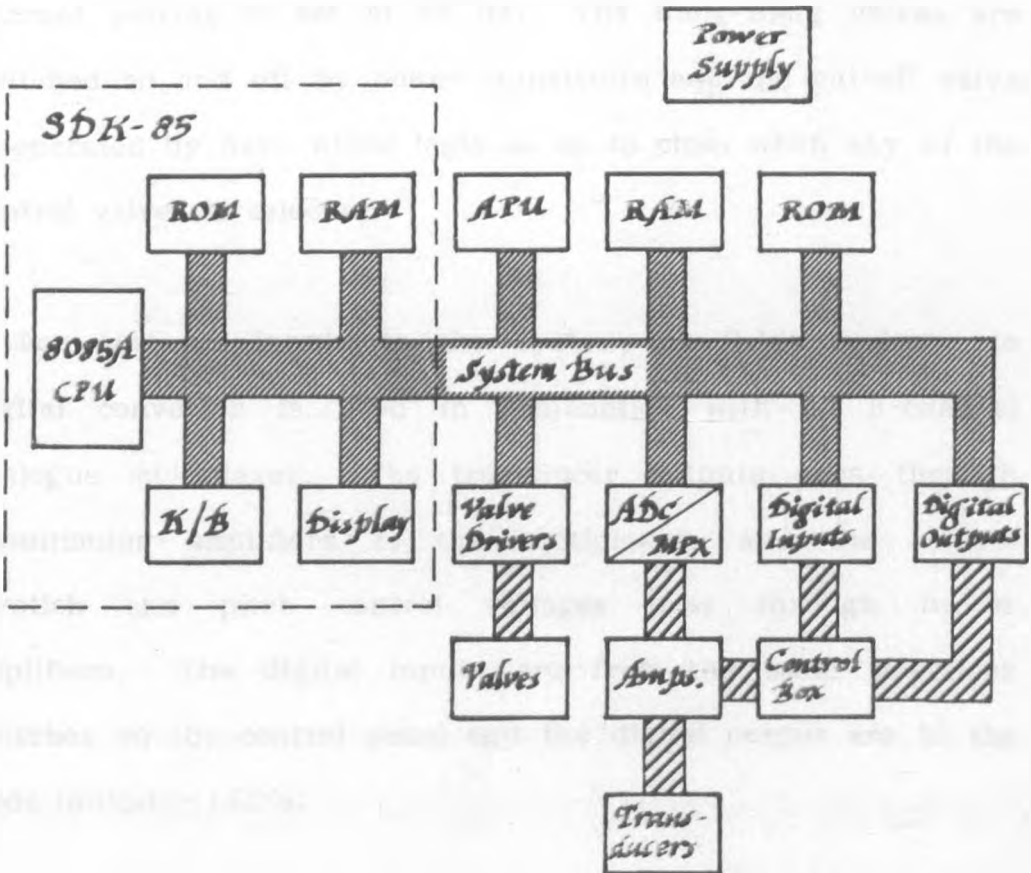


Fig. 6-1: Block Diagram of System Hardware

The memory was expanded to give a total of $4\frac{1}{2}$ K of RAM and 8K of EPROM.

The arithmetic processor unit (APU) is an Advanced Micro Devices AM9511 which will operate on 32 bit floating point data, as well as 32 bit and 16 bit integers. The device performs arithmetic and trigonometric operations and runs with a 3 MHz clock giving a maximum floating point multiply time of $56\mu\text{s}$.

The Valve Drivers interface the CPU to the proportional and Bang-Bang solenoid valves. The current through the proportional valves is controlled to seven bit accuracy, with an eighth sign bit, from zero to full, and the frequency of the current pulsing is set at 50 Hz. The Bang-Bang valves are switched on and off by power transistors and the cut-off valve is operated by hard wired logic so as to close when any of the control valves is selected.

For analogue inputs to the system, an 8-bit analogue to digital converter is used in conjunction with an 8-channel analogue multiplexer. The transducer outputs pass through conditioning amplifiers to the multiplexer, and the control joystick and pitch control voltages pass through buffer amplifiers. The digital inputs are from the mode selections switches on the control panel and the digital output are to the mode indicator LED's.

The power supply provides the 5V digital supply for the computer and logic circuits using the tractor battery as the

power source and employing smoothing circuits and regulators. DC to DC converters are used to provide the dual rail supplies to the amplifier circuitry and for the stable +12 V supply for the APU.

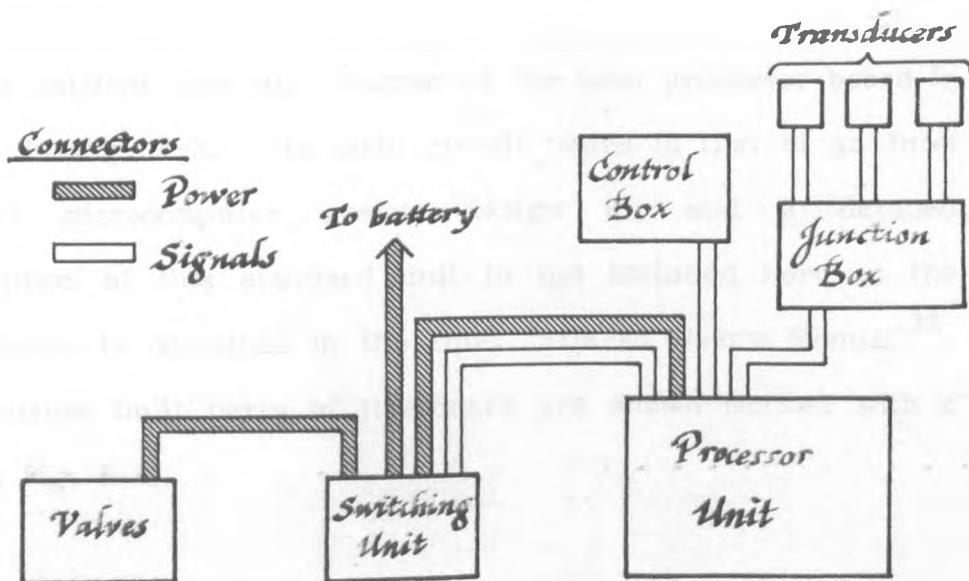


Fig. 6-2: Layout and interconnection of sub-units

The physical layout and interconnection of the different units of the controller are shown in Fig. 6-2. The transducers are connected by screened leads to a junction box mounted on the machine from which a single screened cable then runs to the processor unit. The control box, which houses the control joysticks, pitch control, mode selection and indication circuitry, is linked by a single screened cable to the processor unit.

The switching unit contains the main relay which switches the battery supply to the system on and off, activated by a switch on the control panel. It also supplies the regulators for the proportional valves and the power transistors for all the valves as well as the switching circuit for the cut-off valve. Two

cables link the switching unit to the processor unit: one is a screened signal cable for operating the valves and the other is the power cable for the processor unit.

6.2 Processor Board

The detailed schematic diagram of the main processor board is shown in Fig. 6-3. The main circuit board is that of an Intel SDK-85 microcomputer system design kit and a detailed description of this standard unit is not included here as the information is contained in the Intel "SDK-85 User's Manual"³¹. The custom built parts of the board are shown marked with a dot in Fig. 6-3.

The 8085A crystal which is normally supplied at 6.144 MHz is replaced by one of 6 MHz so that the AM9511 arithmetic processor unit may derive its clock signal of 3 MHz from the CLK pin of the CPU which produces a signal at half the crystal frequency.

The 8205 Address Decoder decodes the bottom 4K of memory into eight 2K blocks. The utilisation of each of the decoder outputs is shown in the Memory Map given below. The 2K Monitor ROM, to which control jumps on power on, may be replaced by an EPROM programmed to transfer control the the digger program stored in the 4K EPROM thus making the computer transparent to the user. To facilitate swapping of these chips, as the monitor is often required in experimental work, the board is fitted with a zero insertion force socket. The monitor ROM, or its substitute, and the two 8155 RAM and

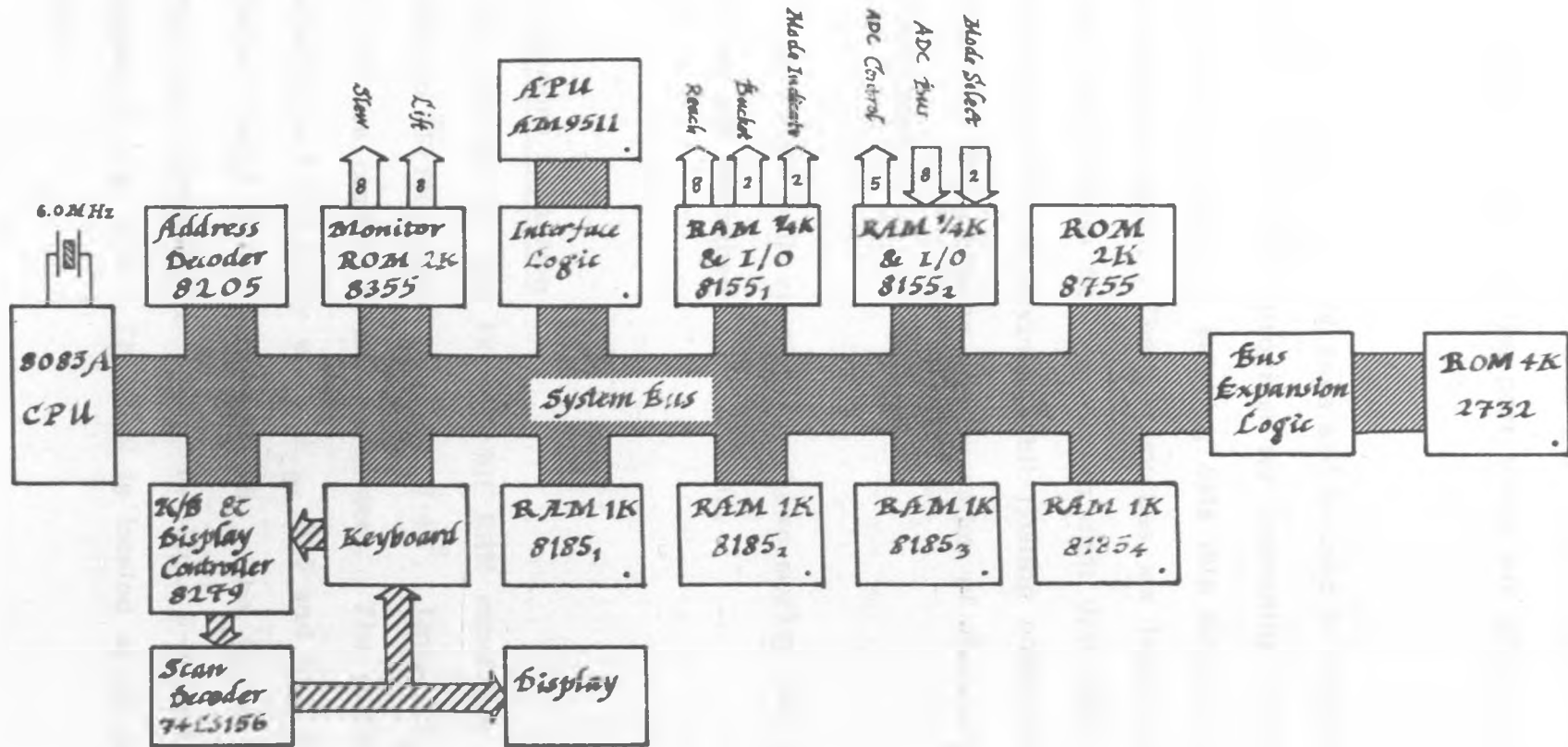


Fig. 6-3: Processor Board Schematic

I/O chips have bit programmable I/O ports used for interface to the valves, the ADC, and the mode selection and indication circuitry. Details of the port usage are given in the I/O map below.

The keyboard has 24 keys and is used in conjunction with the display and monitor program for inspecting memory locations and register contents, entering data into memory, and initiating program execution. The display has six hexadecimal digits: a four digit address field and a two digit data field. A program was written for displaying 32 bit floating point variables stored in memory for checking the operation of the programs during development.

The custom built circuits are shown marked with a dot in Fig. 6-3 and are described in detail later.

6.3 Memory Expansion

The circuit for the 4K x 8 bit RAM expansion for locations 3000H to 3FFFH is shown in Fig. 6-4³². Lines AD₀ to AD₇ and A8, A9 are common to all the devices. The additional address decoding is effected by using A₁₀, CS6 and CS7 and control is effected using ALE, RD, and WR. The 4K x 8 bit EPROM expansion schematic is shown in Fig. 6-5 and the circuit diagram in Fig. 6-6. The ROM is located at address 8000H to 8FFFH.

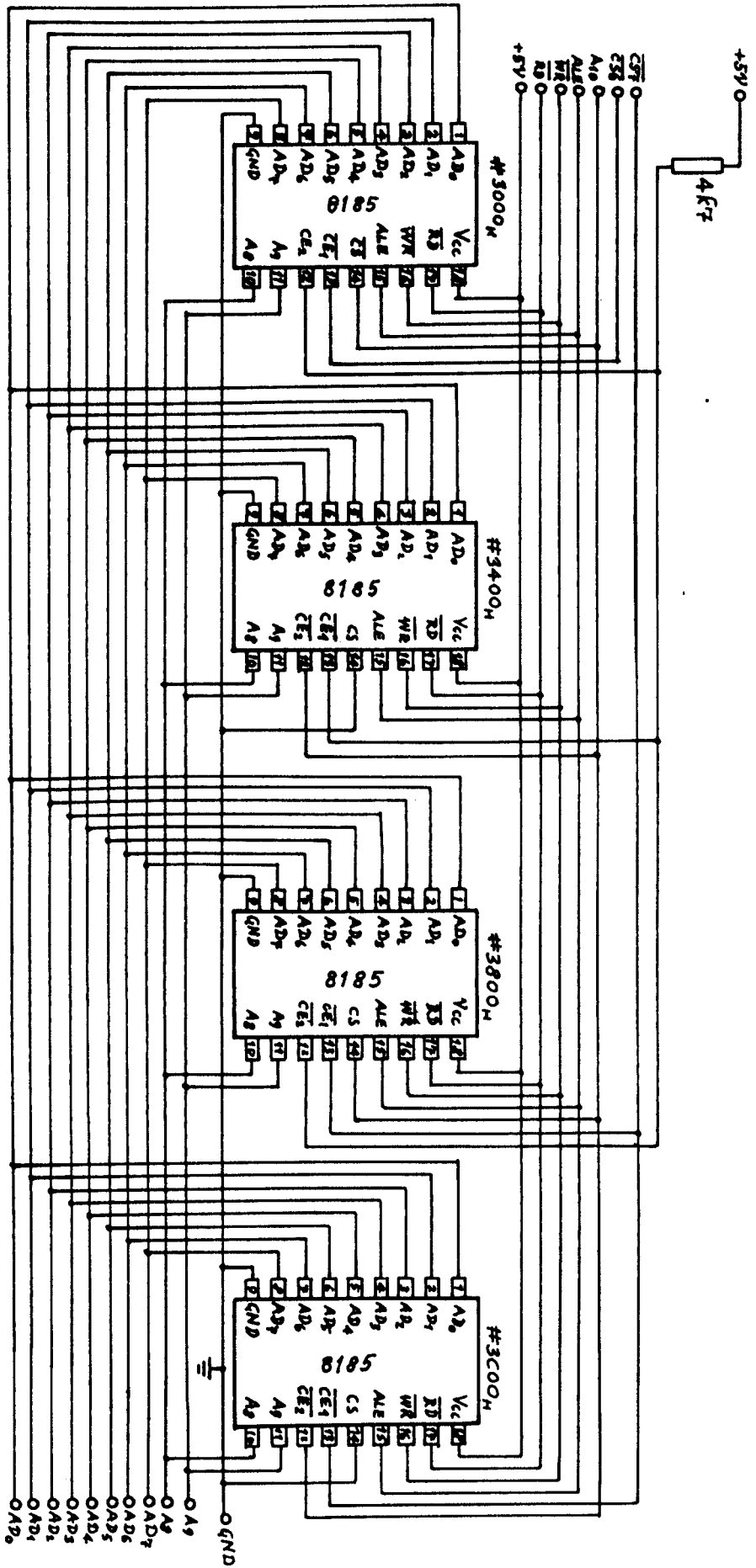


Fig. 6-4: 4K RAM Expansion Circuit

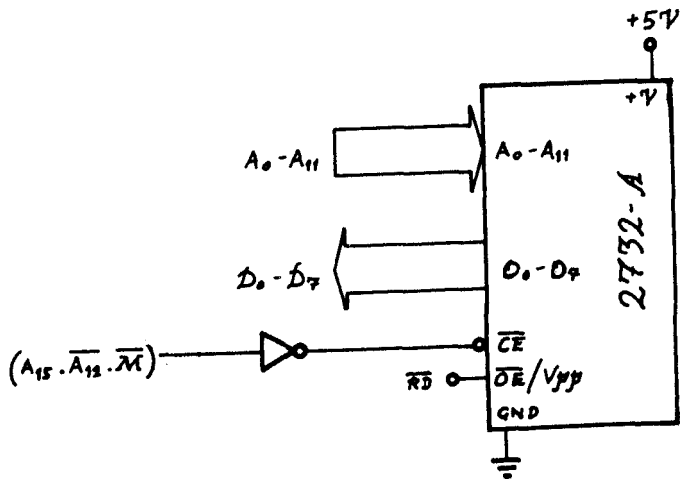


Fig. 6-5: 4K EPROM Expansion Schematic

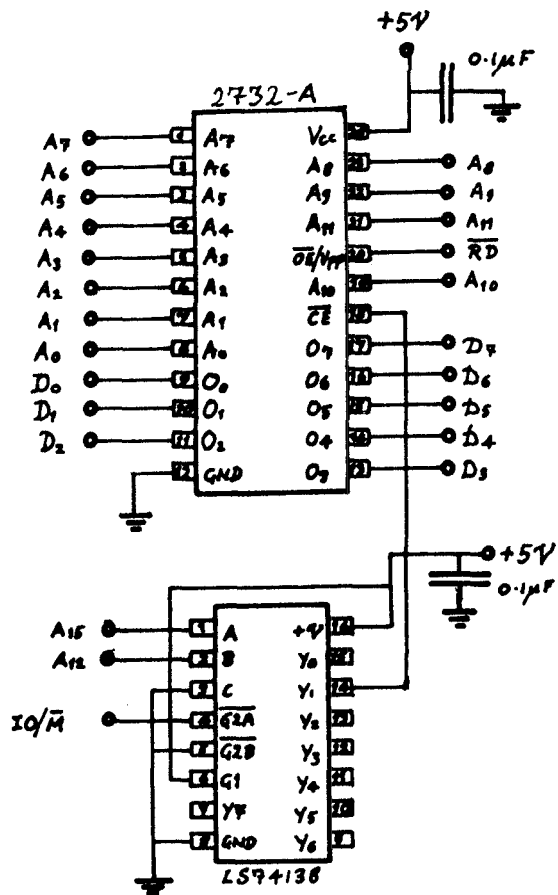


Fig. 6-6: 4K EPROM Expansion Circuit

6.4 Arithmetic Processor Unit

The arithmetic processor unit interface schematic is shown in Fig. 6-7. The APU has an internal stack to which data bytes are pushed and pulled, and a command/status register both accessed by the eight bit bidirectional data bus³³. The stack is located at address 1000H and the command/status register at address 1100H.

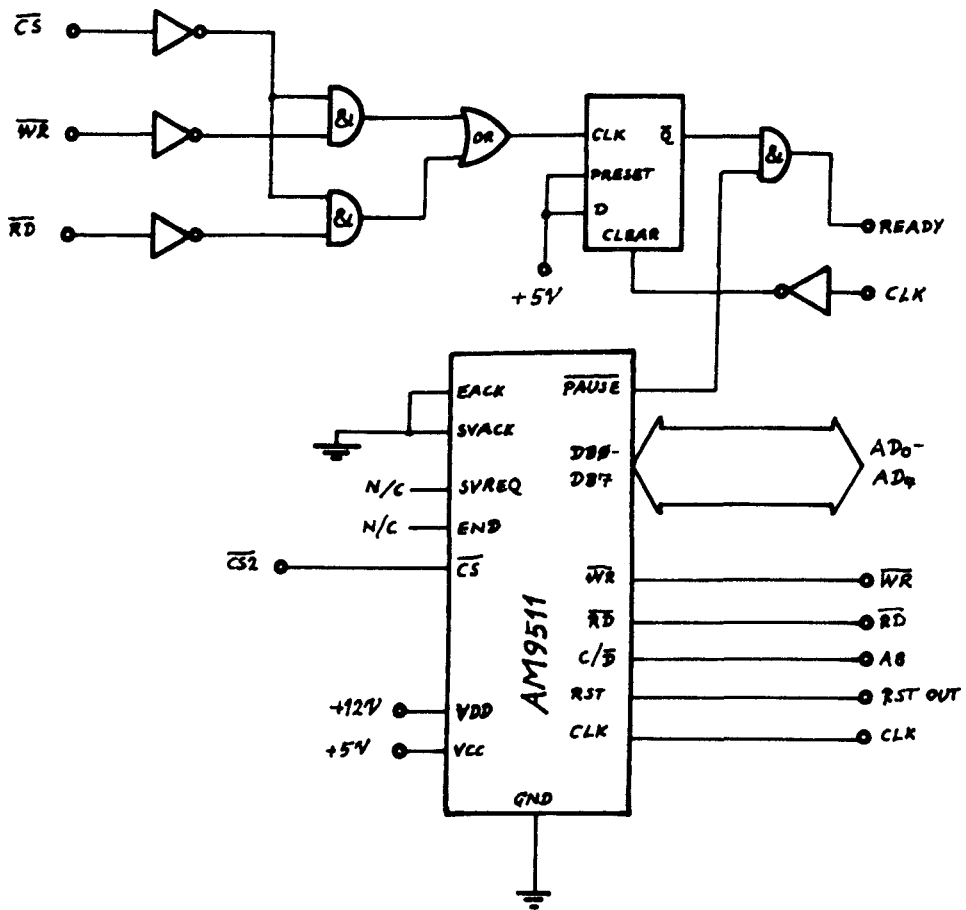


Fig. 6-7: AM9511 APU Interface Schematic

The device has a 3 MHz clock input derived from the CLK pin of the CPU which synchronises the two devices. At power on the device is reset from the RST OUT line of the CPU.

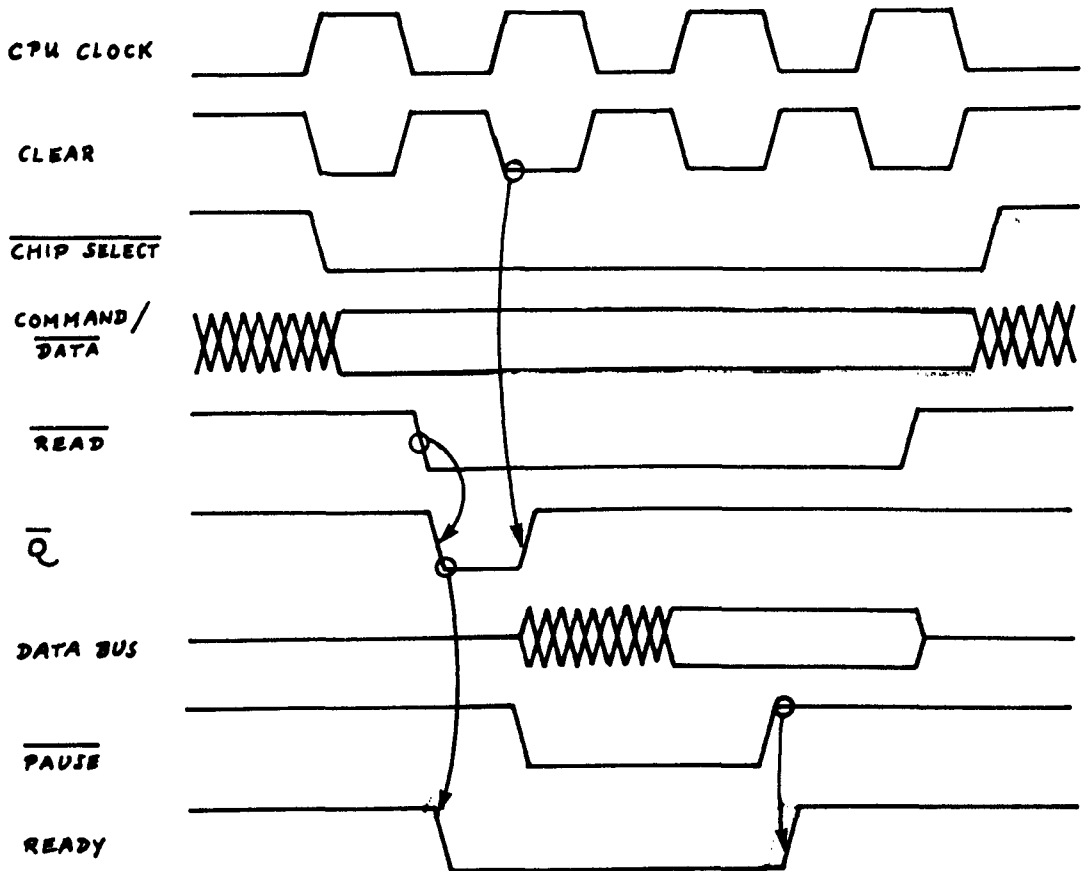


Fig. 6-8: APU Interface Timing Diagram

When reading data from the device with the PAUSE line of the APU connected directly to the CPU READY pin it was found that errors occurred owing to delay in the PAUSE line going low when the APU was accessed by the CPU. The CPU was reading data from the bus before it had settled. The logic shown in Fig. 6-7 pulls the READY line low immediately the device is selected allowing it to return high when PAUSE goes high. The timing and wiring diagrams are shown in Figs. 6-8 and 6-9 respectively.

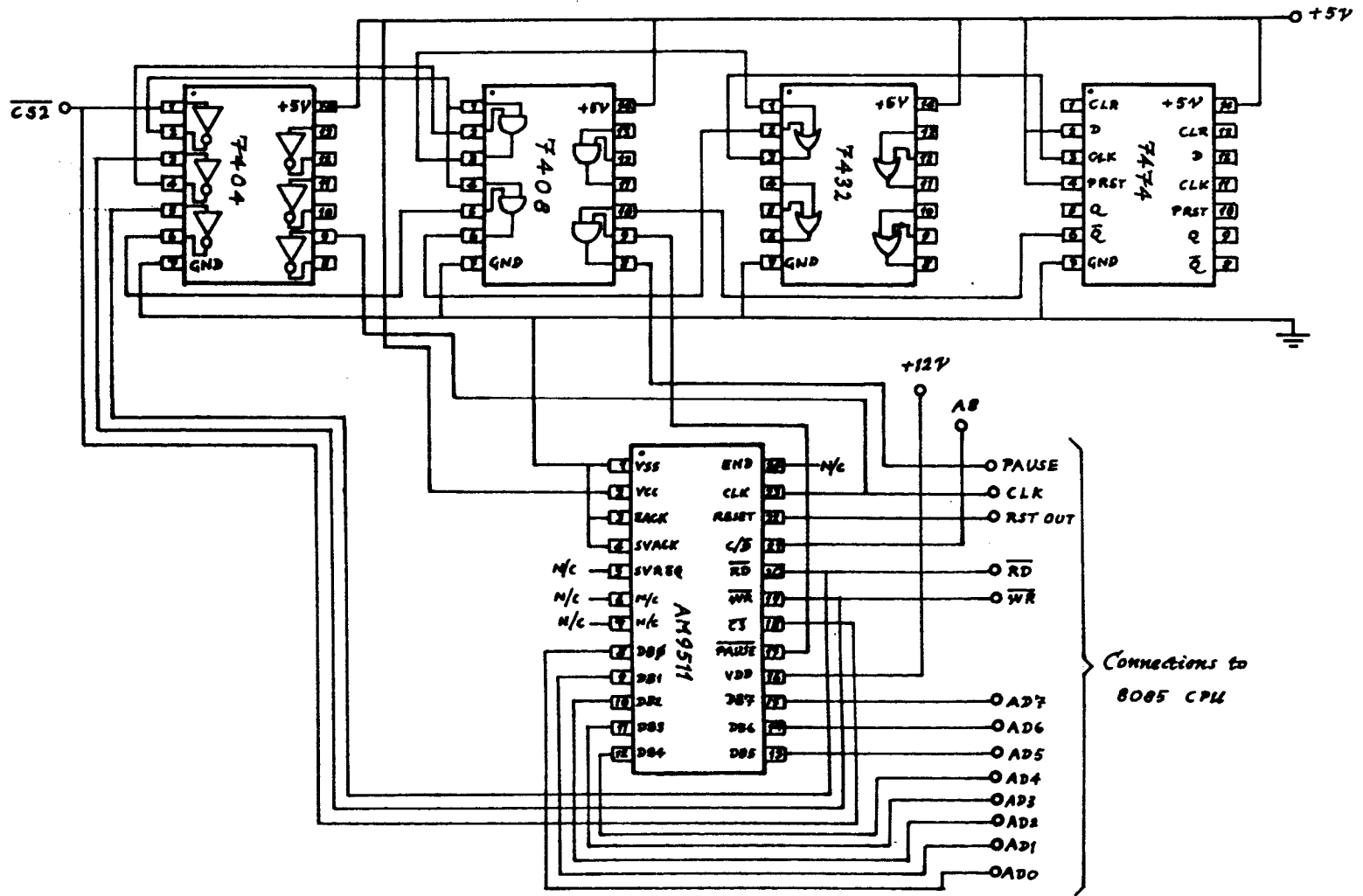


Fig. 6-9: APU Interface Circuit

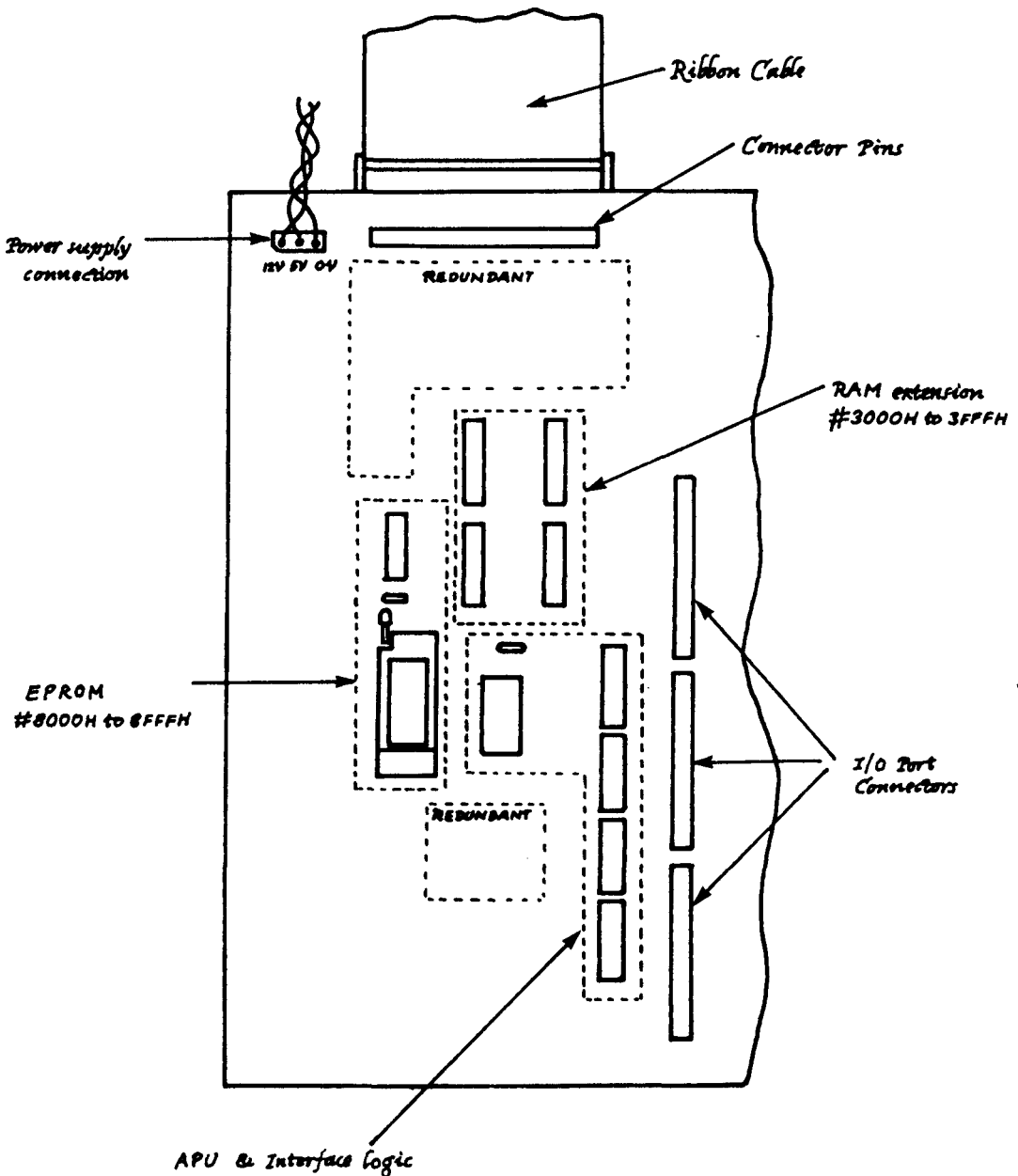


Fig. 6-10: Layout of Modifications to SDK-85 Board

6.5 Board Layout

The layout of the custom built circuits is shown in Fig. 6-10. The diagram also shows the power supply connection to the processor board and the ribbon cable connectors. Plate IV shown a plan of the complete main circuit board. The details of the complete ribbon cable connections are given later, in the chapter covering the rack wiring.

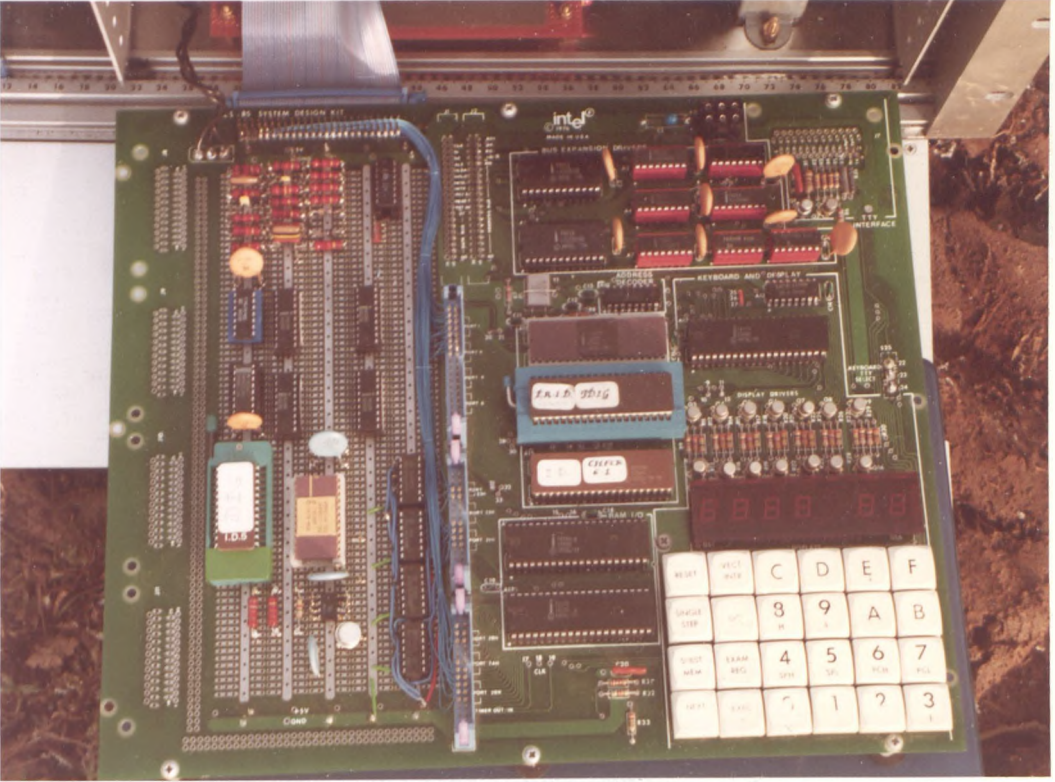


Plate IV: Modified Intel SDK-85 Board

6.6 Memory and I/O Maps

Tables 6-1 and 6-2 respectively show the memory map (including the active 8205 chip select lines) and the I/O map with the usage of the different ports.

I/O Map				
Port Address	Chip	Port	Function	No. of bits used
00H	8355	A	Slew	8
01H	8355	B	Lift	8
21H	8155 ₁	A	Reach	8
22H	8155 ₁	B	Bucket	2 of 8
23H	8155 ₁	C	Mode Indicate	2 of 6
29H	8155 ₂	A	ADC Bus	8
2AH	8155 ₂	B	Mode Select	2 of 8
2BH	8155 ₂	C	ADC Control	5 of 6

Table 6-2: System I/O Map

Memory Map		
Address	Function	Active 8205 chip select
0000H 07FFH	Monitor ROM (8355)	CS0
0800H 0FFFH	Expansion EPROM (8755)	CS1
1000H	APU Data (AM9511)	CS2
1001H 10FFH		
1100H	APU Command/ Status (AM9511)	
1101H 17FFH		
1800H	1800H: Keybd./ Display Ctlr. Command Loc.	CS3
1900H	1900H: Keybd./ Display Ctlr. Data Loc. (8279)	
1FFFH		
2000H 20FFH	Basic RAM (8155 ₁)	CS4
2100H 27FFH	Basic RAM fold back	
2800H 28FFH	Expansion RAM (8155 ₂)	CS5
2900H 2FFFH	Expansion RAM fold back	
3000H 33FFH	Expansion RAM (8185 ₁)	CS6
3400H 37FFH	Expansion RAM (8185 ₂)	
3800H 3BFFH	Expansion RAM (8185 ₃)	CS7
3C00H 3FFFH	Expansion RAM (8185 ₄)	
4000H 7FFFH		
8000H 8FFFH	Expansion EPROM (2732)	

Table 6-1: System Memory Map

CHAPTER SEVEN

HARDWARE II: INTERFACE CARDS, POWER SUPPLIES, & RACK CONNECTIONS

- 7.1 Analogue Interface Unit
- 7.2 Valve Driver Card
- 7.3 Power Supplies
- 7.4 Rack Layout & Interconnection Tables

7.1 Analogue Interface Card

The circuit schematic for the analogue interface card is shown in Fig. 7-1. The 5 V reference supply acts as the reference voltage source for the position transducers, the control joysticks, and the pitch control. The voltage reference is also connected to the Analogue to Digital Converter, the ADC0816 manufactured by National Semiconductor, as the reference supply across the divider chain. The ADC has eight bit resolution and the chip incorporates a sixteen channel multiplexer for analogue inputs of which only eight are used here.

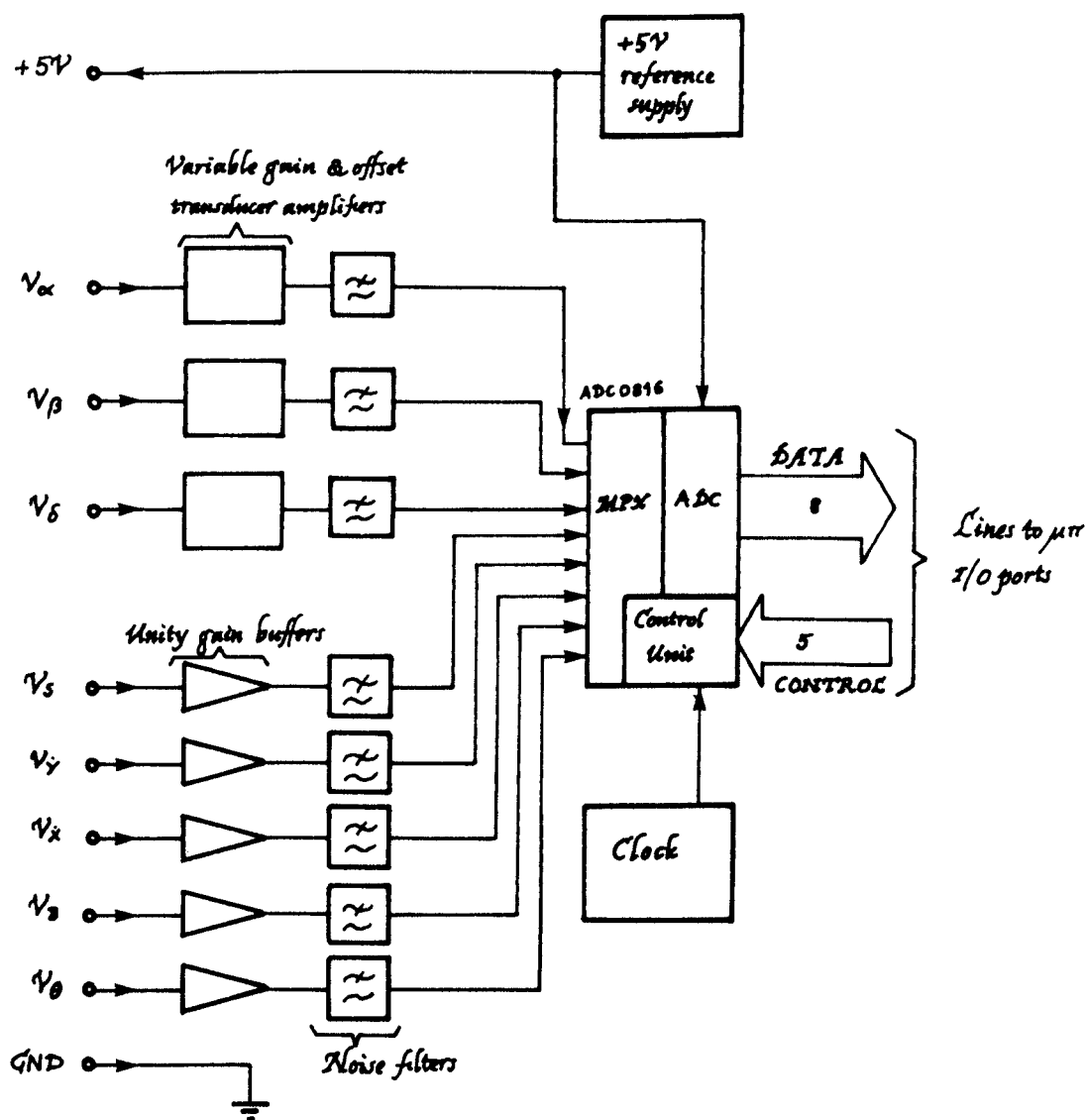


Fig. 7-1: Analogue Interface Card Schematic

The analogue inputs from the transducers pass through signal conditioning amplifiers with a variable gain and offset. The function of these is to map the full scale output swing of the transducers onto the full range of the converter. The joystick and pitch control voltages are fed into unity gain buffers. The range of joystick voltage variation does not require any amplification and the pitch control potentiometer is variable between 0 V and 5 V.

The analogue inputs to the multiplexer all pass through low pass filters to keep the overall noise at the input to the ADC below 10 mV; the cut-off frequency of the filters is set at 1 kHz. The clock for the ADC runs at 640 kHz to give a maximum conversion time of 114 μ s. The control lines select the analogue input, initiate conversion, and signal the data to be output onto the 8 bit bus at the end of the conversion.

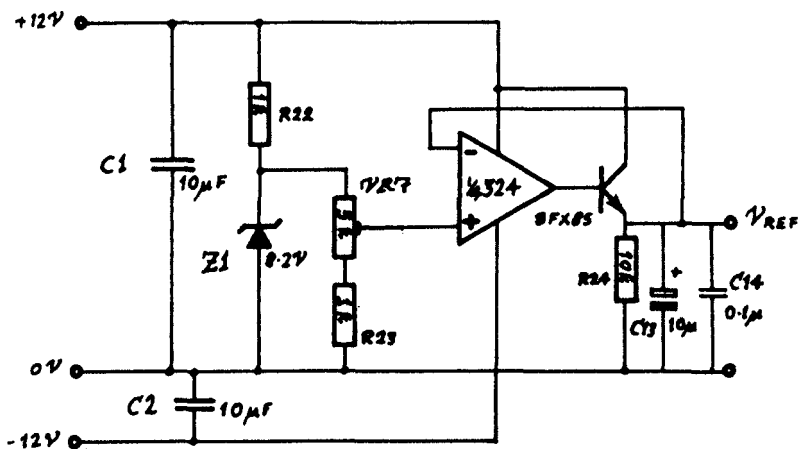


Fig. 7-2: 5 V Analogue Reference Circuit

The circuit for the 5 V analogue reference is shown in Fig. 7-2; the two 10 μ F capacitors C1 and C2 smooth the supply for the operational amplifier and the Zener Z1. The voltage across the Zener is 8.2 V and from this is derived 5 V using the

potential divider of VR7 and R23. This voltage is buffered by the op-amp, and the BFX85 transistor is used to boost the buffer output current. The 10 k resistor provides a load for output stability if no other load is connected. Output smoothing is provided by C13 and C14.

The circuit used for the variable gain and offset amplifiers is shown in Fig. 7-3. Operational amplifier B acts as an input buffer for the transducer and amplifier A buffers the offset voltage into the unity gain summing amplifier C. Amplifier D provides the gain stage. The wiring diagram for the three transducer amplifiers is shown in Fig. 7-4. Operational amplifier 324₄ is used to buffer the voltages from the joysticks.

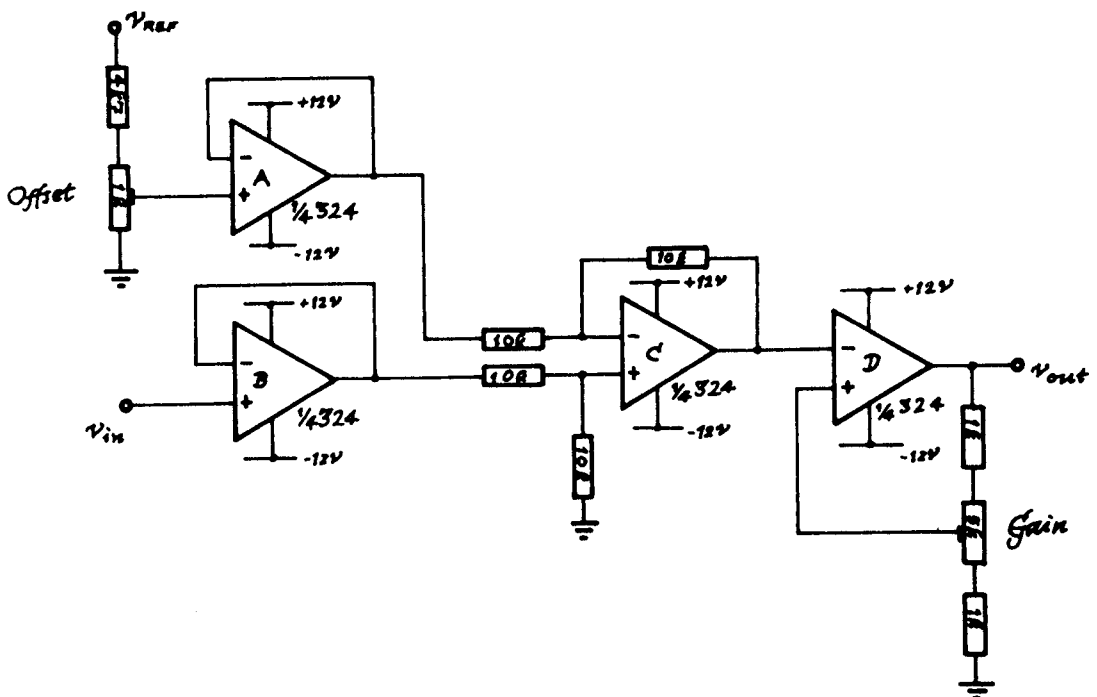


Fig. 7-3: Transducer Signal Conditioning Amplifier

The circuit for the ADC is shown in Fig. 7-5; the ADC0816 has a built-in analogue multiplexer with sixteen inputs of which

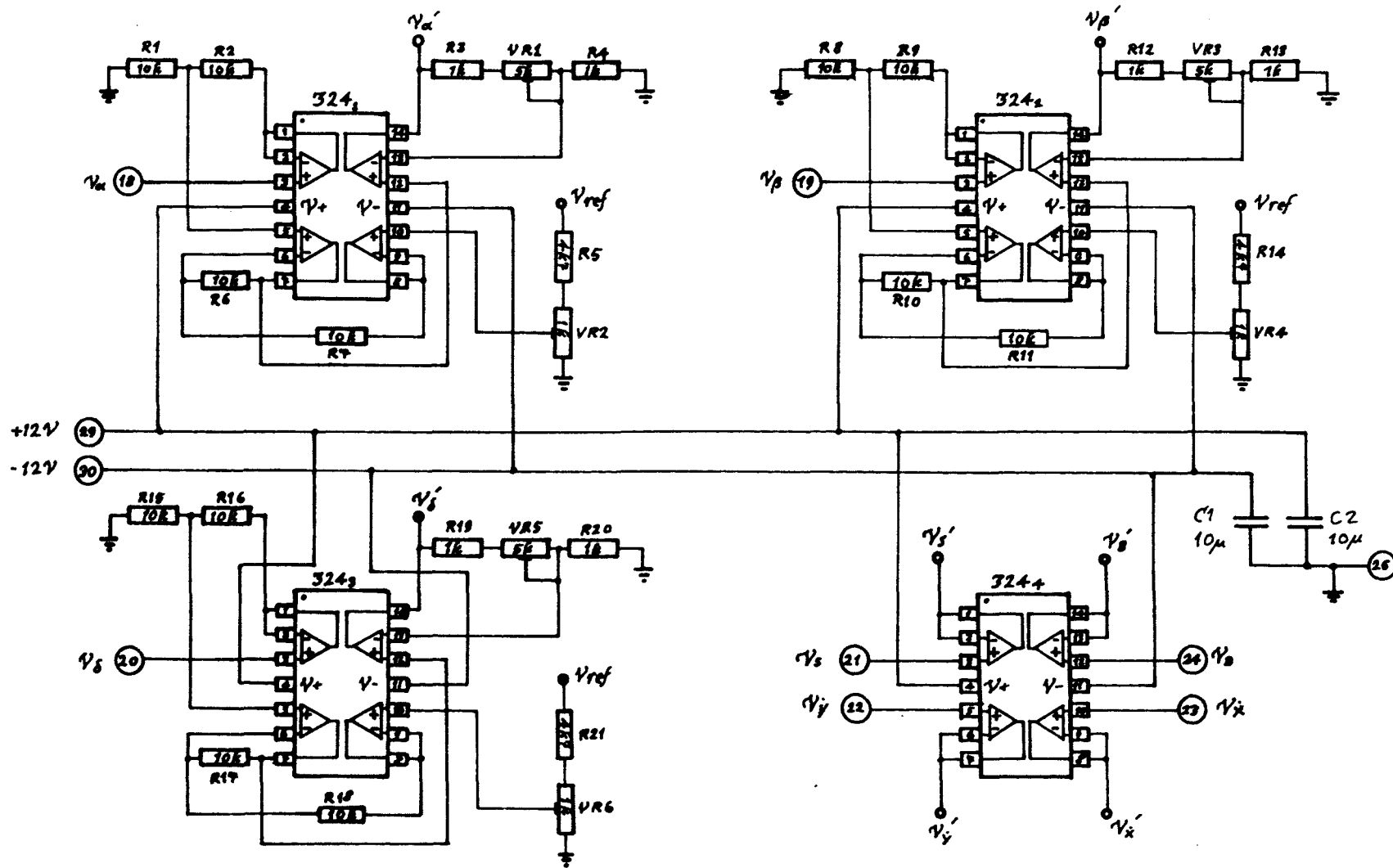


Fig. 7-4: Wiring Diagram of Amplifiers and Buffers

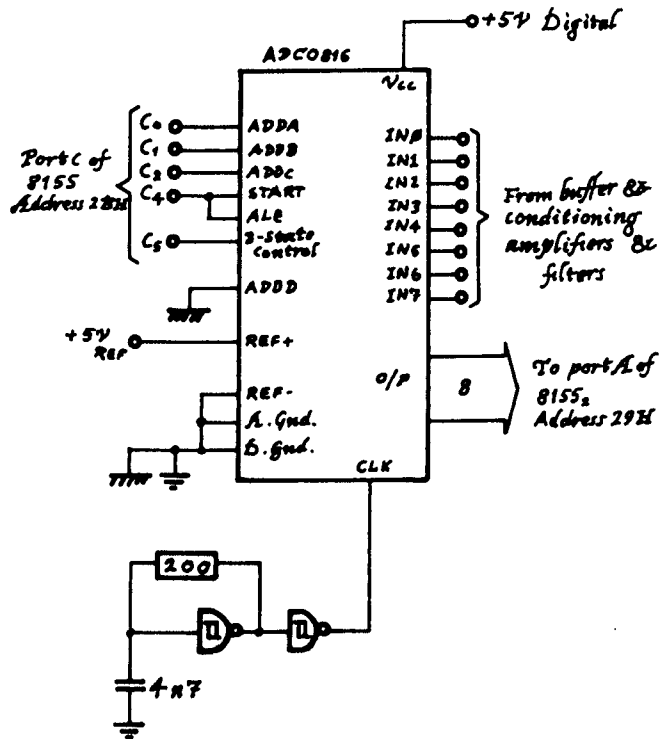


Fig. 7-5: Analogue to Digital Converter

eight, IN0 to IN7, are used here. The chip runs off the 5 V logic supply and also has a 5 V reference input for the divider chain in the ADC. Control lines ADD A, ADD B, ADD C are used to select the input line address. ADD D is tied low as only eight of 16 inputs are used. The START and address latch enable (ALE) are connected to control line C4 which is pulsed high to initiate a conversion once the address for the input has been presented on ADD A-C (see timing diagram Fig 7-6). C5 goes high to activate the tri-stated 8-bit output port at the end of the conversion. The ADC has a clock input of 640 kHz provided by the Schmitt Trigger inverter with the feedback resistor and capacitor to ground, the second gate acting as a buffer.

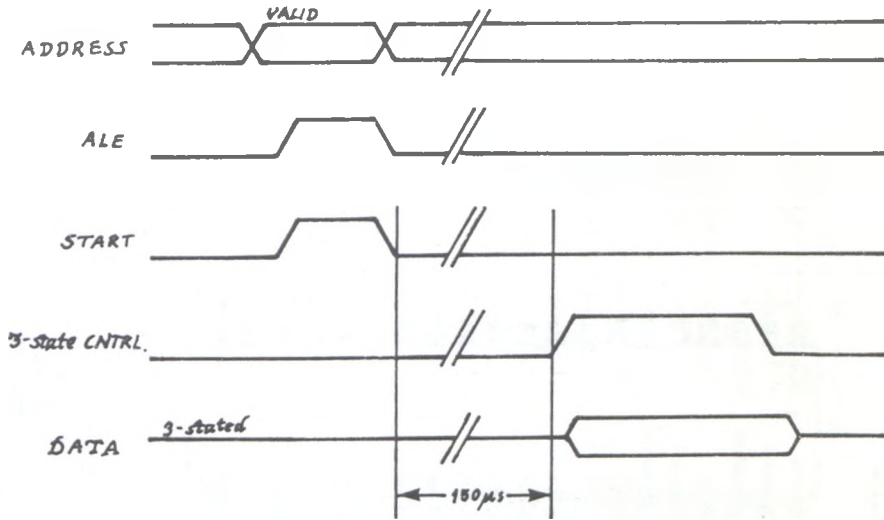


Fig. 7-6: ADC Timing Diagram

The wiring diagram for the ADC circuitry is shown in Fig. 7-7, and the layout in Fig. 7-8 and Plate V.

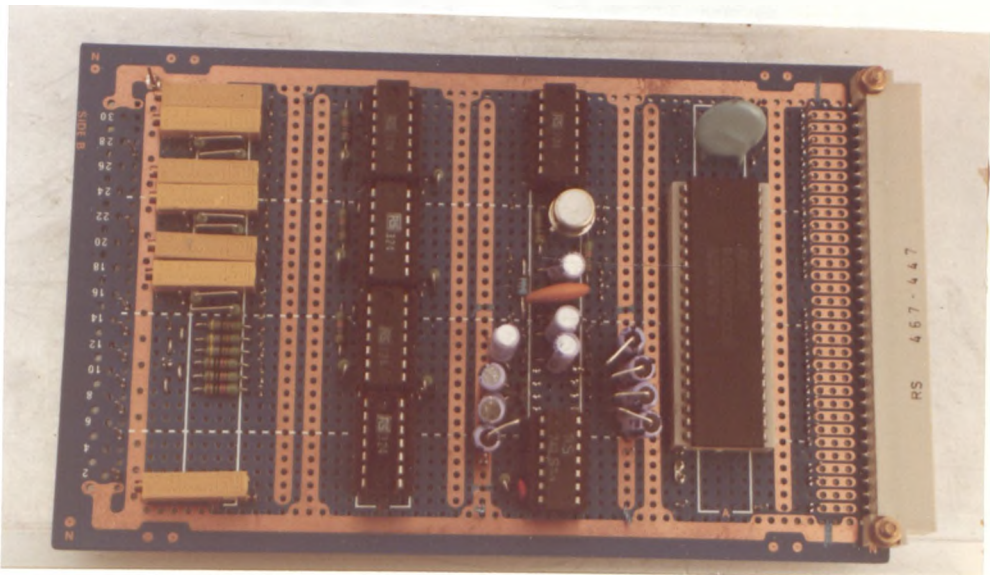


Plate V: Analogue Interface Card

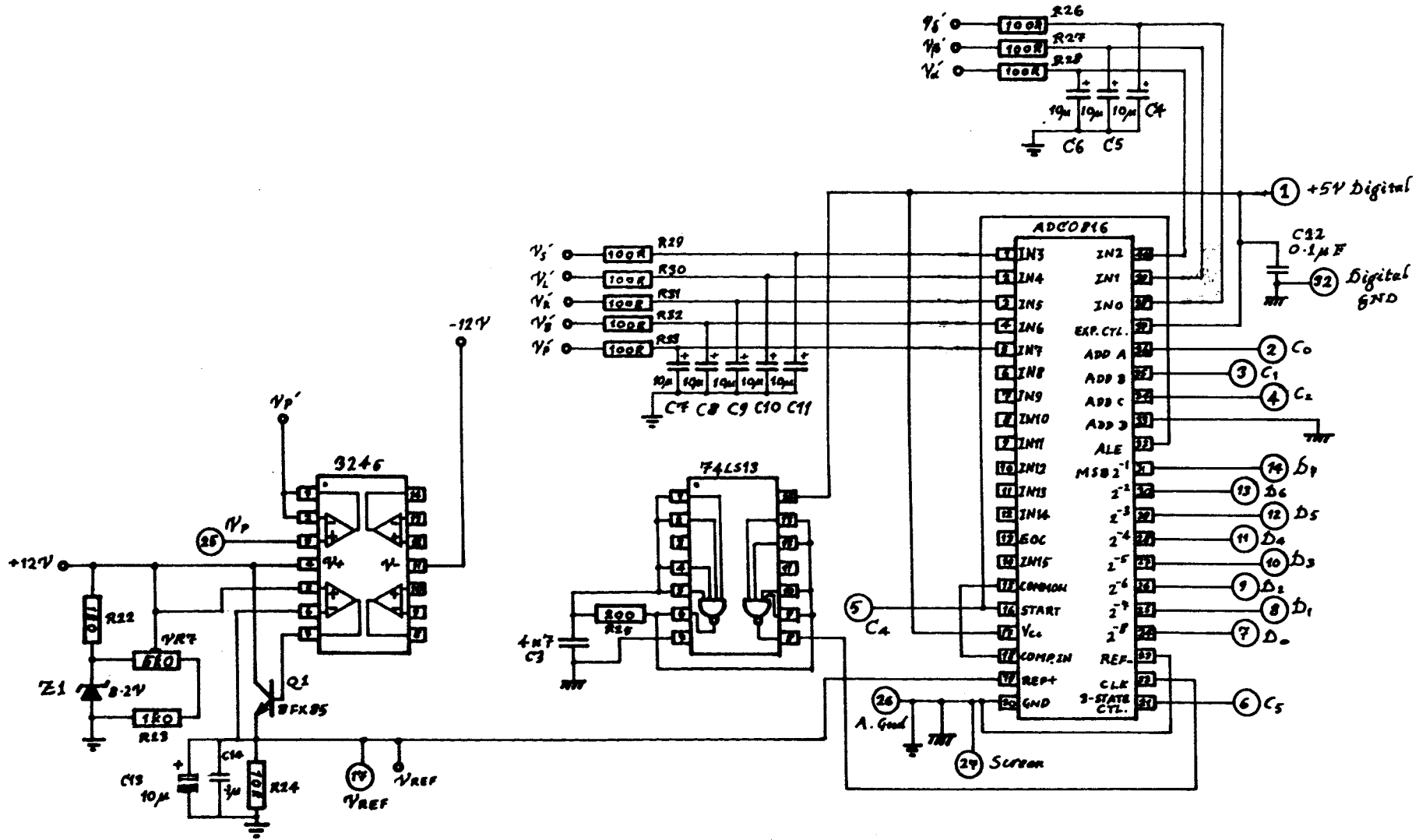
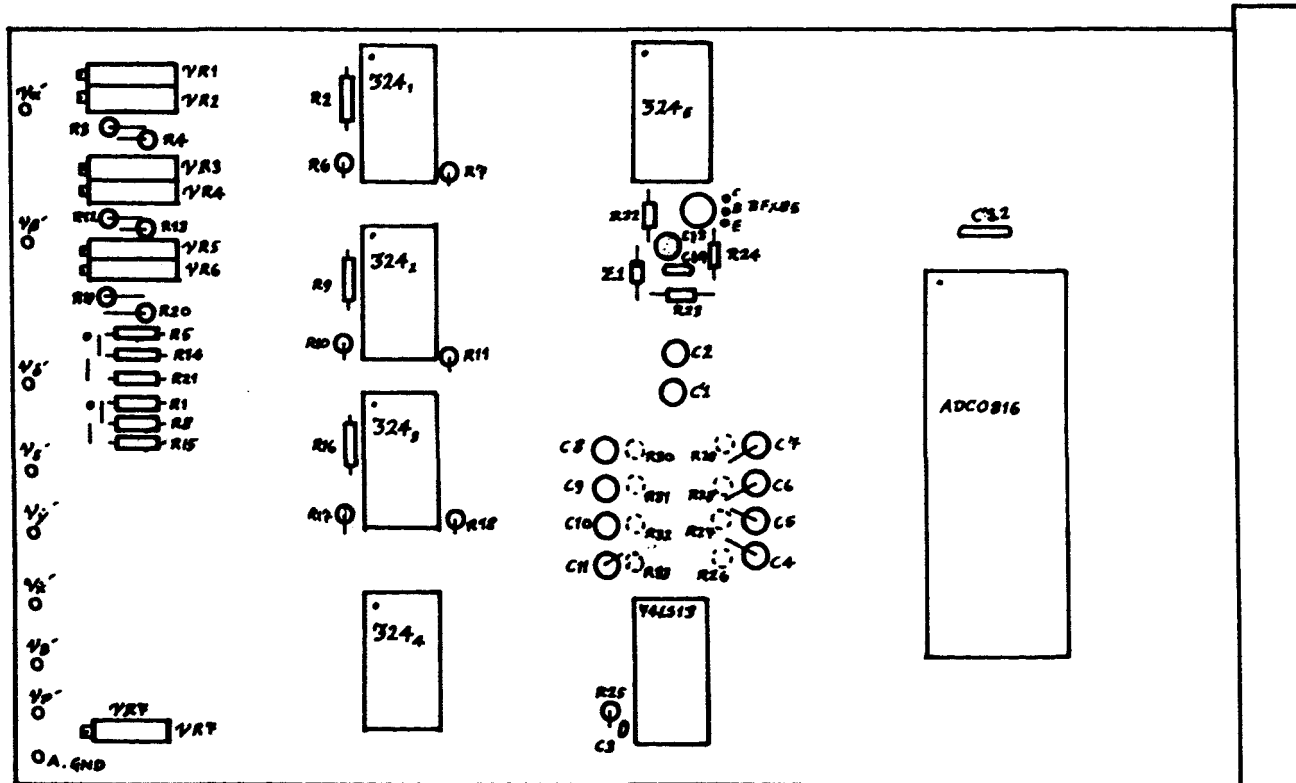


Fig. 7-7: ADC Wiring Diagram



Components shown dotted are on underside of board.

Fig. 7-8: Analogue Card Layout

7.2 Valve Driver Card

The valve driver card is essentially a 3-channel digital pulse width modulator circuit for driving the SLEW, LIFT, and REACH valves. There are three 8-bit digital inputs, seven bits for each channel are used to select the mean valve current and the eighth to select the direction of movement: Right or Left etc.

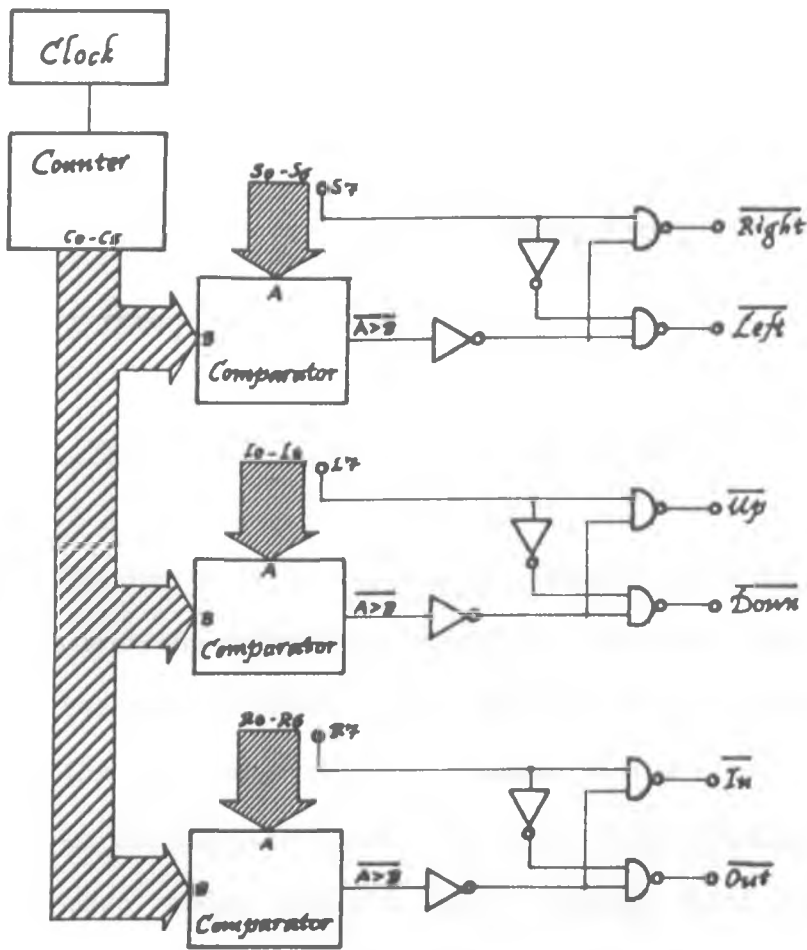


Fig. 7-9: Valve Driver Schematic

The circuit schematic is shown in Fig. 7-9. The three control inputs S0-S7, L0-L7, and R0-R7 are for the Slew, Lift, and Reach functions respectively, line 7 selecting the direction in each case.

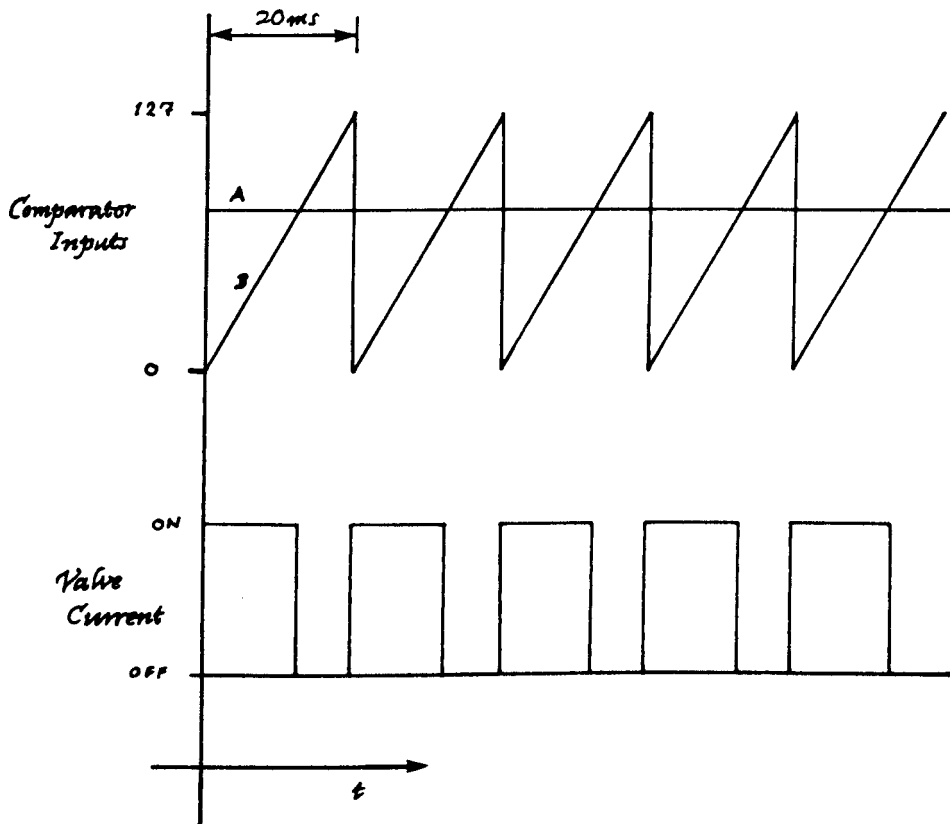


Fig. 7-10: Valve Driver Timing Diagram

For each channel there is a seven bit digital comparator: one input is from a cyclic counter generating a sawtooth output and the other is the control signal. The logic operates as shown in Fig. 7-10 so that the valve current is ON when the control input is greater than the counter value. So over an input range of 0 to 127 the mean valve current varies linearly from zero to maximum. The frequency of the valve switching pulse train is set to 50 Hz by adjusting the clock to run at 6.4 kHz.

The wiring diagram for the clock and counter circuit is shown in Fig. 7-11. A 555 timer is used for generating the clock signal, adjusted by potentiometer VR1. The counter employs two 74LS163 four bit counter chips, the output being taken from the

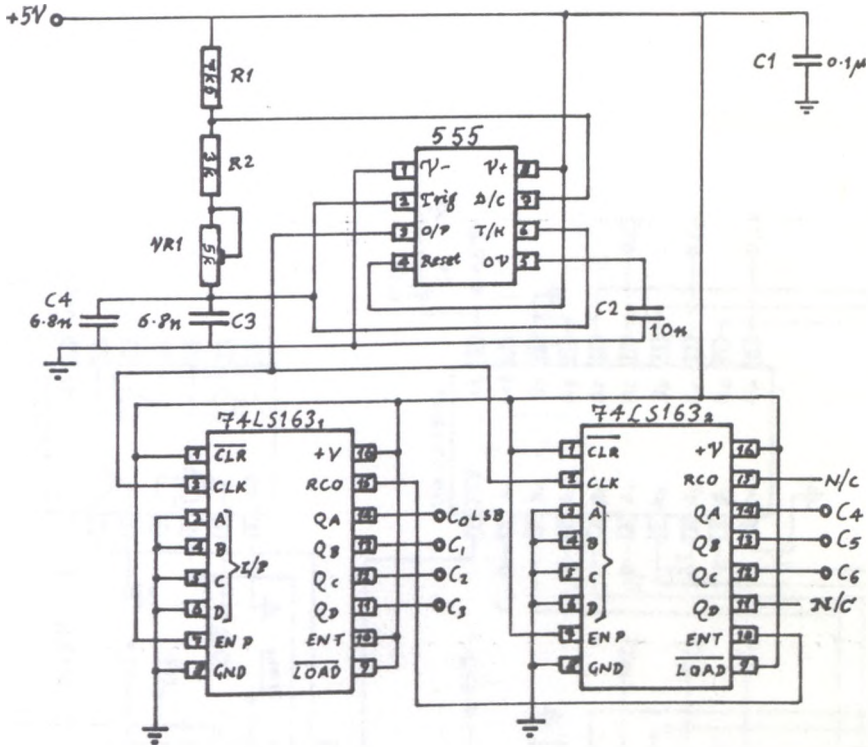


Fig. 7-11: Wiring Diagram of Clock & Counter Circuit

seven least significant bits. Fig. 7-12 shows the wiring of the comparator and logic circuitry. The outputs from the card to the valve switching circuits are active low. The circuit layout is shown in Fig. 7-13 and Plate VI.

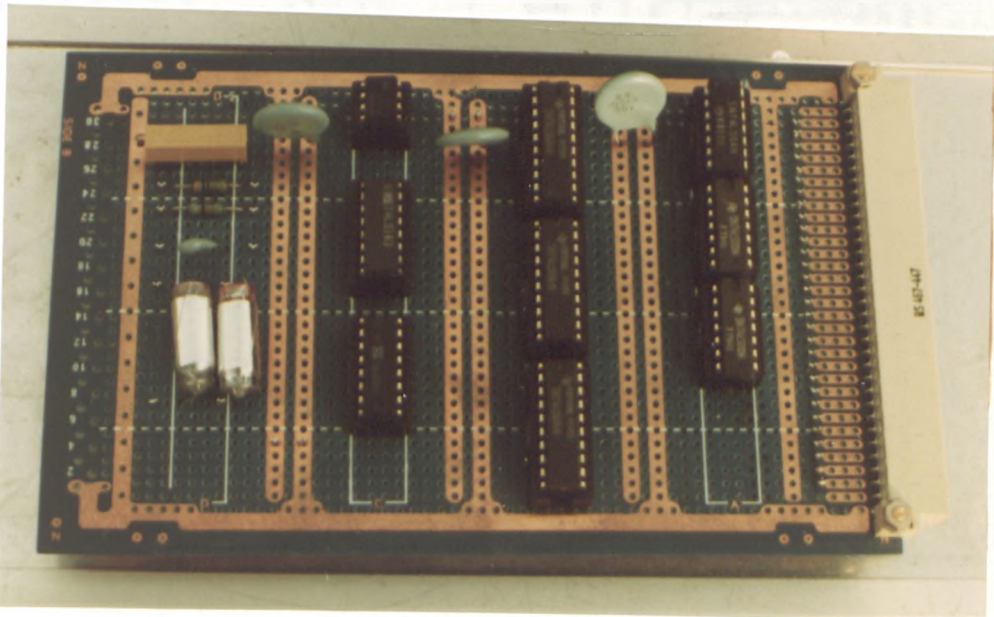


Plate VI: Valve Driver Card

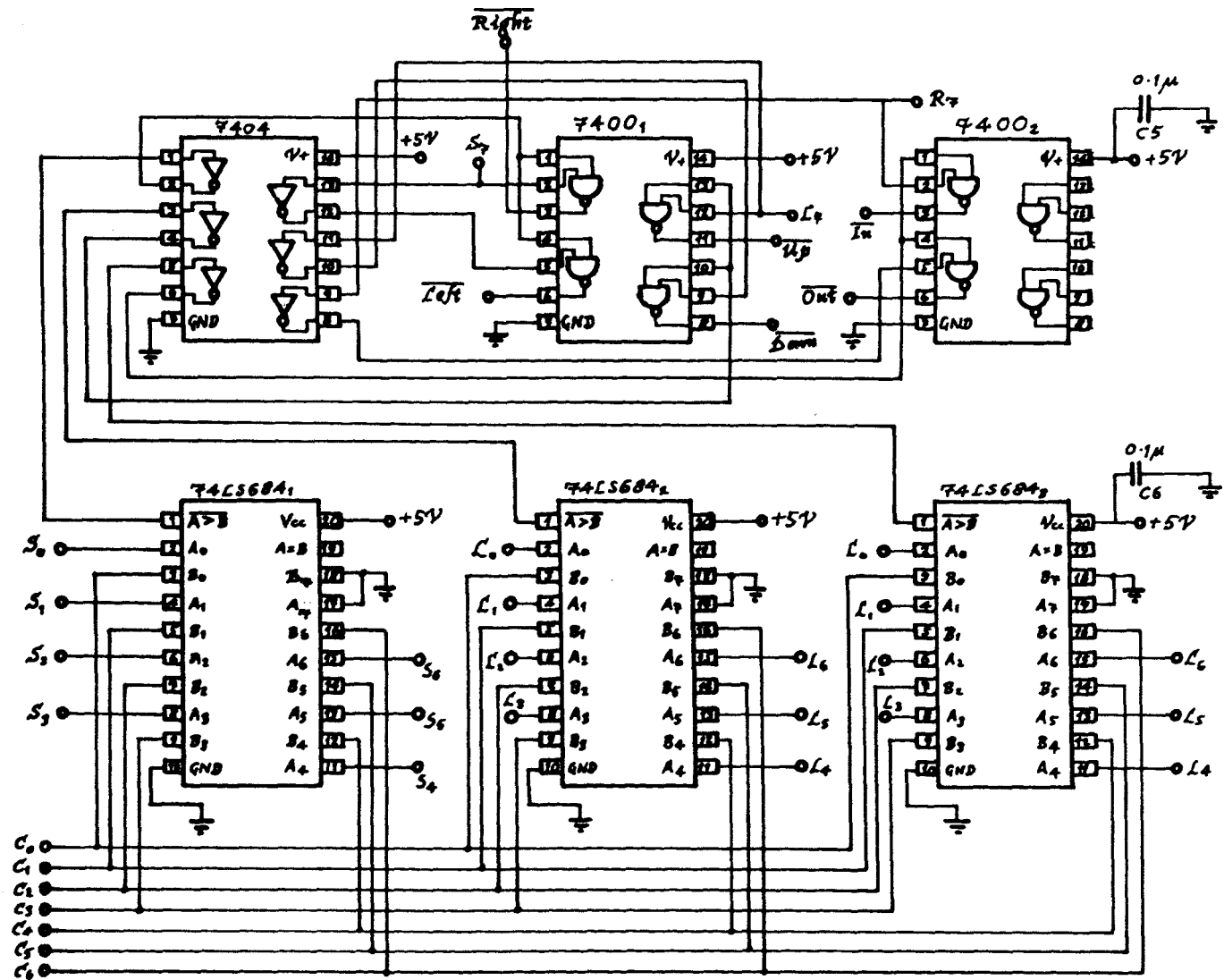


Fig. 7-12: Wiring Diagram of Valve Driver Comparator & Logic Circuitry

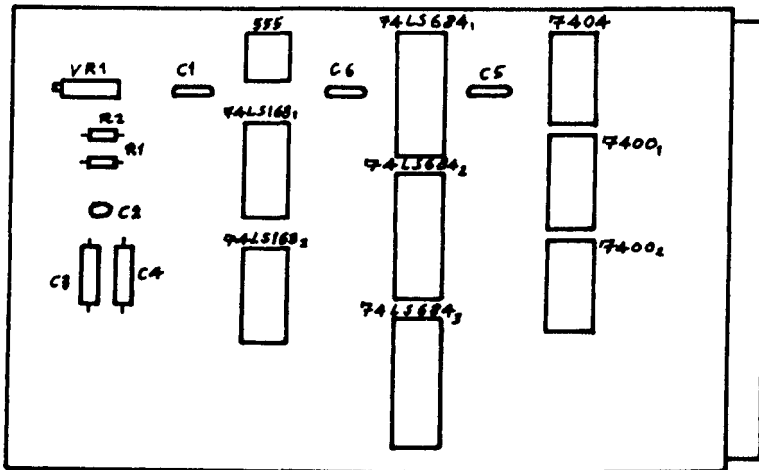


Fig. 7-13: Valve Driver Circuit Layout

7.3 Power Supplies

The main 5 V power supply for the logic circuitry is shown in Fig. 7-14. The input comes from the tractor battery via the power switching relay situated in the switching unit. The 27 V Zener is to act as protection against any high voltage spikes or surges; the smoothing circuit comprising L1, L2, C1, C2 removes ripple and high frequency noise from the input to the regulator RG1. The feedback network of R1 and VR1 may be adjusted to give the desired output of 5V and C3 and C4 provide output smoothing.

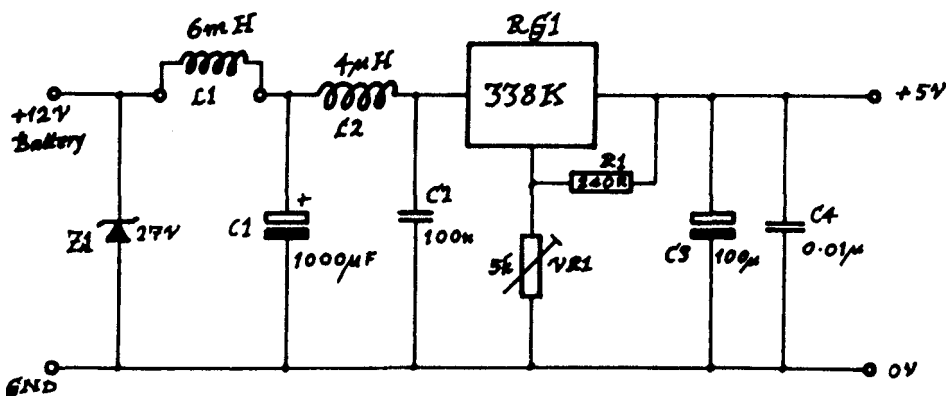


Fig. 7-14: 5 V Regulator Circuit

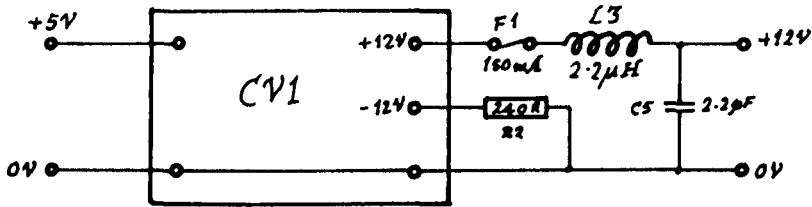


Fig. 7-15: 12 V APU Supply

The +12 V supply for the APU is shown in Fig. 7-15. CV1 is a DC to DC converter with a 100 mA output rating, L3 and C5, serve to eliminate high frequency noise from the output probably due to internal switched mode operation of the converter. The 240 dummy load on the negative output is necessary to preserve regulation of the positive output.

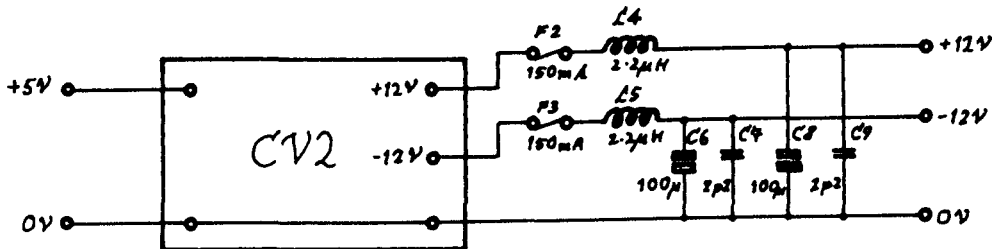


Fig. 7-16: ±12 V Analogue Supply

A similar converter is used in the DC supply for the analogue board (Fig. 7-16) which additionally has 100 μF capacitors on each output line to eliminate ripple. The circuit board layout is shown in Fig. 7-17 and Plate VII.

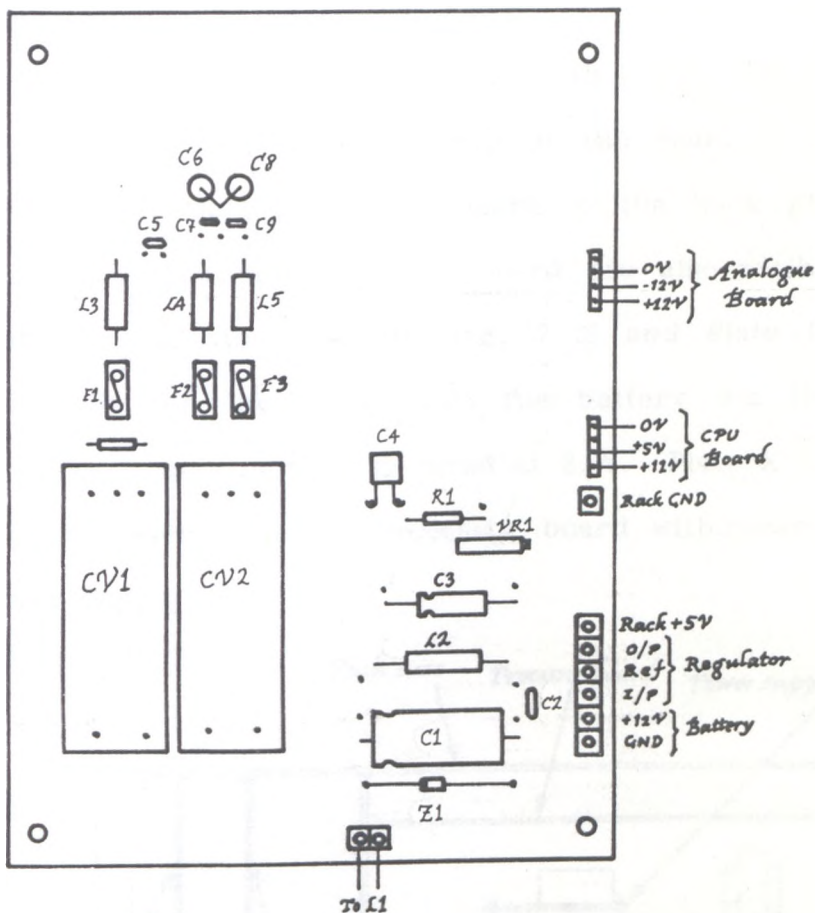


Fig. 7-17: Power Supply Board Layout

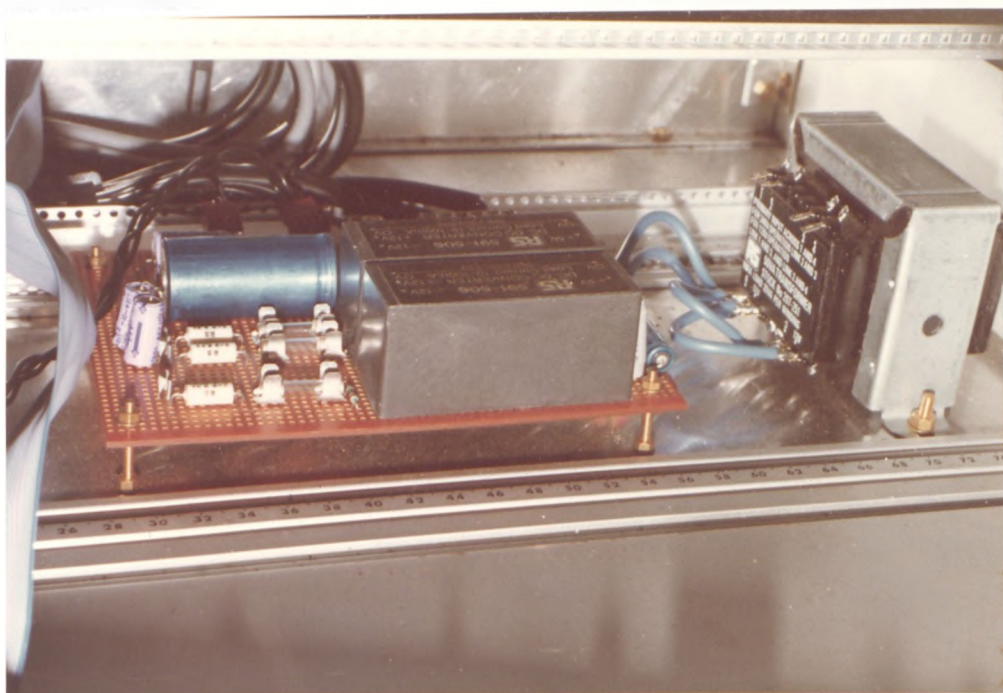


Plate VII: Power Supply Circuitry

7.4 Rack Layout and Connection Tables

The front view of the main rack is shown in Fig. 7-18 and Plate VIII show the interior wiring at the rear. The blue ribbon cable connects the main board to the back plane; the connections to the power supply board are also visible. The rear of the rack is shown in Fig. 7-19 and Plate IX. The fuseholder is for the input from the battery via the power switching unit and the fuse is rated at 2 A. Plate X shows the front of the rack with the processor board withdrawn to show the power supply.

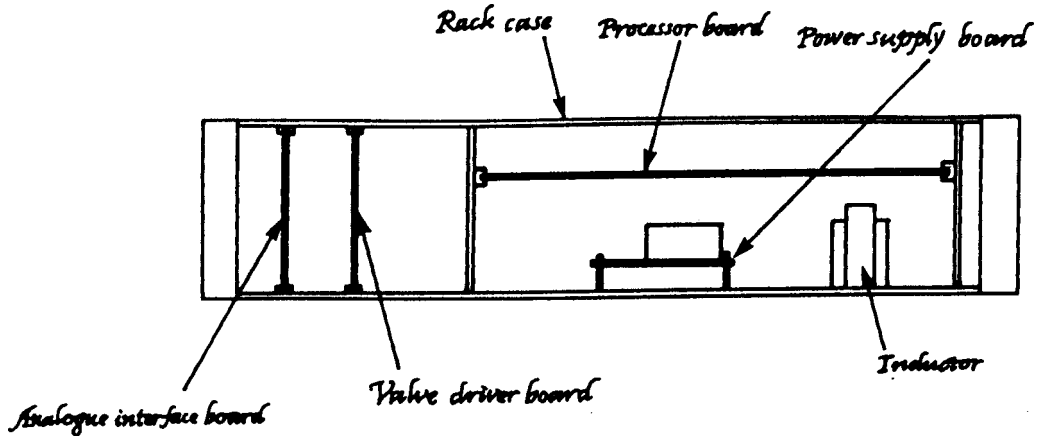


Fig. 7-18: Front View of Main Rack

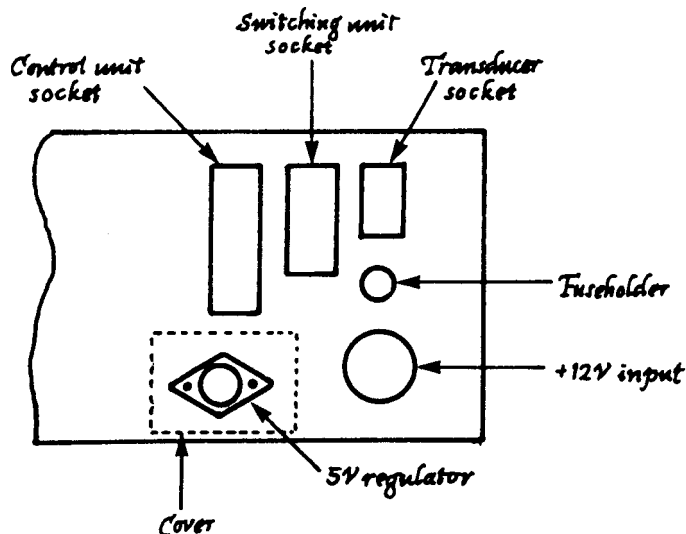


Fig. 7-19: Rear View of Main Rack

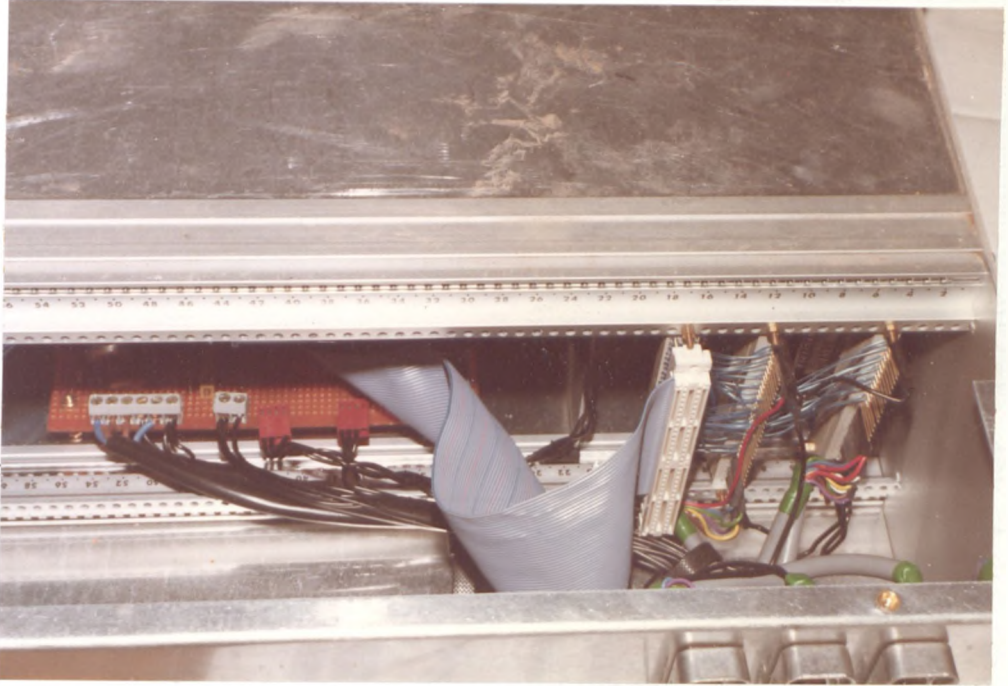


Plate VIII: Wiring at Rear of Main Rack

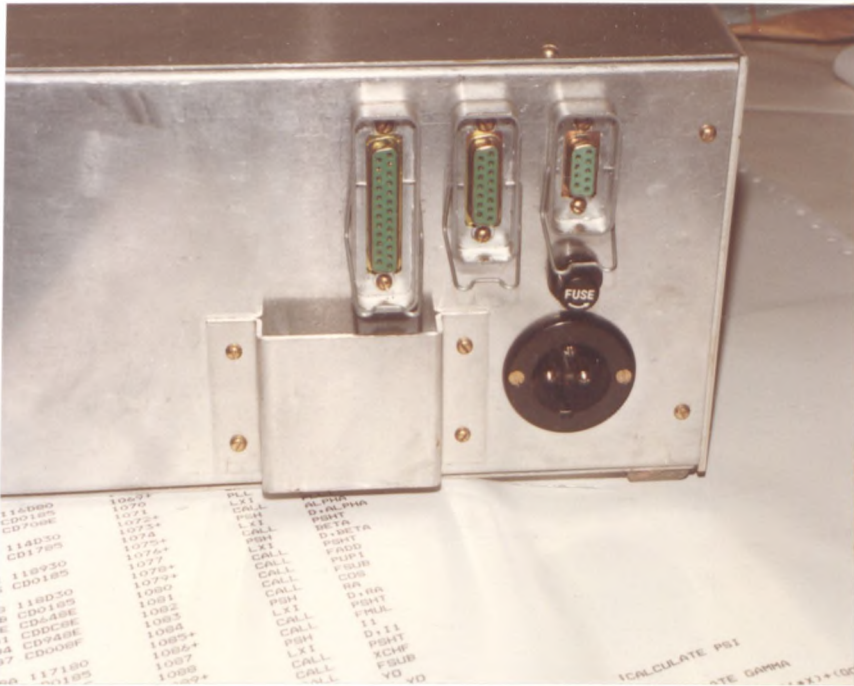


Plate IX: Rear Panel of Main Rack

Tables 7-1 to 7-4 list the connections to the circuit boards and the sockets on the back panel of the rack.

Rack Connections				
SDK-85 Edge Connector	Rack Connector	Function	Analogue Card	Driver Card
1	c 1	S0		3
2	a 1	S1		4
3	c 2	S2		5
4	a 2	S3		6
5	c 3	S4		7
6	a 3	S5		8
7	c 4	S6		9
8	a 4	S7		10
9	c 5	L0		11
10	a 5	L1		12
11	c 6	L2		13
12	a 6	L3		14
13	c 7	L4		15
14	a 7	L5		16
15	c 8	L6		17
16	a 8	L7		18
17	c 9	R0		19
18	a 9	R1		20
19	c 10	R2		21
20	a 10	R3		22
21	c 11	R4		23
22	a 11	R5		24
23	c 12	R6		25
24	a 12	R7		26
25	c 13	OPEN		
26	a 13	CLOSE		
27	c 14	MIO		
28	a 14	M11		
29	c 15	MS0		
30	a 15	MS1		
31	c 16	MS2		
32	a 16	C0	2	
33	c 17	C1	3	
34	a 17	C2	4	
35	c 18	C4	5	
36	a 18	C5	6	
37	c 19	D0	7	
38	a 19	D1	8	
39	c 20	D2	9	
40	a 20	D3	10	
41	c 21	D4	11	
42	a 21	D5	12	
43	c 22	D6	13	
44	a 22	D7	14	

Table 7-1: Main Circuit Board (SDK-85) Rack Connections

Analogue and Driver Card Connectors		
Pin no.	Analogue Card	Driver Card
1	5V	5V
2	C0	RIGHT
3	C1	S0
4	C2	S1
5	C4	S2
6	C5	S3
7	D0	S4
8	D1	S5
9	D2	S6
10	D3	S7
11	D4	L0
12	D5	L1
13	D6	L2
14	D7	L3
15	n/c	L4
16	n/c	L5
17	VREF	L6
18	V	L7
19	V	R0
20	V	R1
21	VS	R2
22	VY	R3
23	VX	R4
24	VB	R5
25	VP	R6
26	A. Gnd.	R7
27	Screen	LEFT
28	n/c	UP
29	+12V	DOWN
30	-12V	IN
31	n/c	OUT
32	GND	GND

Table 7-2: Analogue and Driver Card Connections

Supply	
V _{input}	Brown
GND	Blue

Regulator	
Input	Brown
Ref.	Black
Output	Blue

Position Transducers				
Function	Socket Pin	Colour	Cable No.	Rack Connection
V _{REF}	1	Red	3	A 17
Lift	2	Blue	3	A 18
Reach	3	Yellow	3	A 19
Bucket	4	White	3	A 20
GND	5	Green	3	A 26
Screen	6	Screen	3	A 27
ON/OFF	7&8	Black		Jystk. 8
		Black		Sw. Unit 20

Control Unit					
Function	Socket Pin	Colour	Cable No.	Connections	
				Rack	Other
V _{REF}	1	Red	1	A 17	
5V Dig.	2	Black			Power supply board
Slew	3	Blue	1	A 21	
Lift	4	Yellow	1	A 22	
Reach	5	White	1	A 23	
Bucket	6	Brown	1	A 24	
Pitch	7	Purple	1	A 25	
On/	8	Black			Transducer Skt. 7
Off	9	Black			Switching Unit 11
IWT	10	Black			Switching Unit 9
MSO	11	White	2	c 15	
MS1	12	Purple	2	a 15	
MS2	13	Blue	2	c 16	
MIO	14	Green	2	c 14	
MI1	15	Red	2	a 14	
Dig. GND	16	Black			Power supply board
An. GND	17	Green	1	A 26	
Screen	18	Screen	1	A 27	

Table 7-3: Back Panel Connections (I)

Switching Unit					
Function	Socket Pin	Colour	Cable No.	Connections	
				Rack	Other
Up	1	Green	4	D 28	
Down	2	Purple	4	D 29	
In	3	Yellow	4	D 30	
Out	4	Brown	4	D 31	
Right	5	Red	4	D 2	
Left	6	Blue	4	D 27	
Open	7	Black	4	c 13	
Close	8	White	4	a 13	
IWT	9	Black			Joystk. Unit 10
On/	10	Black			Transducer 8
Off	11	Black			Joystk. Unit 9
GND	12	Black			Power supply Board
Screen	13				
Screen 4					
Screen 2					

Table 7-4: Back Panel Connections (II)

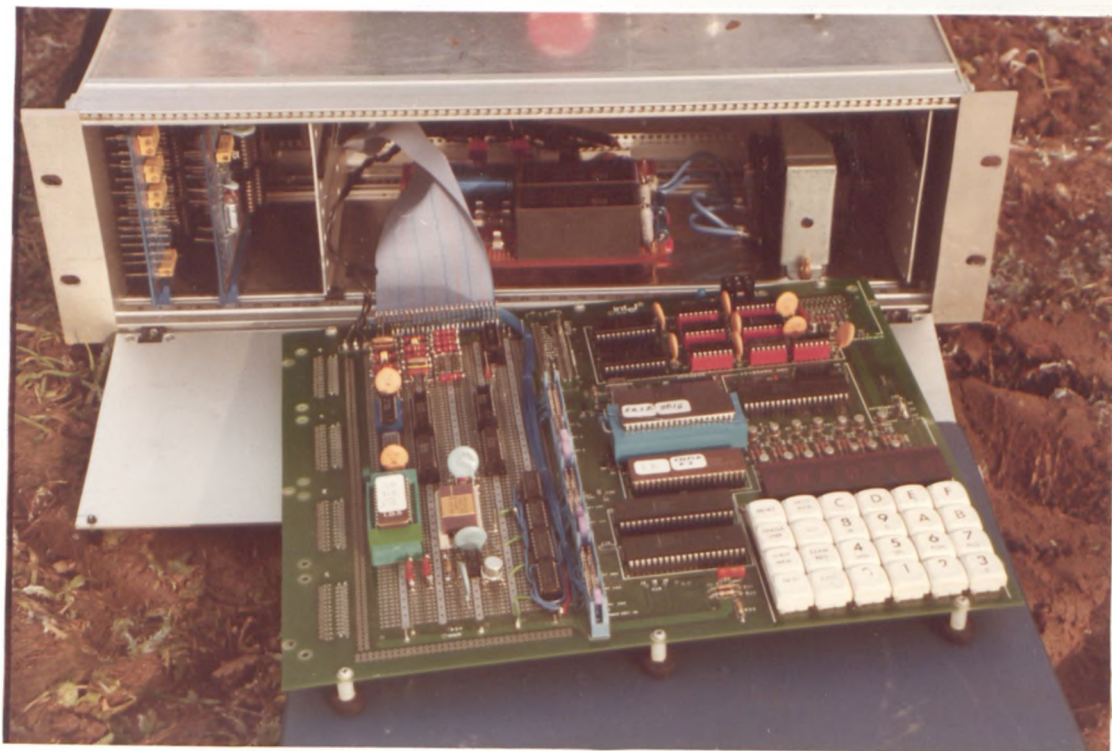


Plate X: Front View of Main Rack

CHAPTER EIGHT

HARDWARE III:

CONTROL UNIT, TRANSDUCER WIRING, &

POWER SWITCHING UNIT

- 8.1 Control Unit
- 8.2 Transducer Wiring
- 8.3 Power Switching Unit

8.1 Control Unit

The layout of the controls on the Control Unit is shown in Fig. 8-1. The joystick units are spring centred inductive devices which are very reliable as there are no potentiometer wipers to wear out. The orientation of the joystick axes and their corresponding functions is in a similar fashion to that of a conventional mechanically controlled digger. This is to minimise the re-learning necessary for operators already familiar with conventional controls. The carry strap supports project out from the case approximately 40 mm on each side to keep the strap, worn around the operator's neck, away from his hands while operating the unit.

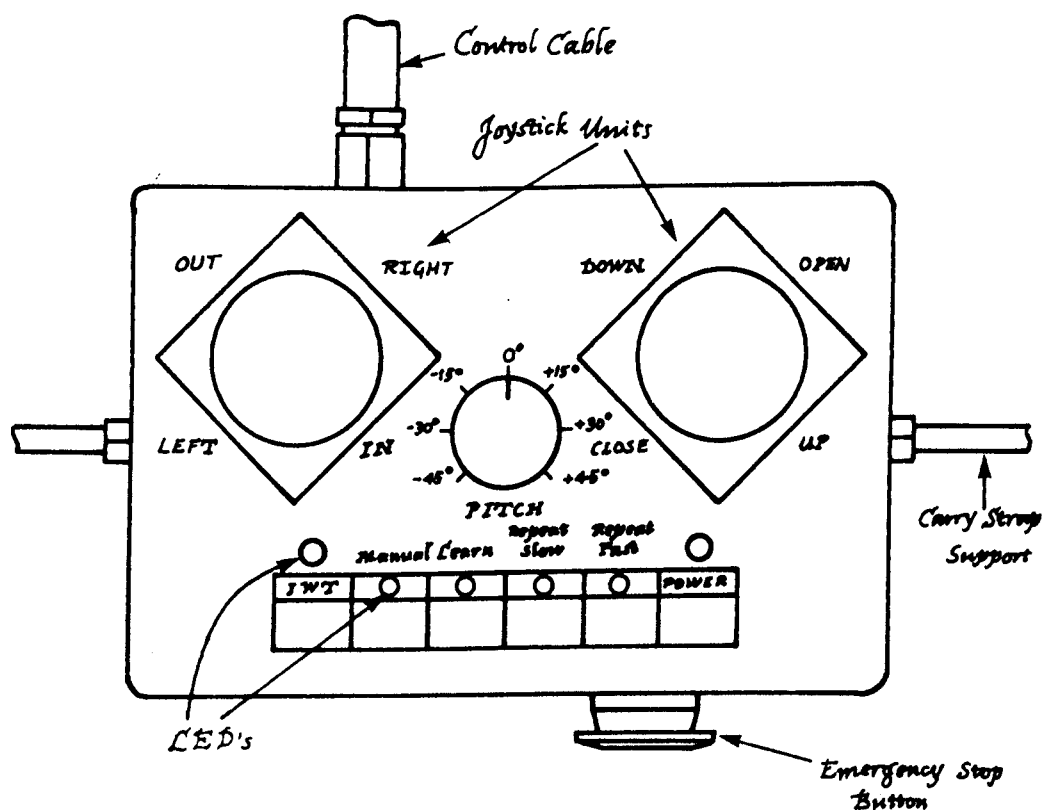


Fig. 8-1: Layout of Controls

The pitch control is situated in the centre of the control panel and comprises a plastic film potentiometer calibrated to correspond to pitch angles of -45° to $+45^\circ$. The power and Instant Weight Transfer (IWT) switches are of the latching type with LED's mounted above them to indicate their status. The mode selection switches are of momentary type and have integral LED's; this arrangement allows mode selections and changes to be made in software e.g. to start up at power on in Manual Mode and to revert to Manual Mode at the end of a Repeat sequence. The large Emergency Stop button is mounted on the front of the control unit and latches when depressed, being released by a twist.

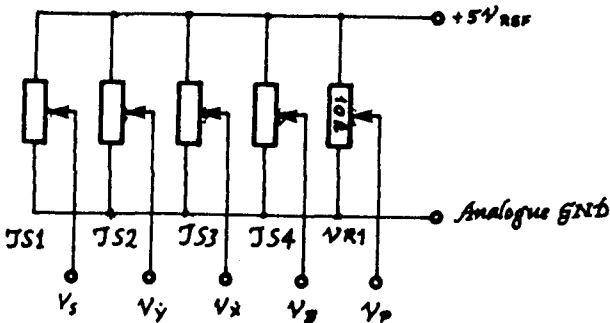


Fig. 8-2: Connection of Joysticks & Pitch Control

The circuit for the joysticks and the pitch control is shown in Fig. 8-2. The 5 V reference is from the analogue interface card; the output voltage swing of the joysticks is $\frac{1}{2}$ V from a central position with a standing output of $2\frac{1}{2}$ V and they have an output resistance of 1.8 k Ω .

The mode selection switch circuitry is shown in Fig. 8-3 along with the truth table for encoding the five possible switch settings to the three mode select lines MS0, MS1, and MS2. The

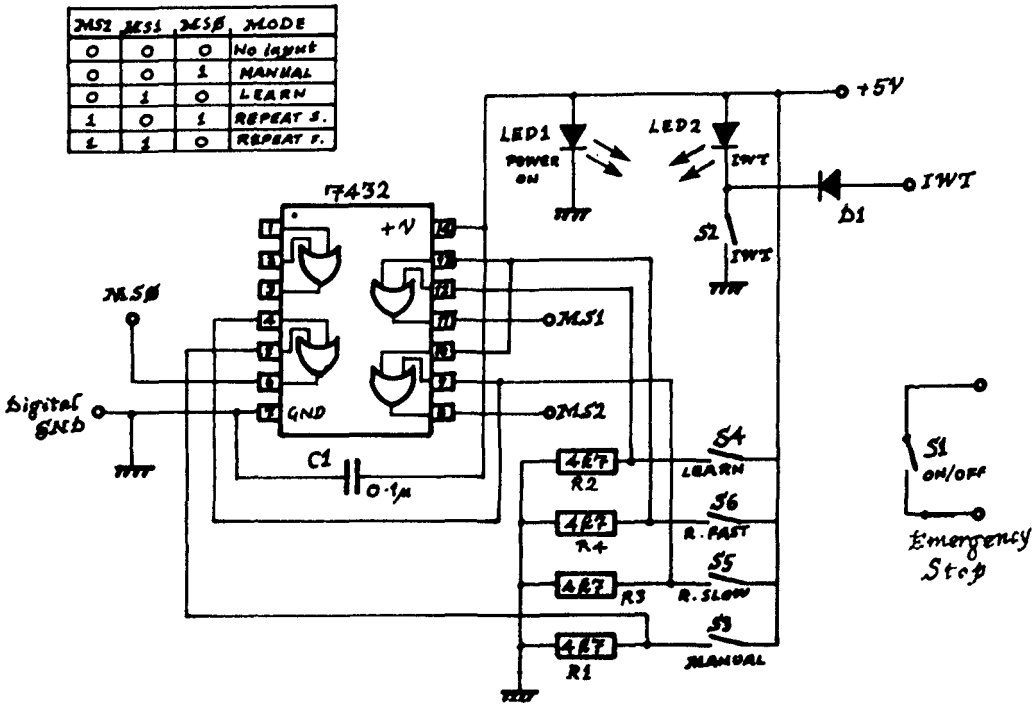


Fig. 8-3: Logic for Mode Selection

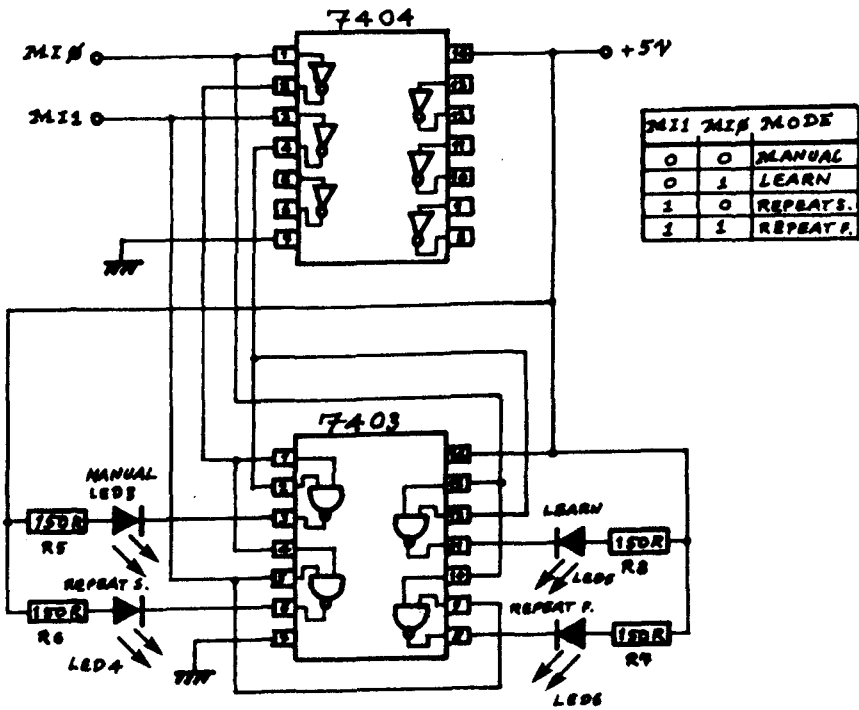


Fig. 8-4: Logic for Mode Indication

normally closed emergency stop switch is in series with the on/off switch and closes the path for operating the power switching relay. The mode indication circuit is shown in Fig. 8-4 and decodes the two mode indication lines MI0 and MI1 to operate the four LED's according to the truth table. The four NAND gates in the 7403 have open collector outputs, turning the corresponding LED on when the output goes low. The layout of the circuit board for the mode selection and indication circuits is shown in Fig. 8-5, and Fig. 8-6 shows the layout of the connecting strip mounted at the bottom of the case and the colour coding of the connector cable. Colour coding for the analogue control leads is given in Table 8-1.

<u>Joysticks</u>	
V _{ref}	Red
Gnd.	Black
Slew	Blue
Lift	Blue
Reach	Yellow
Bucket	Yellow

<u>Pitch Control</u>	
Wiper	Grey
V _{ref}	Violet
A. Gnd.	White

Table 8-1: Colour Coding of Analogue Control Leads

A top view of the control unit is shown in Plate X, and front view with it placed on the processor unit in Plate XI.

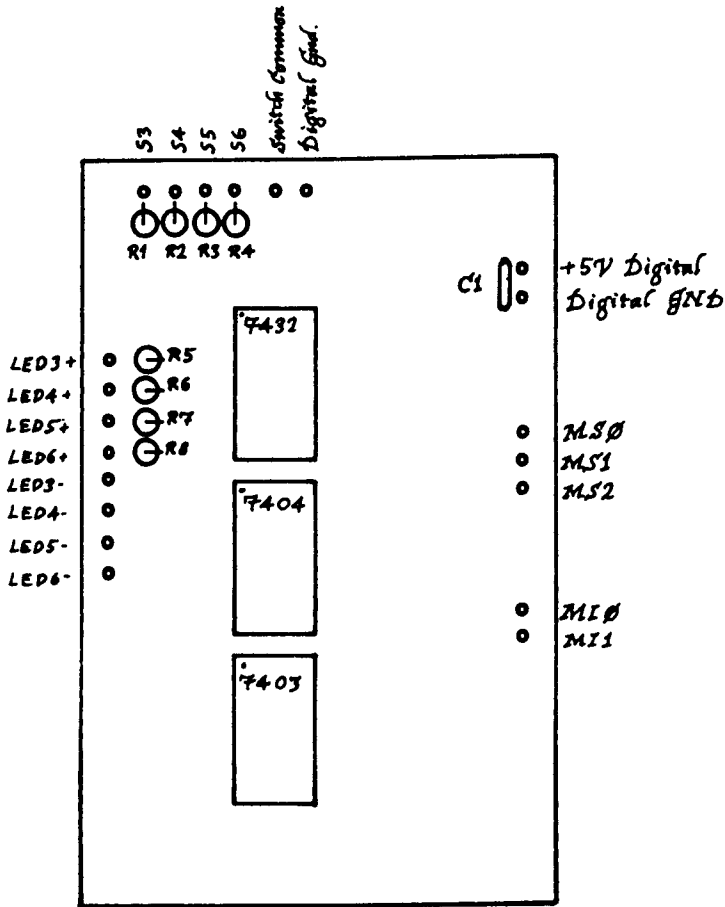


Fig. 8-5: Layout of Logic Board

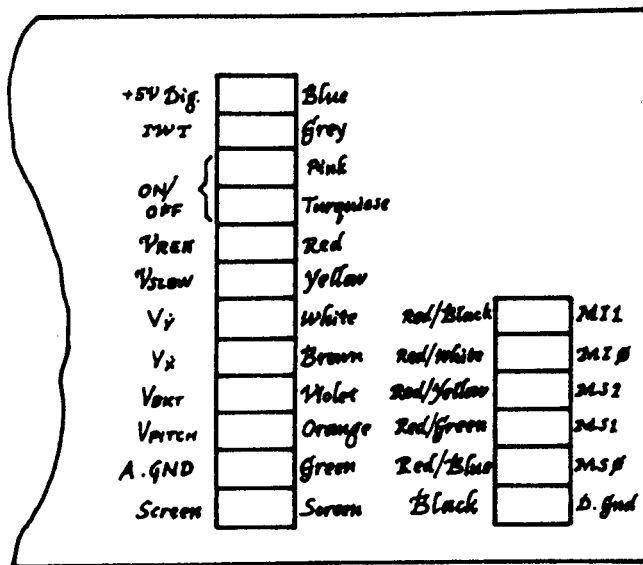


Fig. 8-6: Connector Layout & Control Cable Colour Coding

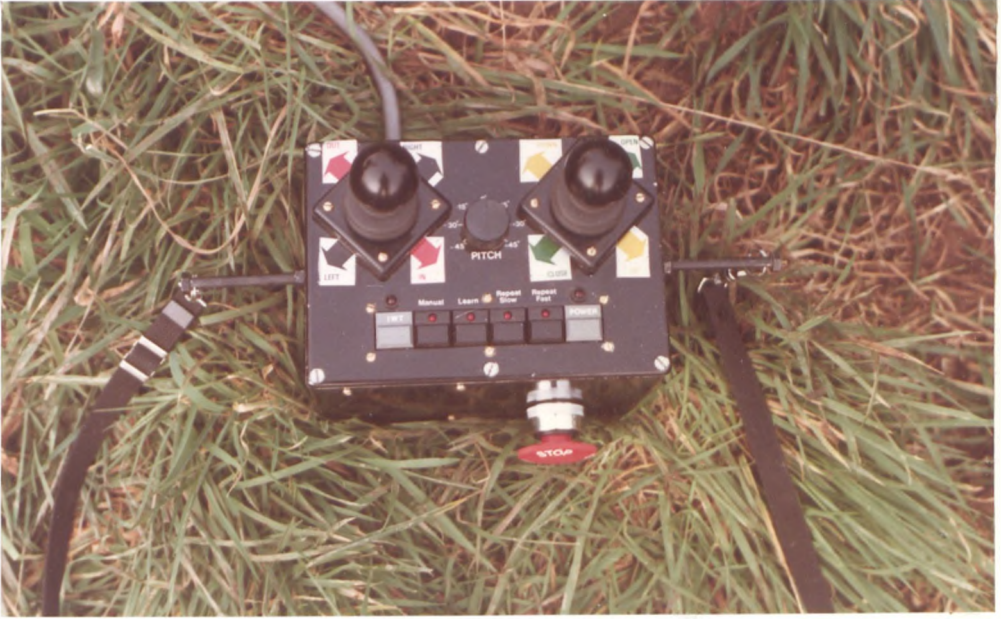


Plate XI: Top View of Control Unit

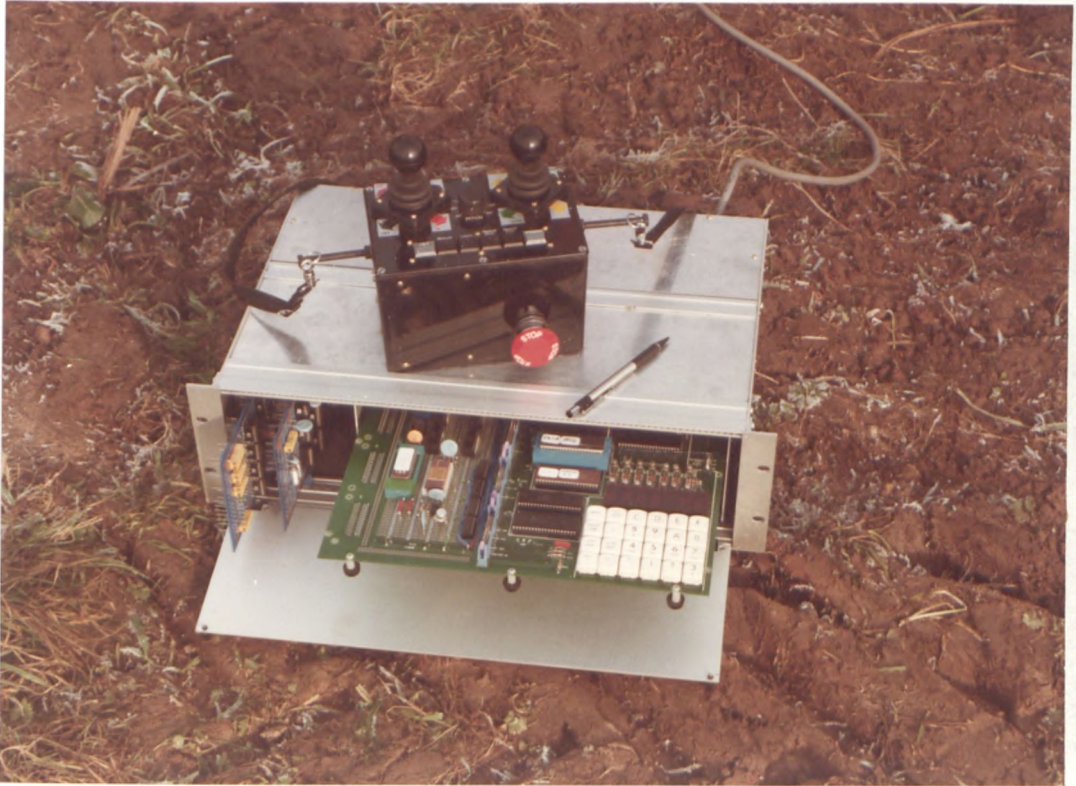


Plate XII: Control Unit & Processor Unit

8.2 Transducer Wiring

Fig. 8-7 and Plate XII show the wiring diagram and junction box mounted on the side of the digger. The cable to each transducer is screened to minimise any pick-up from electromagnetic fields. Linking each transducer to the junction box is an in-line connector so that each transducer may individually be disconnected and replaced. The use of a junction box also reduces the amount of cabling required to link the set of three transducers to the processor unit.

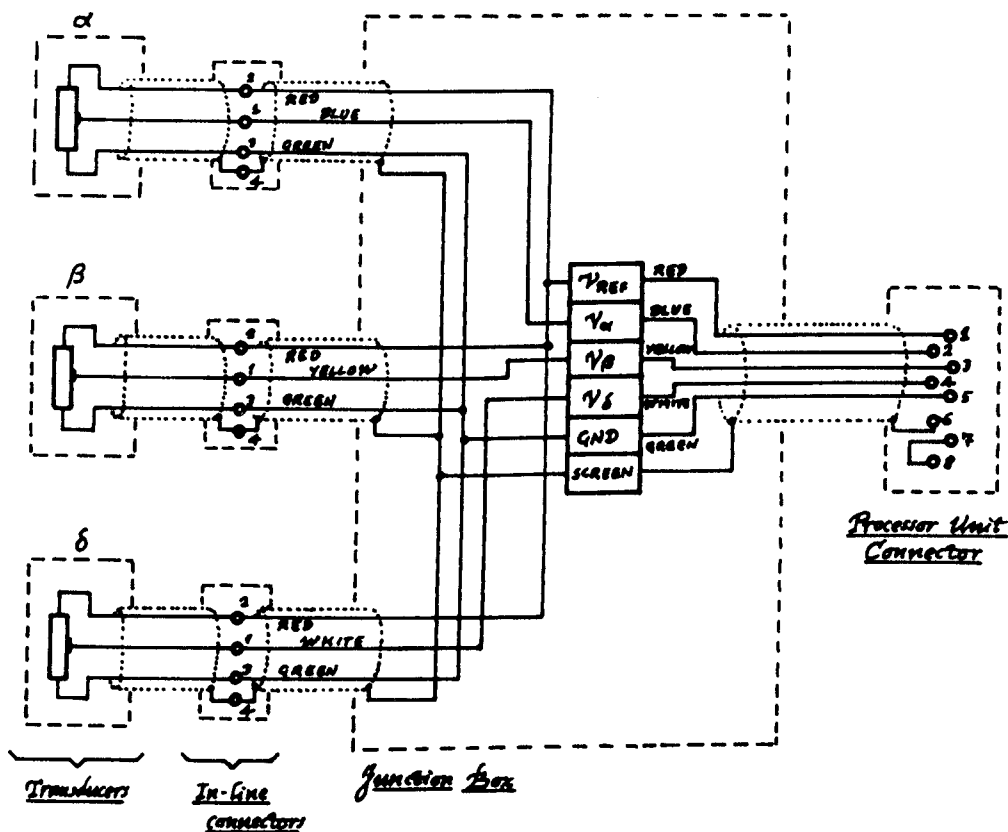
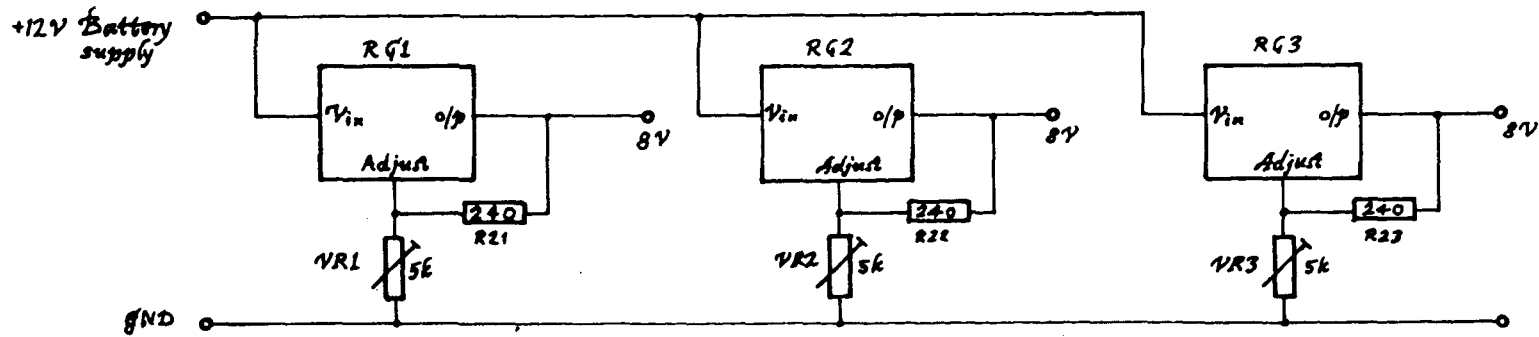


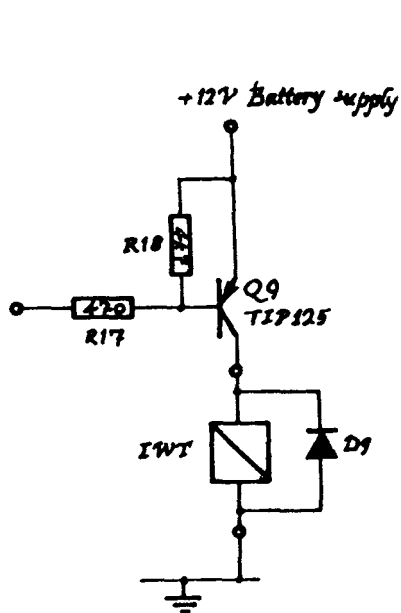
Fig. 8-7: Transducer Circuit

8.3 Power Switching Unit

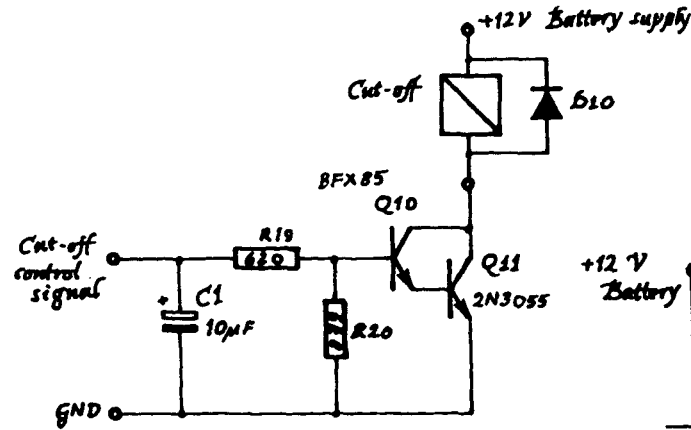
Fig. 8-8(a) shows the three regulator circuits for driving the solenoid valves at 8 V from the nominal 12 V tractor supply.



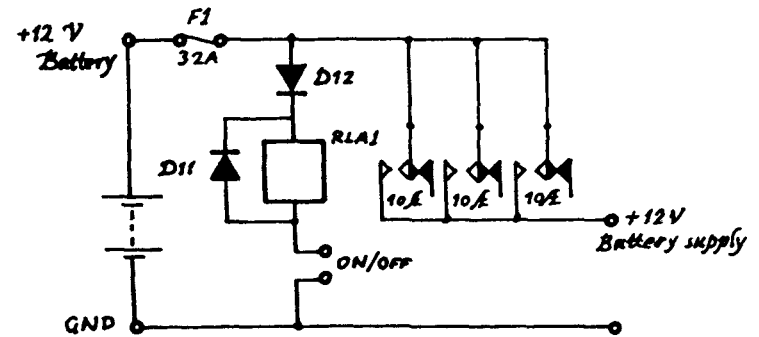
(a) Valve Supply Regulators



(b) IWT Valve Switching Circuit



(c) Cut-off Circuit



(d) Battery Switching Circuit

Fig. 8-8: Power Switching Unit Circuitry



Plate XIII: Side View of Machine Showing Junction Box & Transducer for Main Arm

The IWT valve is driven using a TIP125 transistor (Fig. 8-8 (b)). Resistor R17 limits the base current and R18 ensures that the transistor turns hard off. The operation of the cut-off circuit (Fig. 8-8 (c)) is to switch the cut-off valve using darlington pair Q10, Q11 and delay the turn-off of the valve using C1 and R19 so that the valve is held on between consecutive pulses from one or more proportional valves.

The power switching for the input to the system from the battery is effected using the circuit of Fig. 8-8 (d). Fuse F1 is rated at 32 A to protect the battery and the circuitry against any major short circuit. Relay RLA1 is used to switch the power to the system when the on/off control loop is closed. Diode D12 prevents the relay from operating if the supply is reverse connected by mistake, thus indefinite reverse supply connection does not damage the system.

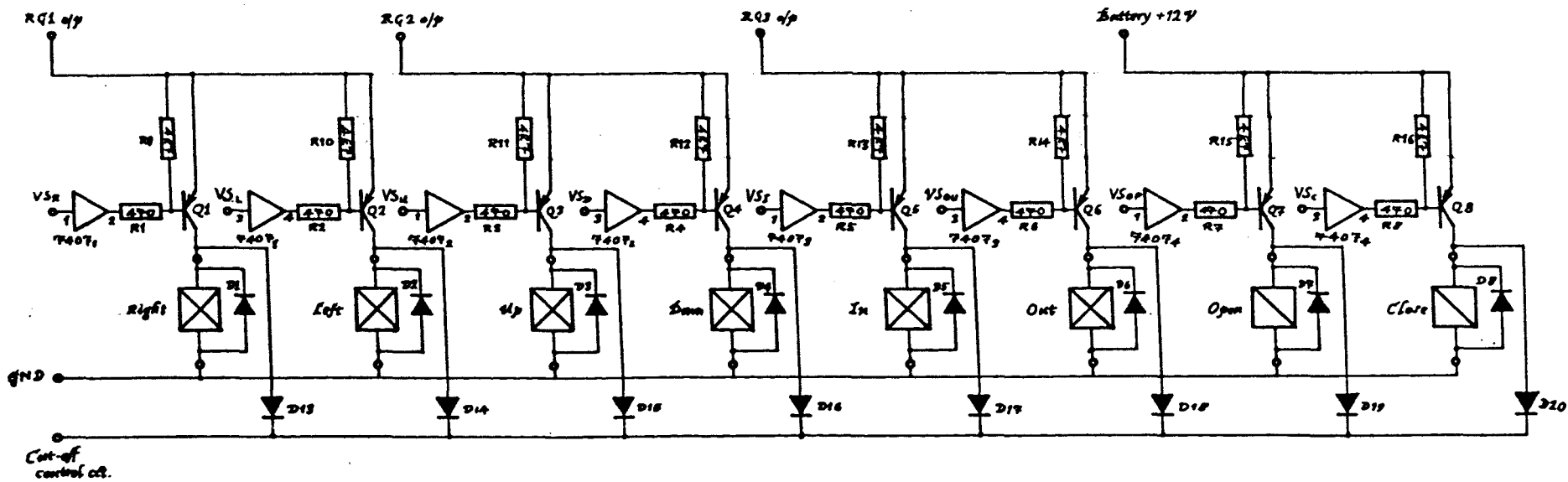




Fig. 8-9: Valve Switching Circuitry

- Q1-Q8: TIP125
 - D1-D10: 1N4001
 - D13-D20: 1N4001
- 

Proportional solenoid
- 

Bang-bang solenoid

Fig. 8-9 shows the complete circuit for the switching of all the proportional and bang-bang valves for the different services. The control inputs are buffered by the 7407 gates and the open collector gate outputs sink the base currents from the switching transistors Q1-Q8 . Diodes D13 to D20 link each of the valve solenoids to the cut-off control circuit while isolating the services from each other.

The circuit board layout is shown in Fig. 8-10 and the layout of the internal connector in Fig. 8-11 with the wiring details in Fig. 8-12. The colour coding of the control cable is shown in Table 8-2. Figures 8-13 and 8-14 show external views of the box and the component mounting configuration and cable gland layout. Plate XIII shows the switching unit on the digger with the cover plate visible at the left hand end and the cable glands to the right. Sealing cable glands and a screw-on lid to the box were used to prevent the ingress of moisture to this particularly exposed part of the system.

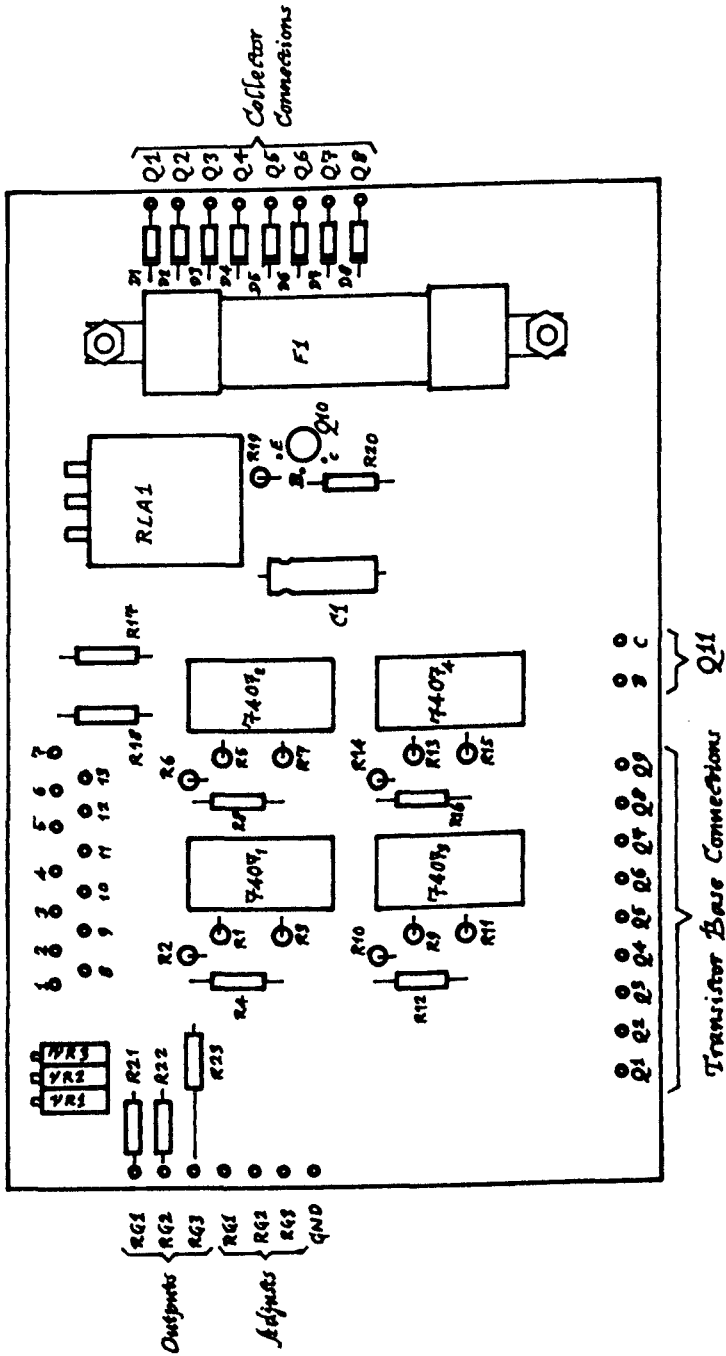


Fig. 8-10: Layout of Power Switching Unit Circuit Board

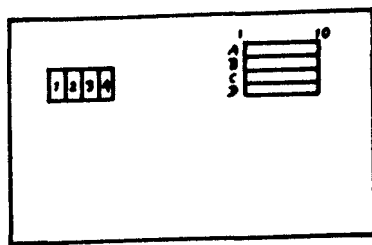


Fig. 8-11: Layout of Power Switching Unit Internal Connecting Blocks

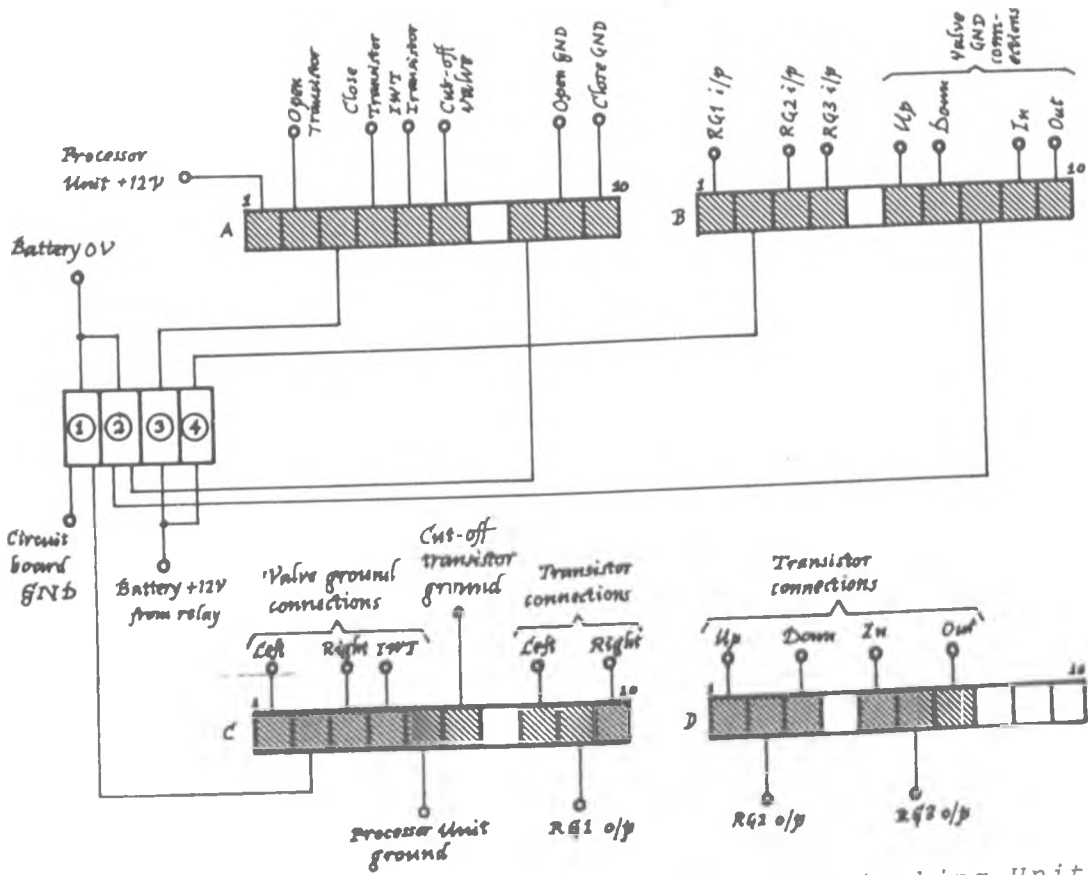


Fig. 8-12: Wiring Diagram of Power Switching Unit Connecting Blocks

Core	Colour	Function
1	Red	Up
2	Blue	Down
3	Yellow	In
4	White	Out
5	Black	Right
6	Brown	Left
7	Violet	Open
8	Orange	Close
9	Pink	IWT
10	Turquoise	On/Off
11	Grey	GND.
12	Green	n/c
13	Screen	n/c

Table 8-2: Colour Coding of Power Switching Unit Control Cable

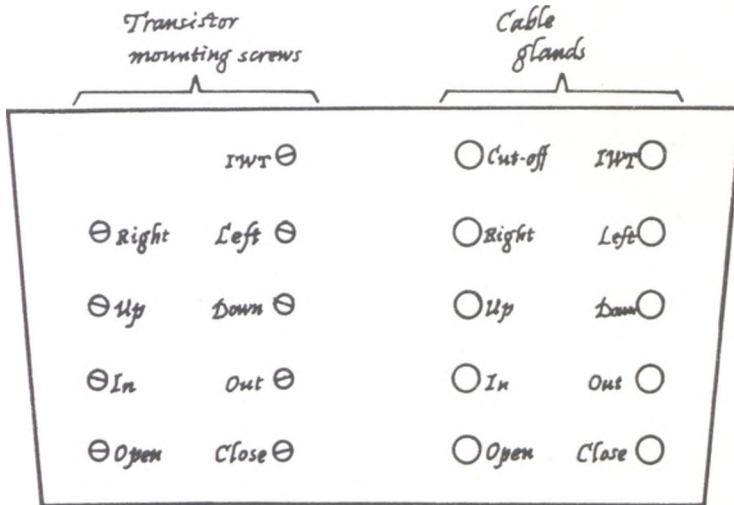


Fig. 8-13: Side View of Power Switching Unit Showing Layout of Power Transistors & Cable Glands

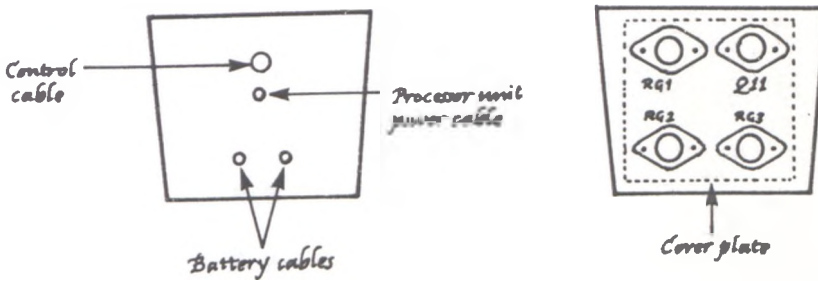


Fig. 8-14: End Views of Power Switching Unit Showing Semiconductors & Cable Glands



Plate XIV: Power Switching Unit

CHAPTER NINE

SOFTWARE I:

GENERAL PURPOSE APU SUBROUTINES & MACROS

- 9.1 Arithmetic Processor Unit
- 9.2 Subroutines for APU Stack Data Transfer
- 9.3 Subroutine for APU operations
- 9.4 Macro for Conditional Jumps

9.1 Arithmetic Processor Unit

The principal advantages of using an Arithmetic Processor Unit (APU) are its speed of operation and the ease with which complex computations may be programmed. Two major programs were written for controlling the digger:

MANCON which mimics the operation of a conventional mechanically controlled digger

and DIG which provides the features described in Chapter Two of automatic straight line cutting, pitch control, and the learn/repeat facility.

Both programs make extensive use of the APU and a set of macros and subroutines common to both programs was written to simplify data transfers and APU commands so that any calculation could be coded as a Reverse Polish sequence of instructions. A macro was also written to effect conditional jumps depending upon the relative values of two 32 bit floating point variables. All the system software was written in assembly language for the 8085A processor using an Intel Intellec Development System.

The arithmetic processor has as internal stack 16 bits wide by 8 levels deep for single precision values or 32 bits wide and 4 levels deep for double precision or floating point values (Fig. 9-1).

Data is entered on the stack in the sequence B1, B2, B3, B4 and removed in the reverse sequence. The stack is located at address 1000H. Commands are written to the APU as 8 bit words to the address 1100H and commands operate on either the

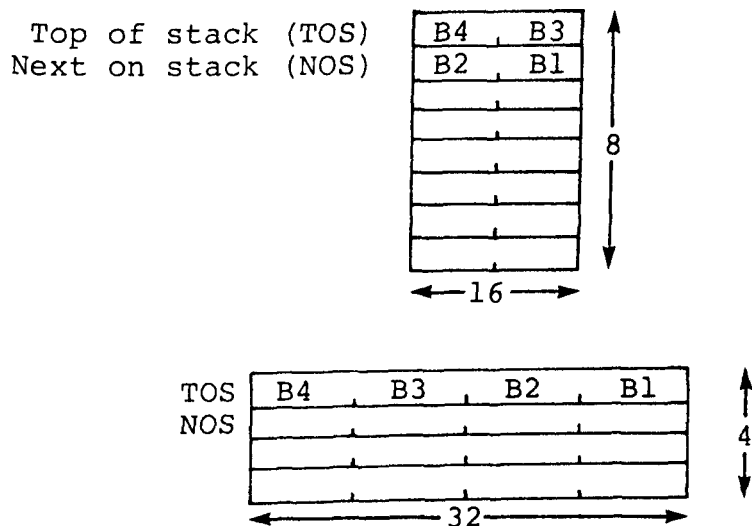


Fig. 9-1: APU Internal Stack Structures for Single and Double Precision Data

TOS or NOS or both. The device status (Busy, Sign, Zero, Error, etc.) may be read from the status register, also located at address 1100H.

Address	Data	
n	byte 0	l.s. byte
n+1	byte 1	
n+2	byte 2	
n+3	byte 3	m.s. byte

Fig. 9-2: Data Format for 32 Bit Floating Point Variable

Thirty-two bit floating point variables and constants used in the programs are stored in RAM or EPROM as a sequence of four consecutive bytes as shown in Fig. 9-2 with the least significant byte at the lowest address. The variable name or identifier acts as a label to the address of the least significant byte.

9.2 Subroutines for APU Stack Data Transfer

Subroutine PSHT pushes a 32 bit variable onto the APU stack. Register pair DE, used as a data pointer, controls the

address of the least significant byte on calling and of the most significant byte at return (see Fig. 9-3).

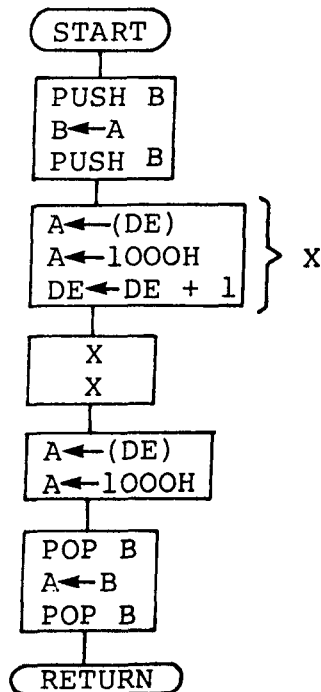


Fig. 9-3: Flowchart of Subroutine PSHT

A more efficient coding for storing the A register would be PUSH PSW, and for recovering it POP PSW.

Subroutine PLLT pulls a 32 bit variable from the APU stack. Register pair DE, used as a data pointer, contains the address in memory of the least significant byte of the variable (see Fig. 9-4).

A more efficient coding for storing the A register would be PUSH PSW, and for recovering it Pop PSW.

Macro PSH generates the code for pushing a 32 bit variable onto the APU stack using subroutine PSHT.

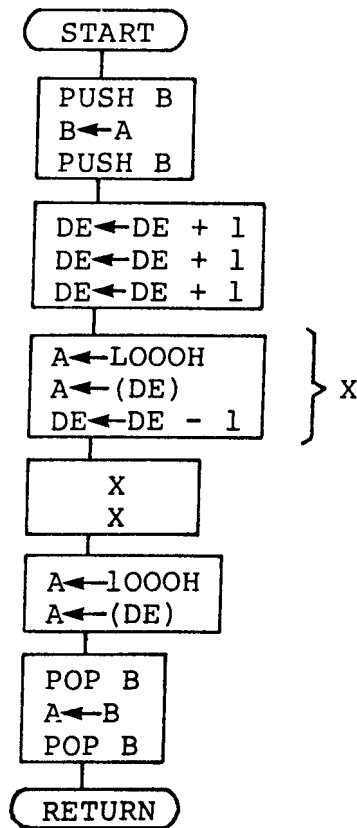


Fig. 9-4: Flowchart of Subroutine PLLT

The call instruction is of the form

PSH var

Where var is the identifier of the variable to be pushed, and the corresponding code generated by the macro is

```

LXI    D,var          ;Load data pointer
CALL   PSHT             ;Call APU stack push
                               subroutine
  
```

Macro PLL generates the code for pulling a 32 bit variable from the APU stack using subroutine PLLT.

The call instruction is of the form

PLL var

Where var is the identifier of the variable to be pulled, and the corresponding code generated by the macro is

```
LXI  D,var           ;Load data pointer
CALL  PLLT          ;Call APU stack
                        pull subroutine
```

9.3 Subroutines for APU Operations

Macro MATHS generates subroutines which when called give commands to the APU to perform different arithmetic operations.

The calling instruction is of the form

```
MATHS  function,code
```

Where function is the name of the operation carried out by the APU and the name of the subroutine generated by the macro and code is the 8 bit code written to the APU command register to carry out the required operation.

The macro generates code of the form

```
function:  STA  ASTR      ;put A reg. in
                        temporary location
            MVI  A,code   ;A←APU op code
            STA  1100H     ;A→APU command
                        register
            LDA  ASTR      ;restore A register
            RET
```

Registers affected: None

Subroutine FIX is used to convert the 32 bit floating point

contents of the TOS to 8 bit integer format in the A register (see Fig. 9-5).

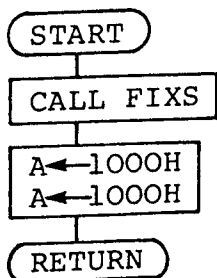


Fig. 9-5: Flowchart of Subroutine FIX

Subroutine FLOAT converts the 8 bit integer contents of the A register to 32 bit floating point format on top of the APU stack (see Fig. 9-6).

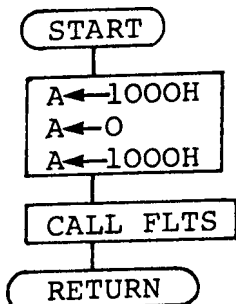


Fig. 9-6: Flowchart of Subroutine FLOAT

9.4 Macros for Conditional Jumps

Macro IFF generates code for conditional jumps depending upon the relative values of two floating point variables. It generates code to operate as follows:

```

IF var1{>|≥|=|*|≤|<}var2
  THEN GOTO label
  ELSE CONTINUE
  
```

The calling statement is of the form

IFF var1, {GTHAN|GEQUAL|EQUALS|NEQUAL|LEQUAL|
LTHAN}, var2, label

and the macro generates code as in the flowchart of Fig. 9-7.

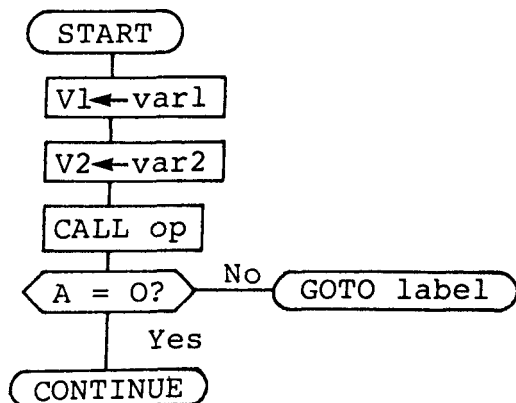
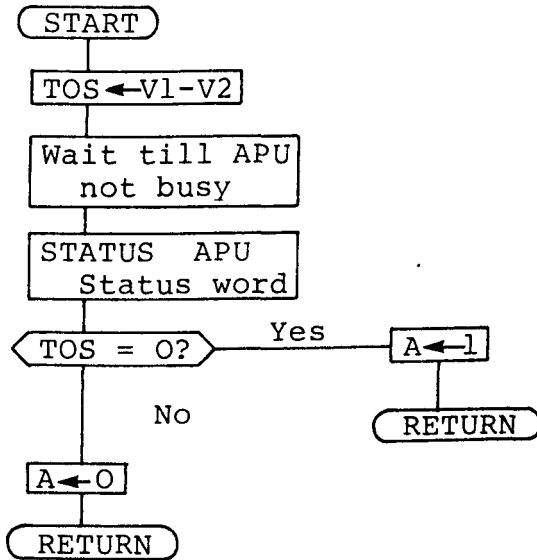
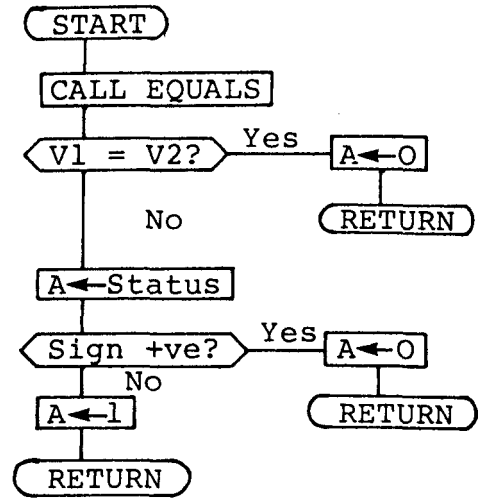


Fig. 9-7: IFF Macro Object Code

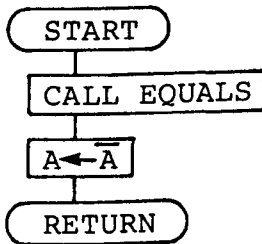
Subroutine *op* tests the validity of the relational operator (>, ≥, etc.) on V1 and V2, returning the result as True (1) or False (0) in the A register. The different cases for subroutine *op* are flowcharted in Fig. 9-8.



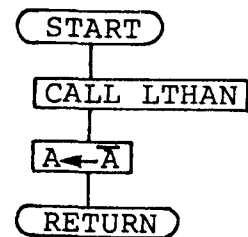
(a) Subroutine EQUALS



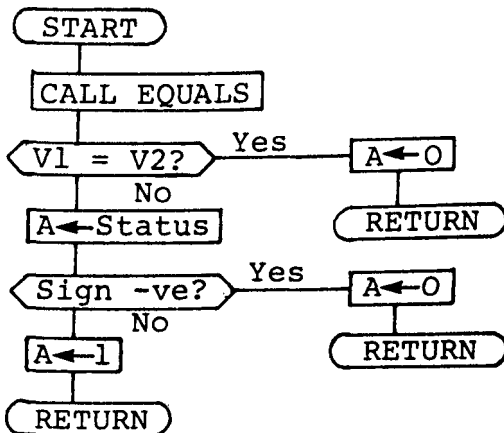
(d) Subroutine LTHAN



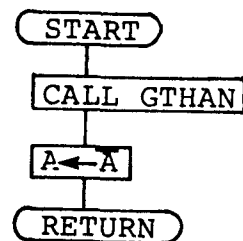
(b) Subroutine NEQUAL



(e) Subroutine GEQUAL



(c) Subroutine GTHAN



(f) Subroutine LEQUAL

Fig. 9-8: (a)-(f) Flowcharts of Relational Operator Subroutines called in Object Code of IFF Macro

CHAPTER TEN:

SOFTWARE II:
PROGRAM MANCON

- 10.1 Introduction
- 10.2 Algorithm
- 10.3 Memory Utilisation
- 10.4 Code Documentation

10.1 Introduction

Program MANCON simulates the operation of a conventional mechanical control system, opening each hydraulic valve in relation to the corresponding joystick deflection. In addition to the routines for utilisation of the arithmetic processor described in the previous chapter there are a number of subroutines common to program MANCON and program DIG, which is described in the next chapter. These common subroutines are mainly for input and output.

10.2 Algorithm

The flowchart for the main program is shown in Fig. 10-1 indicating which code segment, the main program or a subroutine, executes each function.

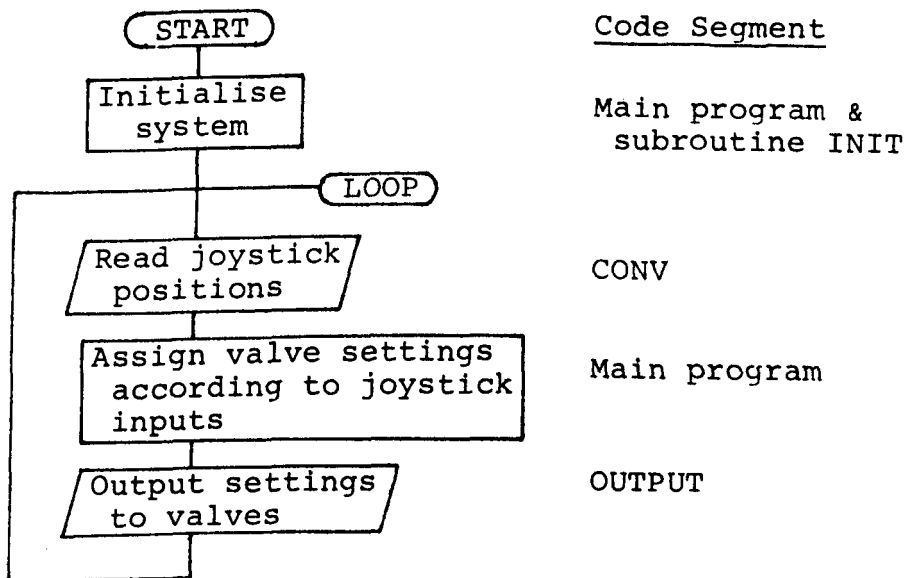


Fig. 10-1: Flowchart for Main Program

The executable code begins at address 80D0H in ROM with the system initialisation procedure. Default values of characteristic

constants for the valves are copied from ROM into RAM. This is so that the constants may be changed by the user when operating the system and program execution may be resumed from location 80E0H to avoid corrupting the modified data. The interrupts and stack pointer are initialised to allow the program to be interrupted at a selected point when the Vectored Interrupt key on the keyboard is depressed. Subroutine INIT sets the I/O port data direction registers.

Location 20CEH in RAM, to which control jumps when the Vectored Interrupt key is pressed, is loaded with the instruction code CFH (RST1) to return control to the monitor.

The main control loop first calls subroutine CONV which reads in the joystick deflection JXDOT, JYDOT, JBKT, and JSLEW corresponding to Lift, Reach, Bucket, and Slew. These variables are assigned values in the range -1 to +1 according to the magnitude and sense of the corresponding joystick deflections.

The values of JXDOT, JYDOT, JBKT, and JSLEW are copied via the top of the APU stack to variables VVBETA, VVALFA, VVBKT, and VVSLEW which are the corresponding valve settings.

Subroutine OUTPUT is then called and sets the control signals for the valve drivers. The final part of the main control loop allows an interrupt from the 'Vectored Interrupt' key of the monitor; this allows the program to be halted at this specific

point so that the values of variables may be examined. Control then jumps back to the start of the main control loop.

Memory Utilisation

The basic memory utilisation for the program is shown in Fig. 10-2. Program variables are stored in RAM (block A); certain constants, those describing valve characteristics, are also stored in RAM (block B). Default values of user alterable constants are stored in EPROM in block C, and fixed constants in block D. The program code is stored in ROM in block E.

RAM		
3000H	A	Program variables
3043H		
3044H	B	User-alterable constants
304FH		
EPROM		
8000H	C	Default constant values
800BH		
800CH	D	Constants
803BH		
80DOH	E	Program code
8550H		

Fig. 10-2: Memory Map

The control structure for setting up default constants is shown in Fig. 10-3. Normally program execution begins at START A and the default constant values are copied from Block C to block B then control moves to the main routines. If the

program is halted by depression of the Vectored Interrupt button or Reset then the user alterable constants may be changed and program execution recommenced from START B to preserve the modified data values.

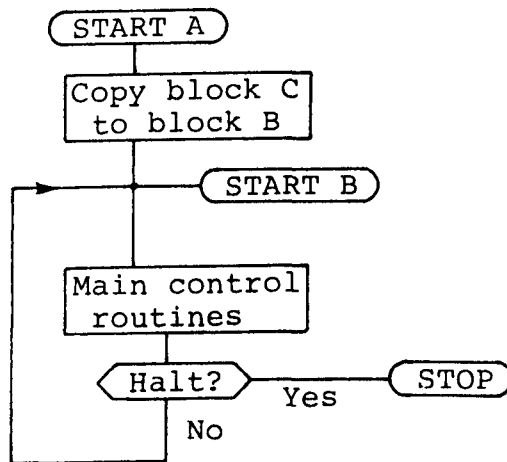


Fig. 10-3: Control Structure for Setting Default Constants

10.4 Code Documentation

Line numbers refer to those on the listing included in Appendix A.

Subroutine INIT (lines 203-210)

This subroutine writes the appropriate bit patterns to the I/O port data direction registers as given in Table 10-1.

Registers affected: A

Subroutine CONV (Lines 219-246)

This subroutine reads the output from each joystick axis

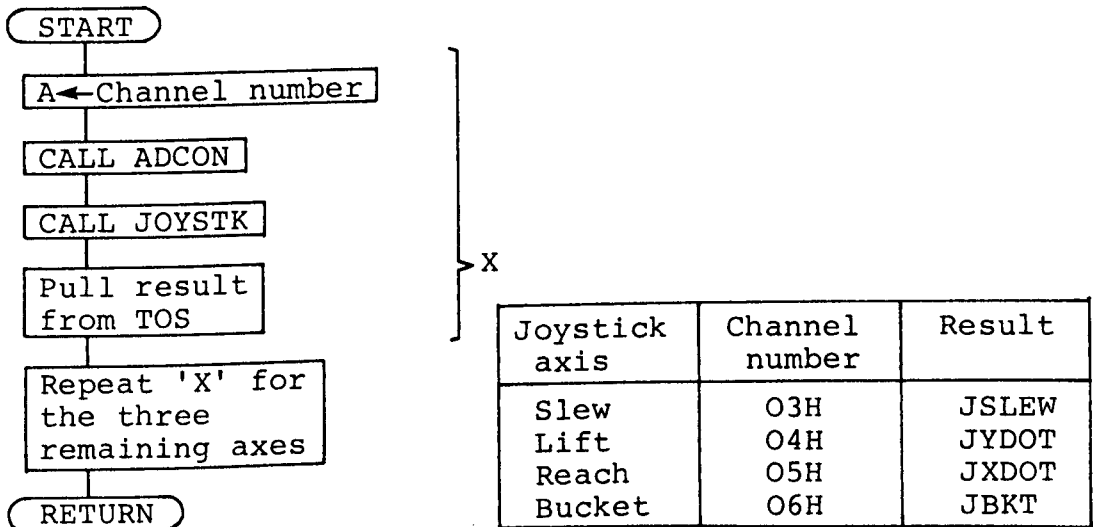


Fig. 10-4: Flowchart for Subroutine CONV

using subroutine ADCON and sends the result to subroutine JOYSTK which transfers the result to the range -1 to +1 in 32 bit floating point format. This process is effected four times to obtain values for the Slew, Lift, Reach, and Bucket joystick axes. The subroutine is flowcharted below in Fig. 10-4 and the table gives the channel number and result name for the different

I/O Port Address	Function	Data Direction	Data Direction Register	Control Byte
21H	Reach	Out	} 20H	OFH
22H	Bucket	Out		
23H	Mode indicate	Out		
00H	Slew	Out	02H	FFH
01H	Lift	Out	03H	FFH
29H	ADC Bus	In	} 28H	OCH
2AH	Mode select	In		
2BH	ADC Control	Out		

Table 10-1: I/O Port Usage and Control Bytes

Registers affected: A,D,E,H,L, Status

Subroutine ADCON (lines 259-273)

This subroutine operates the analogue to digital converter. The channel number is passed to the routine in the A register and the A register contains the eight bit result at return. The flowchart for the routine is shown in Fig. 10-5.

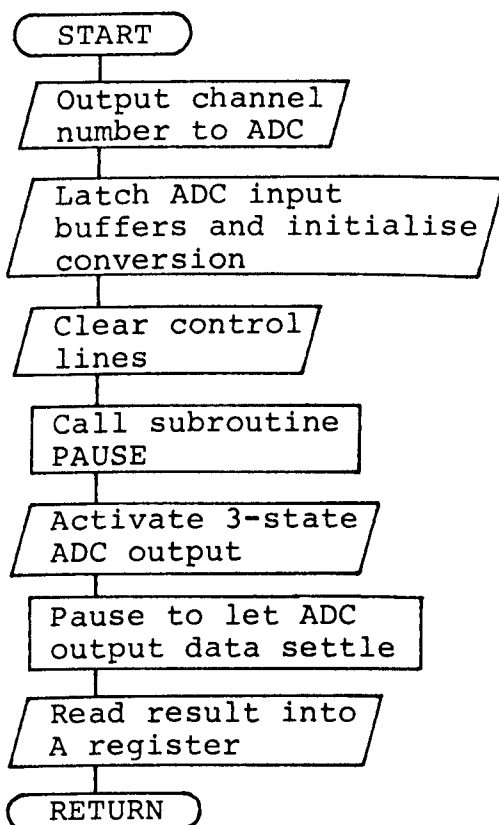


Fig. 10-5: Flowchart for Subroutine ADCON

Registers affected: A, H, L, Status

Subroutine PAUSE (lines 284-288)

This subroutine effects a delay, the duration of which is determined by the contents of the HL register pair on calling and given by the formula

$$\text{Delay} = (0.008 C + 0.013) \text{ ms}$$

Where C = value of counter in HL register pair on calling.

The subroutine flowchart is given in Fig. 10-6.

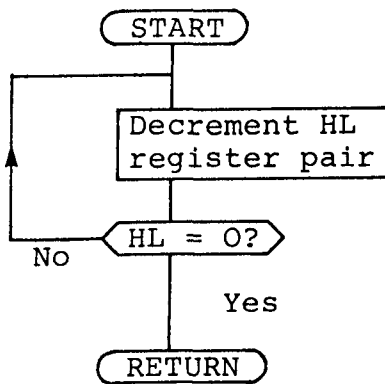


Fig. 10-6: Flowchart for Subroutine PAUSE

Registers affected: H, L.

Subroutine JOYSTK (Lines 439 - 505)

This subroutine converts the eight bit joystick voltage to the range -1 to +1, corresponding to the full mechanical travel of the lever. This is shown graphically in Fig. 10-7 and Fig. 10-8 gives the program flowchart.

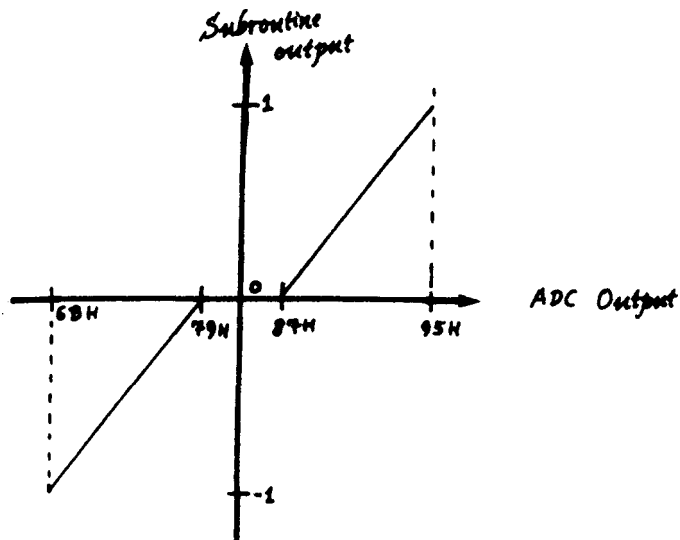


Fig. 10-7: Transfer Characteristic of Subroutine JOYSTK

Registers affected: A, D, E, Status.

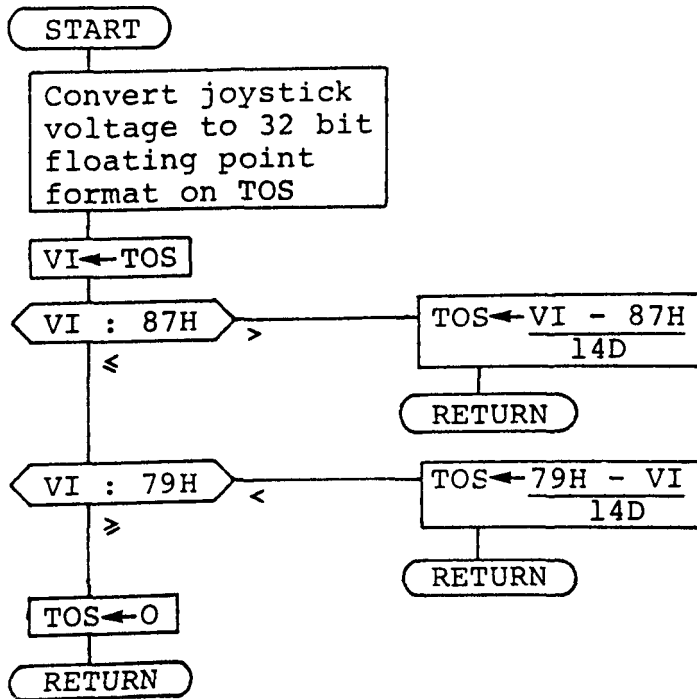


Fig. 10-8: Flowchart for Subroutine JOYSTK

Subroutine OUTPUT (lines 519 - 622)

This subroutine takes as input parameters the fractional valve openings VVSLEW, VVALFA, VVBETA, and VVBKT. They are offset and scaled in turn by subroutine VLIN to give the required valve control bytes which are then output to the valve drivers. The subroutine has the following input parameters.

Fractional valve opening	FVO
Positive Offset	POF
Positive Maximum	PMAX
Negative Offset	NOF
Negative Maximum	NMAX

The driver control byte is returned in the A register.

The input parameter names for the different valves are as follows:

	Slew	Lift	Reach
FVO	VVSLEW	VVALFA	VVBETA
POF	SPOF	APOF	BPOF
PMAX	SPMAX	APMAX	BPMAX
NOF	SNOF	ANOF	BNOF
NMAX	SNMAX	ANMAX	BNMAX
Control byte	VS	VL	VR

The bucket is controlled by a bang-bang valve and is operated by a separate piece of code which switches the bucket valve according to the sign of VVBKT.

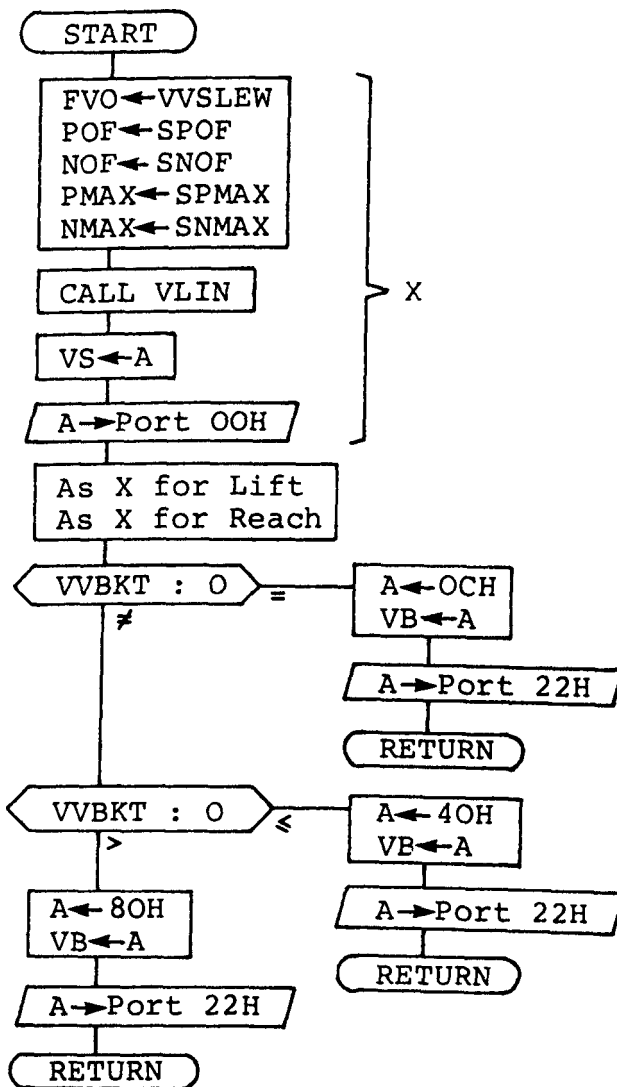
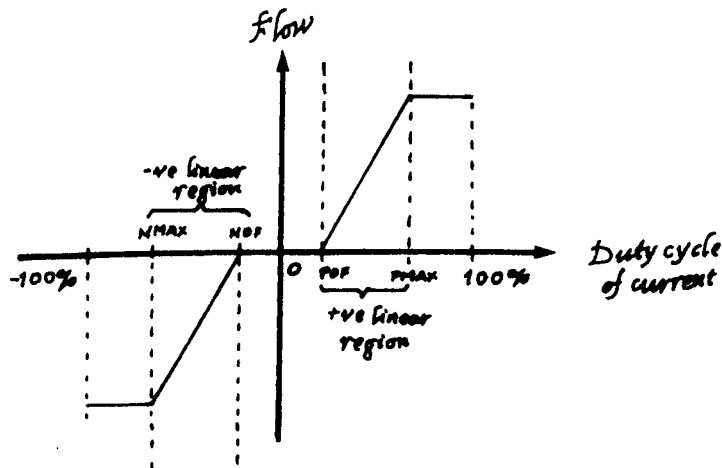


Fig. 10-9: Flowchart for Subroutine OUTPUT

Subroutine VLIN (Lines 661 - 761)

This subroutine derives the control byte to be output to a proportional valve given the demanded fractional valve opening and a set of parameters describing the valve characteristics. The demanded fractional valve opening (FVO) is expressed as a 32 bit floating point quantity in the range -1 to +1. The simplified characteristic of a valve is shown in Fig. 10-10.



POF - Positive Offset
 PMAX - Positive Maximum
 NOF - Negative Offset
 NMAX - Negative Maximum

Fig. 10-10: Simplified Valve Characteristic

The subroutine maps an input in the range 0 to -1 onto the negative linear region. The format of the control word is as shown below in Fig. 10-11.

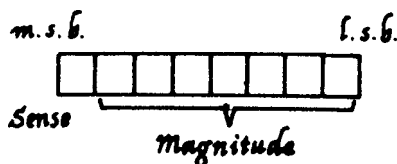


Fig. 10-11: Valve Driver Control Word Format

The most significant bit gives the sense of the movement as follows:

	1	0
Slew	Right	Left
Lift	Up	Down
Reach	In	Out

The seven least significant bits determine the magnitude of the mark to period ratio (duty cycle) of the valve current. The magnitude is calculated for positive inputs as

$$\text{Magnitude} = \text{POF} + \text{FVO} (\text{PMAX} - \text{POF})$$

and for negative inputs

$$\text{Magnitude} = \text{POF} + \text{FVO} (\text{NMAX} - \text{NOF})$$

The subroutine flowchart is shown in Fig. 10-12.

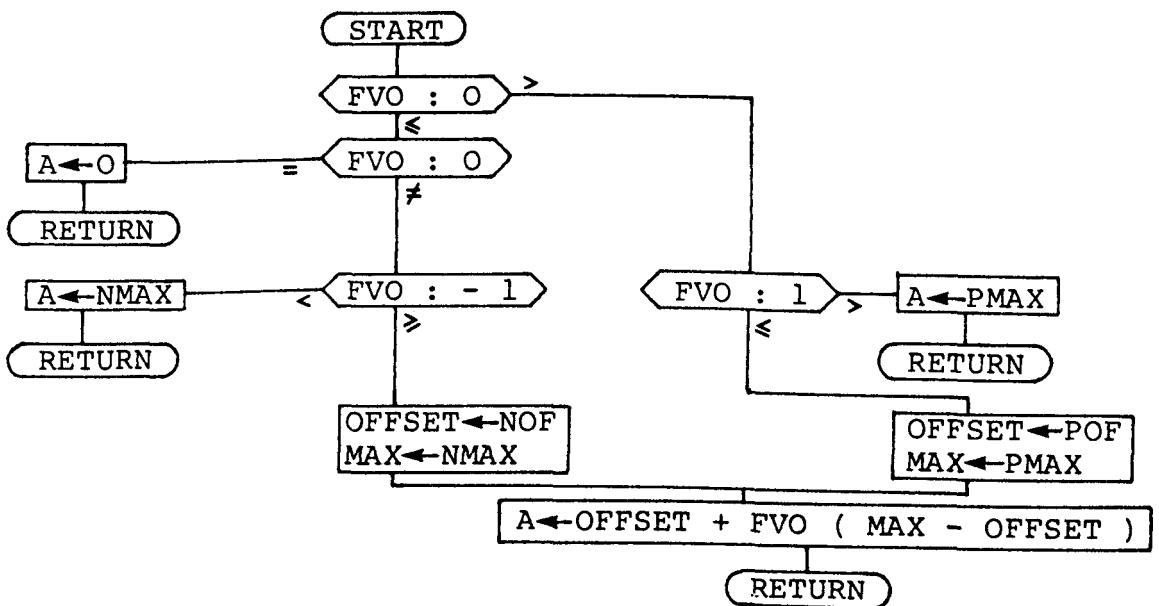


Fig. 10-12: Flowchart for Subroutine VLIN

Registers affected: A, D, E, Status.

CHAPTER ELEVEN

SOFTWARE III:

PROGRAM DIG

- 11.1 Functional Description & Algorithms
- 11.2 Memory Utilisation
- 11.3 Code Documentation

11.1 Functional Description and Algorithms

Program DIG is the main control program which implements the function specified in Chapter Two of automatic linear cutting of the blade, calibrated variable pitch, and a learn and repeat facility. The program effects four modes of machine operation:-

Manual: 'X-Y' control of bucket movement, Bucket Angle and Slew from joysticks. Calibrated Pitch control.

Learn: Control is as for Manual but path is recorded as a sequence of X, Y, ψ , coordinates. Any path previously recorded is overwritten.

Repeat Slow: Path is repeated at a slow speed from the machine position when the mode is selected. If this mode is selected when the machine is already in repeat fast mode, the path is not recommenced but continued at the slow speed.

Repeat Fast: Path is repeated at maximum speed from the machine position when the mode is selected. If this mode is selected when the machine is already in Repeat Slow mode, the path is not recommenced but continued at the higher speed.

Figure 11-1 illustrates the different possible mode transitions and the conditions causing them. The flowchart for mode control, which is the highest level of the machine software is shown in Fig. 11-2.

Manual Mode

The manual routine, flowcharted in Fig. 11-3 first sets the mode indicator on the control panel and then enters the main loop. Subroutine XY reads in the machine position and control

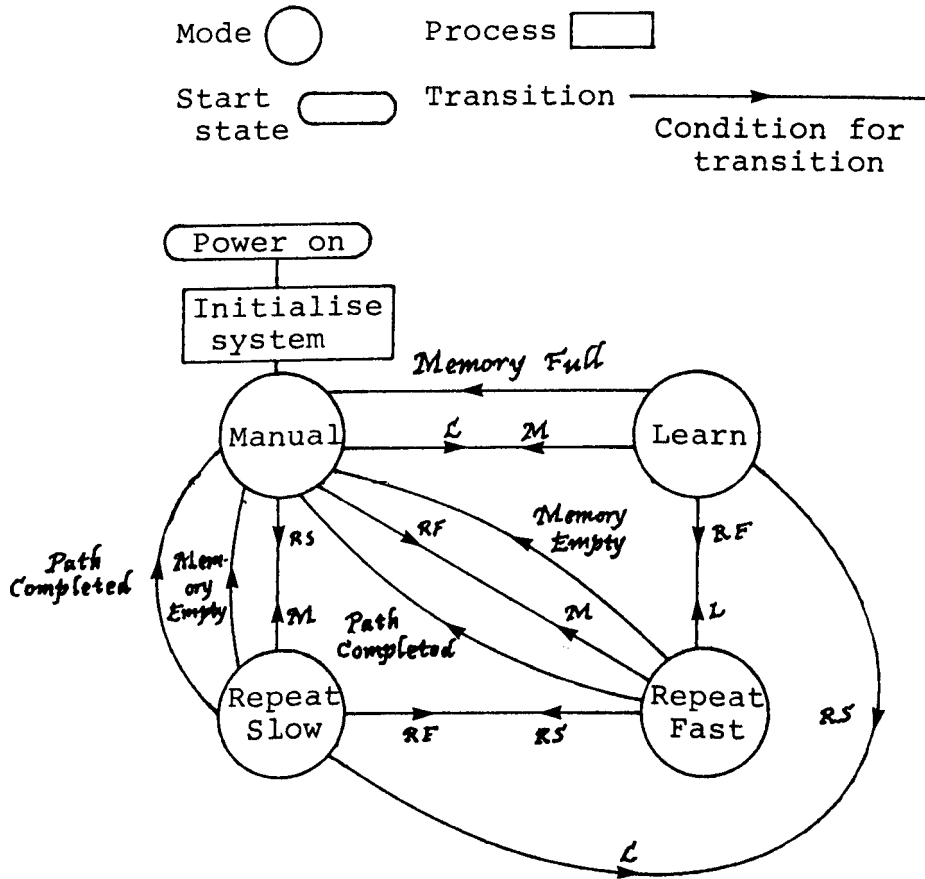


Fig. 11-1: Modes and Mode Transitions

inputs and sets the control valves accordingly. If any mode select key has been depressed then control returns to the main mode control program. The Vectored Interrupt key is briefly enabled so that program operation may be checked, which completes the sequence of operations of the subroutine's main control loop.

Learn Mode

The learn routine allows the user to control the machine as in Manual mode but equi-spaced points in the current X-Y coordinate framework are stored sequentially in memory as the

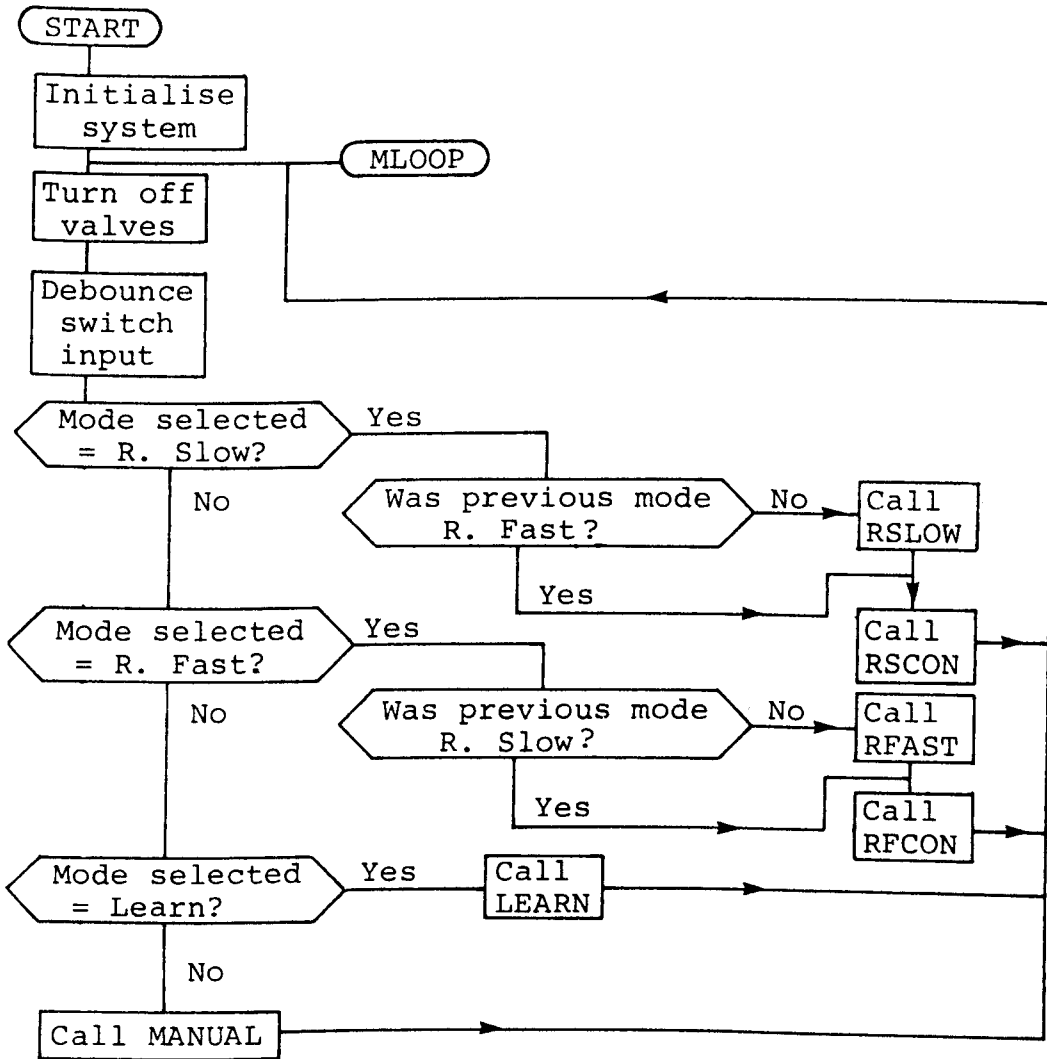


Fig. 11-2: Flowchart for Mode Control

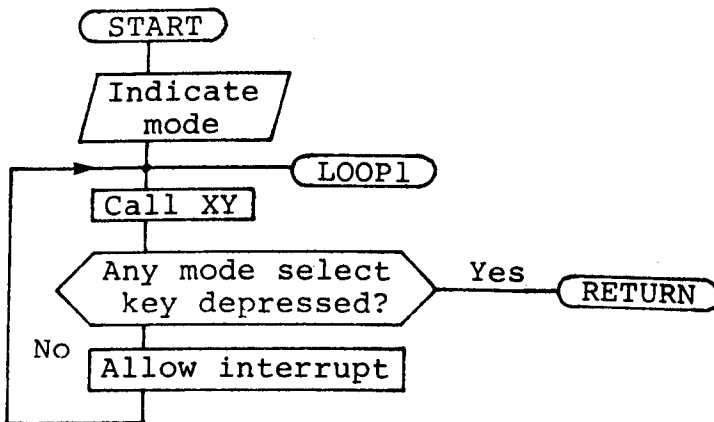


Fig. 11-3: Flowchart for Manual Mode

machine moves. The first point stored is the initial position of the machine when the mode is selected. The routine starts (see Fig. 11-4) by indicating the mode by the appropriate LED on the control panel, then the data pointer and counter are initialised and the current output position stored.

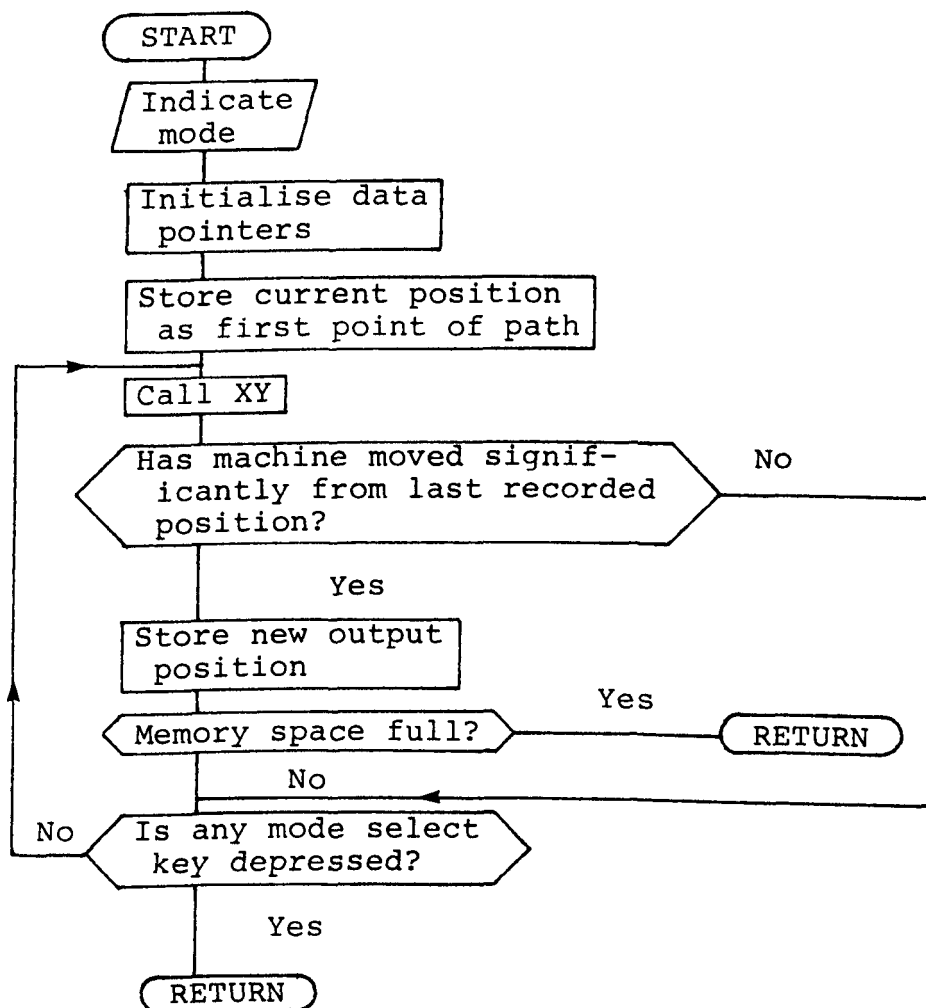


Fig. 11-4: Flowchart for Learn Mode

In the main loop of the subroutine, subroutine XY is called to read the machine inputs, output position, and to set the valve outputs. The updated machine output position is compared with the latest stored value and if the separation is greater than a critical value then the new position is recorded. Thus

approximately equi-spaced points are stored as the trajectory is executed and there is no time constraint upon the operator as would be imposed by sampling at regular time intervals. Once the memory is full then control returns to the mode selection program which defaults the system to manual mode. Control may also leave Learn Mode if one of the mode selection keys is depressed.

Repeat Slow and Repeat Fast Modes

The essential operation of the routine is to feed the stored path points to the position control program as target points, offset to accommodate the new starting point. The stored points are approximately equi-spaced so the delay between each point controls the speed. The main program for Repeat Slow mode is flowcharted in Fig. 11-5.

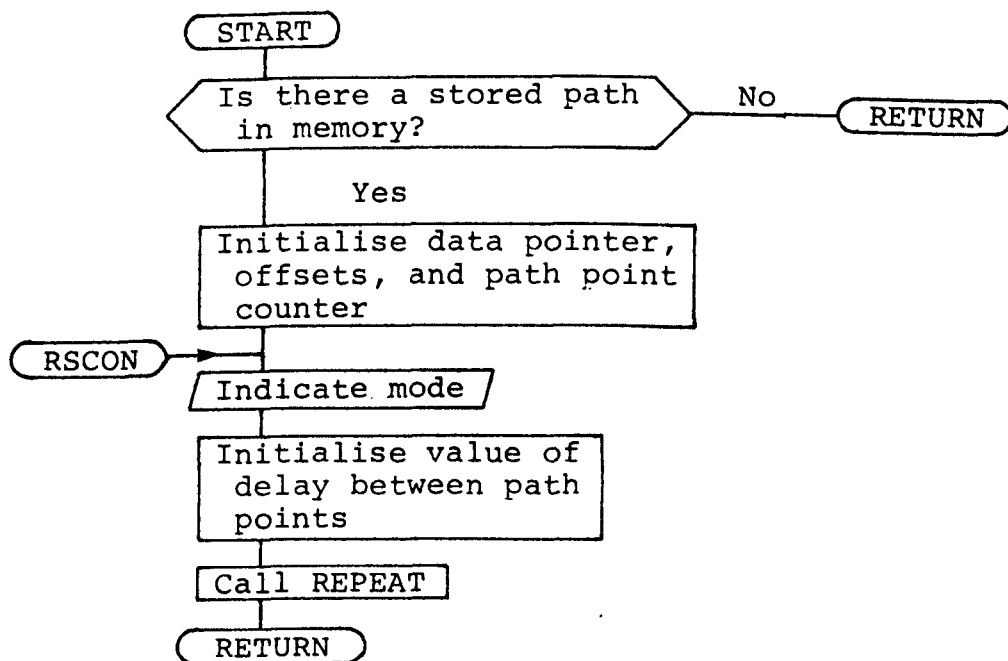


Fig. 11-5: Flowchart for Repeat Slow Mode

The routine starts by checking that there is a path stored in memory and if there is not, control returns to the calling program. If there is a path in memory, the data counter which counts the successive path points is set to zero, and the data pointer to the base address for the stored path. If Repeat Slow mode is selected while the system is in Repeat Fast mode then the path being repeated at the mode change is continued at the new slow speed, so control enters at point RSCON. The Repeat Slow mode indicator on the control panel is then set. The value for the delay between successive path points is set and this determines the speed at which the path is repeated. Subroutine REPEAT is then called which has as calling parameters the number of path points, the data pointer, and the delay between points.

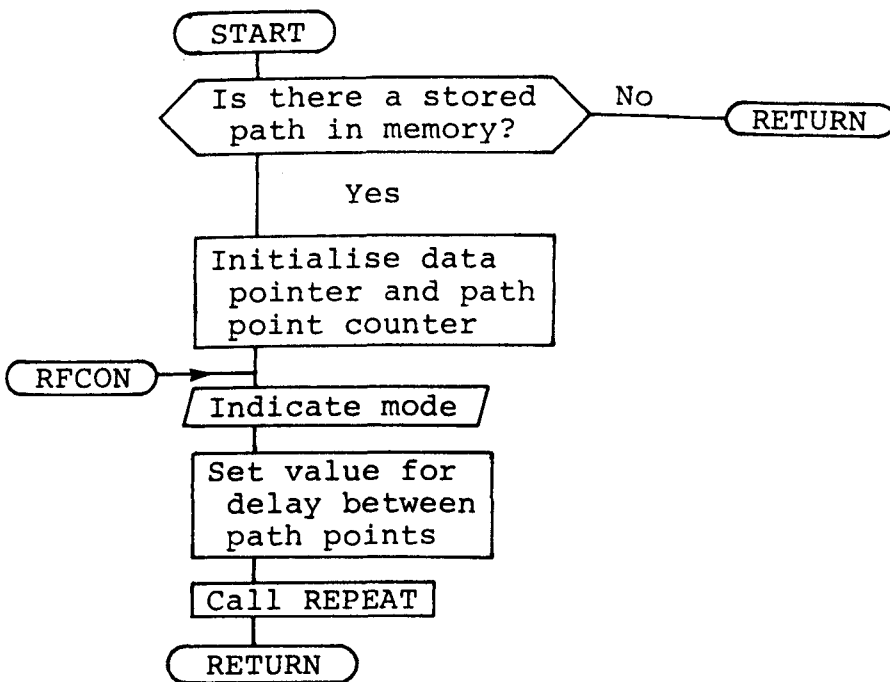


Fig. 11-6: Flowchart for Repeat Fast Mode

The operation of Repeat Fast mode (see Fig. 11-6) is very similar to that of Repeat Slow mode described above. Entry point RCON is used when the mode is changed from Repeat Slow to Repeat Fast so that the path being repeated is continued but at a higher speed. No additional delay is introduced between path points so the path execution is as fast as the system will allow.

11.2 Memory Utilisation

In program DIG, as for program MANCON described in the previous chapter, certain program constants are made user alterable by storing them in RAM, allowing access through the SDK-85 monitor. Default values of the constants are stored in ROM and these are loaded into RAM by the first segment of the main program.

ROM	
0000H	JMP 80DOH
RAM	
3000H	Program variables
30CCH	
30CDH	Program constants
3111H	
ROM	
8000H	Default values for constants
804BH	
804CH	Program data
80CCH	
80DOH	Main Program
8F2FH	

Fig. 11-7: Memory Utilisation

At power on control goes to address 0000H at which may be located the monitor program or an EPROM programmed so as to send control to the start of the main program at address 80D0H (see Fig. 11-7). The latter arrangement makes the system transparent to the user.

11.3 Code Documentation

(Line numbers refer to those on the listing in appendix C).

Main Program (Lines 189 - 271)

The flowchart for the main program is shown in Fig. 11-8.

The program starts at address 80D0H and the first segment copies the default values of user-alterable program constants from ROM, starting at address 8000H, to RAM, starting at address 30DCH. Register B is used as a data counter and 68₁₀ bytes are transferred.

The interrupt mask is set to allow the VECT. INT. key to operate and the interrupt mask is disabled, to be re-enabled at specific points within the program. The stack pointer is then set to 20C2H, and subroutine INIT called to set up the I/O port data direction registers. The byte MODFLG which acts as a mode flag for the previous mode is set to Manual and this completes the initialisation process.

The main control loop starts at label MLOOP and the first operation is to turn off the valves by outputting the appropriate bit patterns to the drivers (Lines 217 - 221). The system then

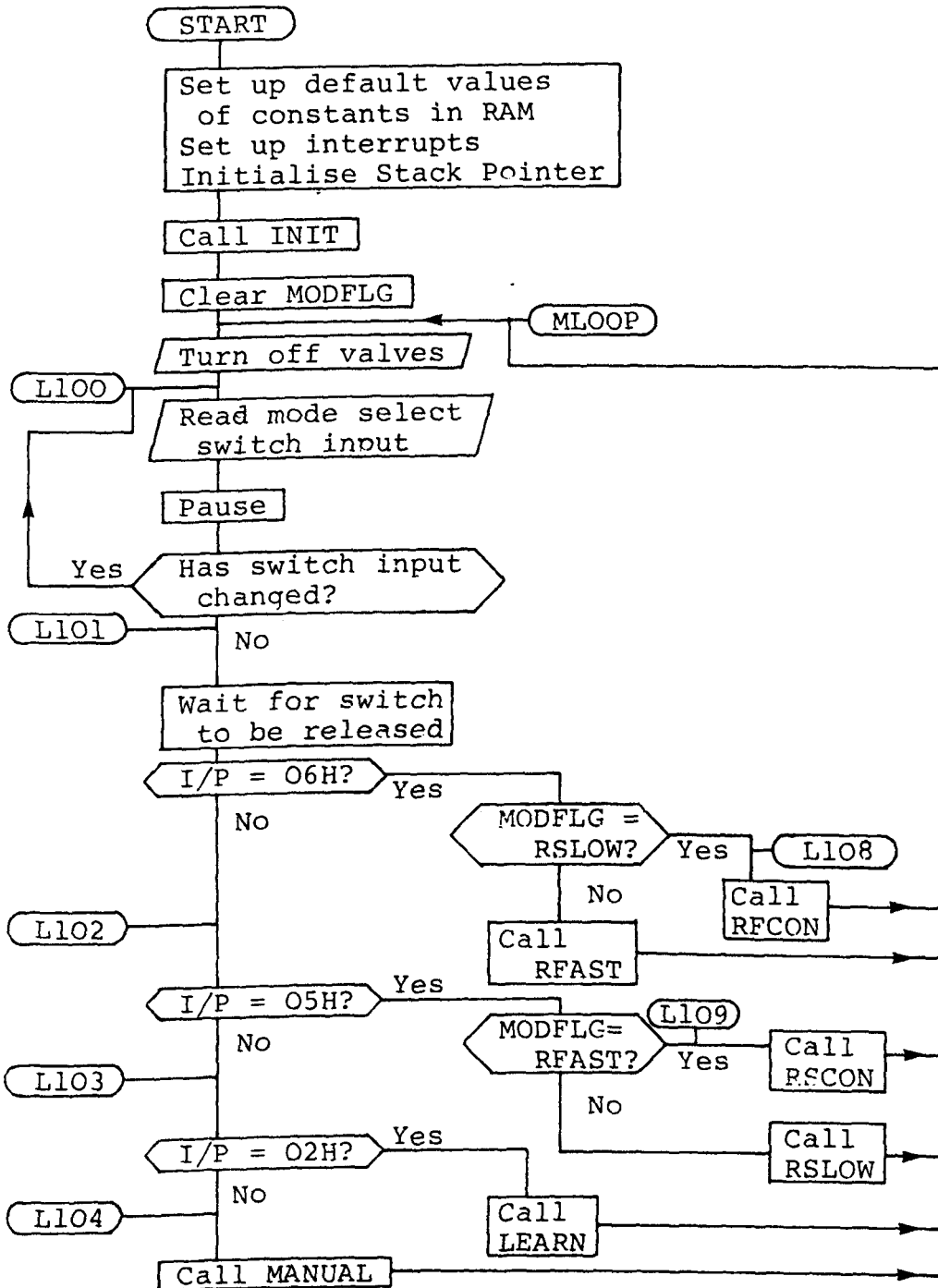


Fig. 11-8: Flowchart for Main Program

reads the status of the mode select switches, MODE, the switch status is debounced by a delay, and the processor waits for the switch to be released. By not proceeding to the selected mode until the switch is released, holding a mode select button down

for an extended period does not give rise to any undesired system response by repeatedly entering and immediately leaving the selected mode. According to the bit pattern input from the mode select switches, the appropriate mode subroutine is called (Lines 242 - 271). If two buttons are depressed simultaneously a priority system is effected. The bit patterns are arranged so that the depression of two buttons simultaneously does not generate the pattern of a third. When control returns from the selected mode it re-enters the mode selection segment.

Subroutine MANUAL (Lines 280-290)

MANUAL is the master subroutine called when Manual mode is selected (see Fig. 11-9). MODFLG is updated and the appropriate mode indicator is set on the control panel (lines 280 - 282). The main loop then begins: subroutine XY is called to implement X-Y control of the machine from joystick inputs, the mode switches are checked and control returns if any of the switches is depressed (lines 284 - 286). An interrupt from the Vectored Interrupt key is allowed and then control jumps to the start of the main loop.

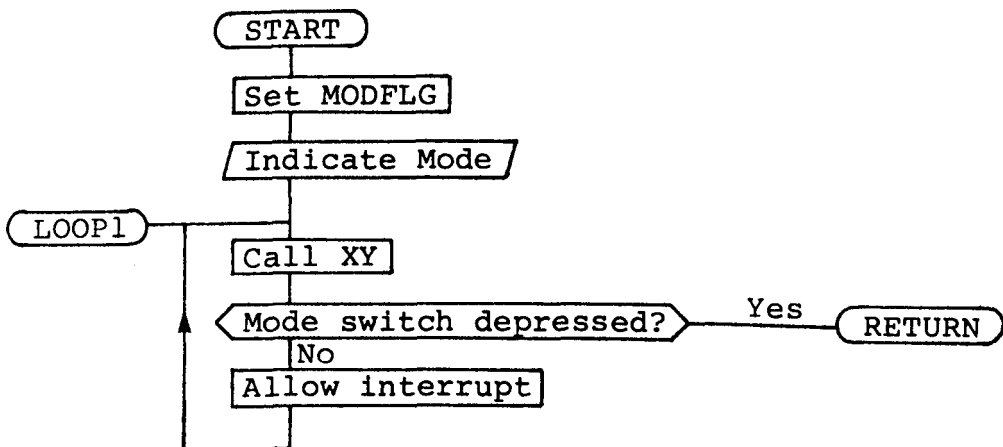


Fig. 11-9: Flowchart for Subroutine MANUAL

Subroutine XY (Lines 303 - 319)

Subroutine XY is the subroutine used in Manual and Learn modes to read the control settings and machine position and assign the valve settings accordingly. It simply calls a sequence of subroutines to effect the different operations (see Fig. 11-10).

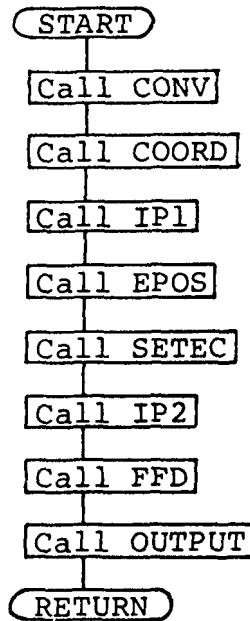


Fig. 11-10: Flowchart for Subroutine XY

Subroutine CONV reads in the joystick positions, pitch control setting, and the position of the machine arms. COORD then calculates the output position in the Cartesian user coordinate system. Subroutine IP1 compares the settings of the joysticks with previous values and if there is significant difference then updates the input velocities to the control system. This has the effect of filtering out any noise due to unsteadiness of the operator's hand. The positional error between the output position and the latest value of the demanded position or Target Point is calculated by subroutine EPOS. A

critical value of position error is set by subroutine SETEC according to the input velocities such that if the system is saturated (i.e. valves fully open) then the target point is frozen.

Subroutine IP2 freezes the target position if the modulus of the positional error, ETA, exceeds ECRIT, otherwise a new position on the demanded trajectory is assigned to the target point. Subroutine FFD assigns the valve openings depending on the angular positional errors at the individual pivots. Subroutine OUTPUT then converts the demanded valve settings to control bytes which are output to the valve drivers.

Subroutine LEARN (Lines 463 - 552)

The first operation performed by the subroutine (Fig. 11-11) is to indicate Learn Mode by outputting the bit pattern 01H to the LED control port at I/O address 23H. PCOUNT which is a counter of the number of points in the stored trajectory is set to zero and the data pointer PPOINT is set to the base address of the path storage area. Subroutine XPXO is called to store the current output position defined by XO, YO, PSIO in the variables XP, YP, PSIP respectively (initialising the so-called Previous Output Position). Subroutine TPUSH pushes the three variables comprising the Previous Output Position onto the stored path stack. This constitutes the first path point and control then enters the main loop at label L206.

The first operation in the main loop is to call subroutine XY which implements the control of the valves. The distance of the

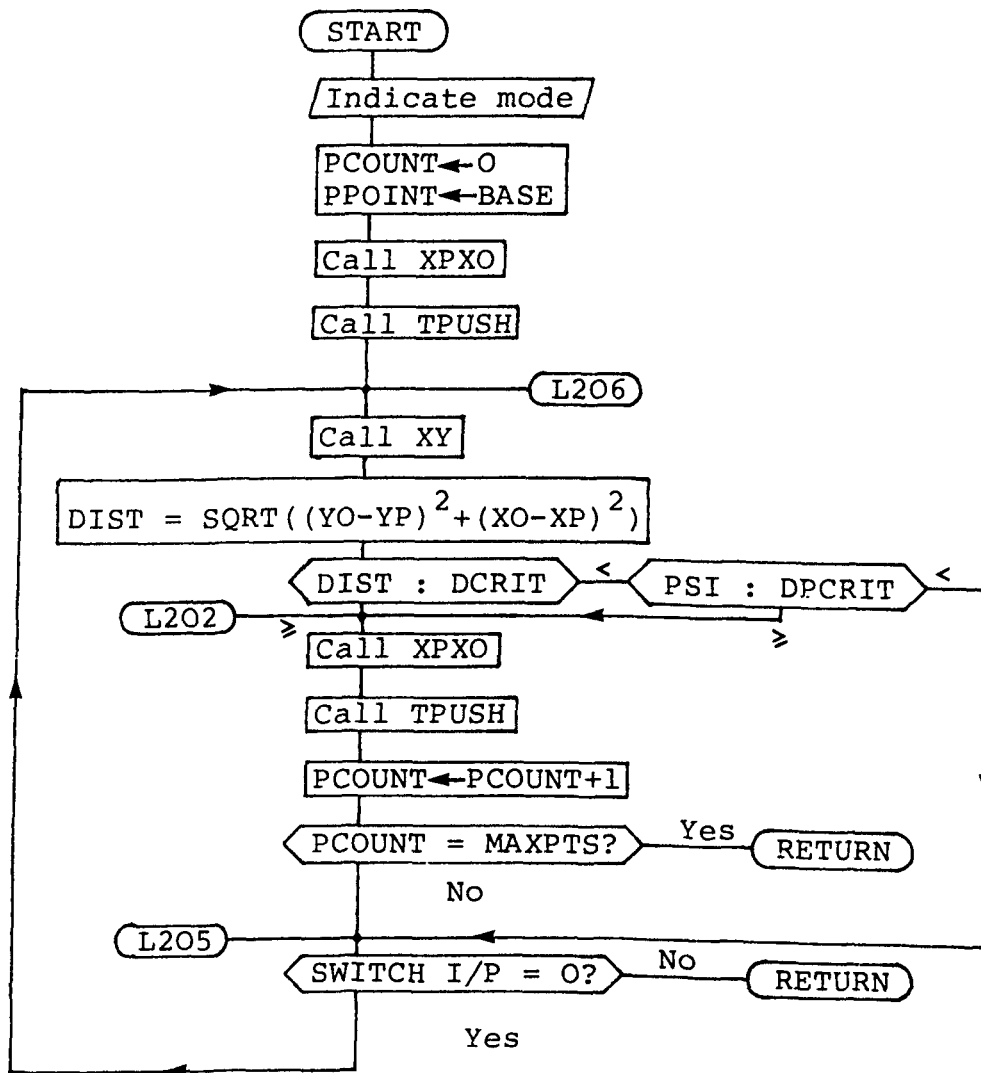


Fig. 11-11: Flowchart for Subroutine LEARN

current XY coordinate from the last stored point XP, YP is calculated and if it exceeds the critical value DCRIT, set at 0.1 m, the new output position is stored on the stack. The bucket angle PSI is also compared with PSIP and if a change greater than DPCRIT, set to 5°, has occurred then also is the new position recorded.

The sequence of operations for recording a path point (Lines 540 - 548) is as follows: subroutine XPXO is called to update

the value of XP, YP, PSIP to the current output values. Subroutine TPUSH pushes the new point onto the path stack. The path point counter PCOUNT is incremented and compared with MAXPTS, the maximum number of points that can be stored, and if the memory is full control returns to the main program.

The final part to the main loop (Lines 541 - 551) is to check that none of the mode select switches is depressed and to jump to the start of the loop or else to return.

Subroutines RFAST and RCON (Lines 729 - 744)

Figure 11-12 shows the flowchart for subroutine RFAST and when subroutine RCON is called control enters at label RCON. Subroutine RFAST is for repeating a stored path i.e. operating the system in repeat fast mode, and is called when changing from manual or learn mode to Repeat Fast mode. When changing from Repeat Slow mode to Repeat Fast mode RCON is called to continue, at a faster rate, a path already being repeated.

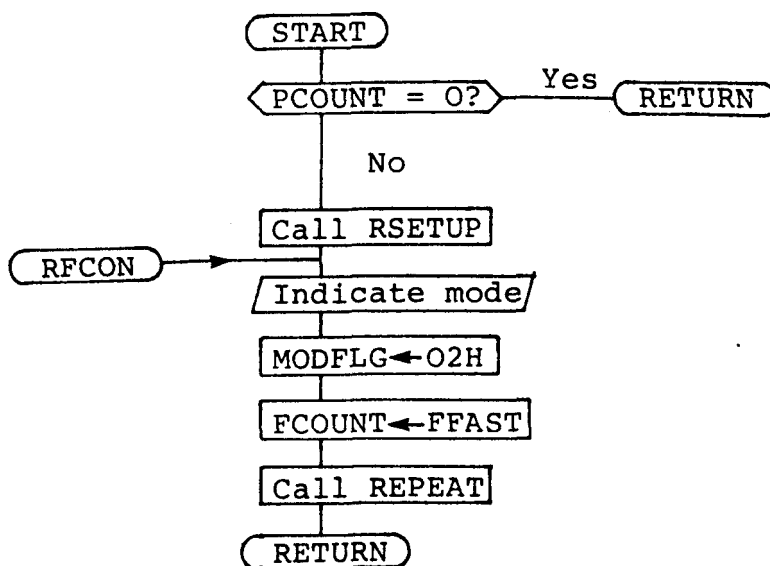


Fig. 11-12: Flowchart for Subroutines RFAST and RCON

The first operation when RFAST is called is to check that there is a path in memory by examining the value of PCOUNT, the counter of the number of points stored. If PCOUNT is zero then control returns to the calling program (lines 729 - 733). Subroutine RSETUP is then called to initialise the data points and the offsets in the X and Y directions to compensate for the new starting point being different from the first stored point.

The Repeat Fast mode indicator LED on the control panel is then turned on and MODFLG byte is set to indicate repeat fast (Lines 735 - 738). To control the speed of execution of the stored path, the rate at which the target points are presented to subroutine XY is varied. The number of calls of subroutine XY in between successive points is stored in FCOUNT and is assigned the value FFAST, here set to 1. NCOUNT, the number of the path point reached is then initialised to zero. Subroutine REPEAT is then called to execute the repeat process using the above defined initial conditions and parameters.

Subroutines RSLOW and RSCON (Lines 762 - 775)

Subroutine RSLOW (see Fig. 11.13) is for operating the system in Repeat Slow mode and if this mode is selected from Repeat Fast mode then control enters at Label RSCON. The routine is similar to RFAST.

The path point counter is checked to determine if there is a path in memory: if it is zero then control returns. Subroutine RSETUP is called to initialise the data pointer and the position offsets to be added to each successive path point to compensate

to the new start point.

The mode indicator LED's are set to indicate RSLOW and MODFLG to the value 01H. PCOUNT is assigned the value of FSLOW (12_{10}) so that a new target point is assigned every 12 calls of routine XY. Subroutine REPEAT is then called to execute the path using the above assigned parameters.

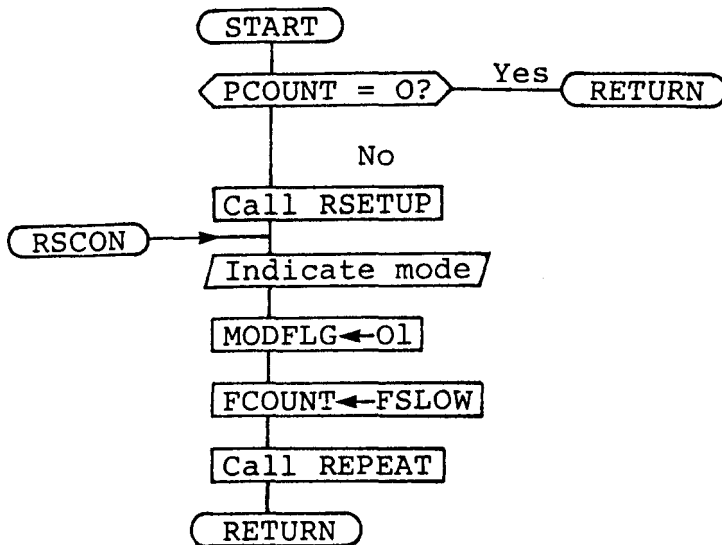


Fig. 11-13: Flowchart for Subroutines RSLOW and RSCON

Subroutine REPEAT (Lines 617 - 713)

This subroutine is called in both Repeat Fast and Repeat Slow modes to pull points from the stored path stack, add the appropriate offset and call the control routines for operating the valves. The subroutine flowchart is shown in Figure 11-14.

The magnitude of the current output error, ETA, is compared with the value ECRIT and if ETA is greater control jumps to the segment for setting the output. This is to ensure that the machine gets close to one target point of the path before inputting the next.

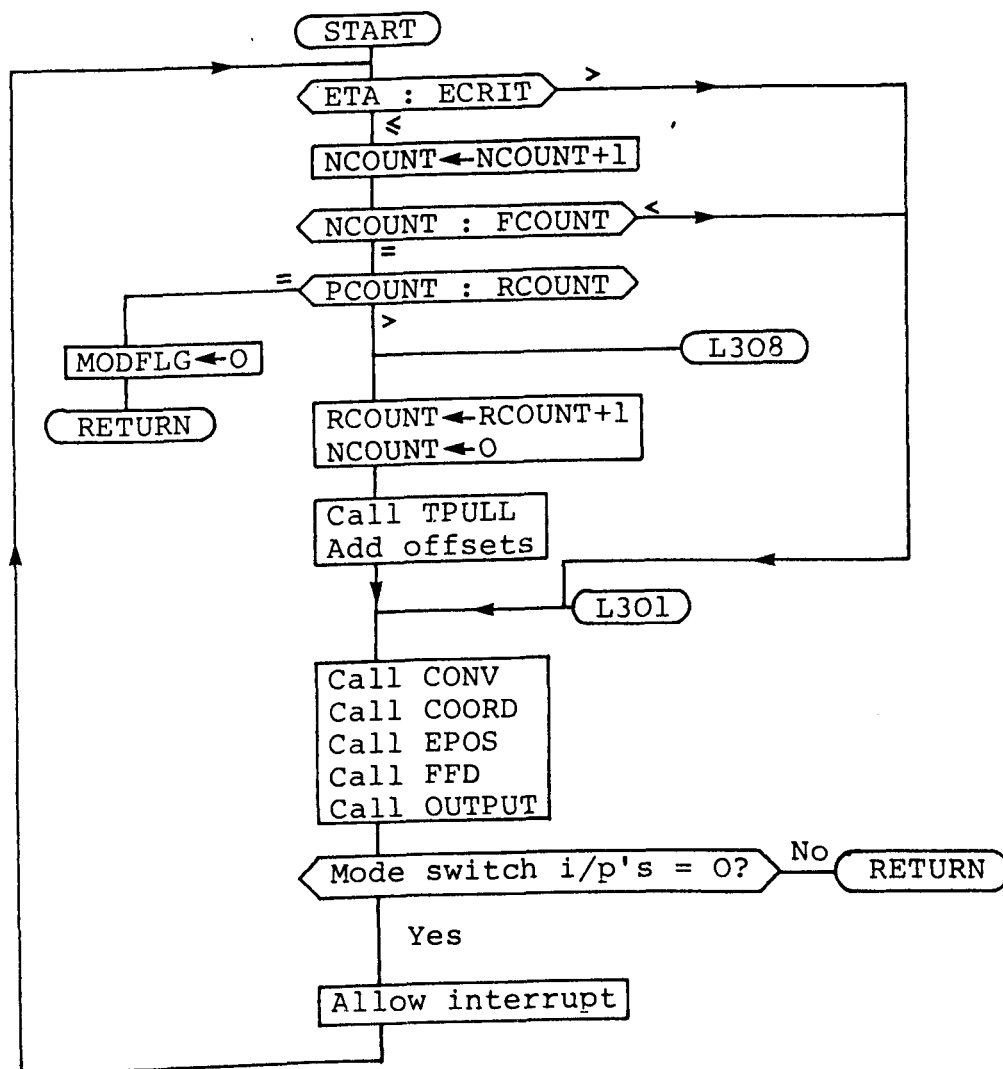


Fig. 11-14: Flowchart for Subroutine REPEAT

NCOUNT, which is a count of the number of calls to the set of position control routines, is incremented and compared with PCOUNT, the value of which determines the frequency at which target points are pulled from the stack. If NCOUNT has not yet reached the value FCOUNT then control moves to L301 to call the position control subroutines.

Otherwise, the path point counter RCOUNT is compared with the total number of points stored, PCOUNT, and if the final

point has been pulled from the stack MODFLG is set to zero and control returns to the calling program. At label L308 path point counter RCOUNT is incremented and NCOUNT reset to zero. Subroutine TPULL is called (Line 678) to pull the top of the path stack and assign the values to XI, YI, and PSII which are the inputs to the position control loop. The X and Y offsets are then added (lines 679 - 698). Starting at label L301 the sequence of position control subroutines is called: CONV inputs the machine position, COORD calculates the output X and Y coordinates, EPOS calculates the positional errors, FFD calculates the required valve settings, and OUTPUT sets the valve control bytes. The mode selection switches are checked and if any is depressed then control returns to the calling program (lines 704 - 706). An interrupt is then allowed from the keyboard so that program execution may be stopped at this point.

Subroutine CONV (Lines 808 - 845)

Subroutine CONV reads all the inputs from the control box and the positions of the arms from the transducers. The flowchart is given below in Fig. 11-15. For operating the analogue to digital converter subroutine ADCON (see Chapter 9) is used. The joystick input voltages are normalised to the range -1 to +1 by subroutine JOYSTK (see Chapter 9). Subroutine SLOPE converts the voltages read by the analogue to digital converter from the pitch control knob to the range $-\pi/2$ to $+\pi/2$. Subroutines ALFIP, BETIP, and DELTIP input angles α , β , and δ respectively.

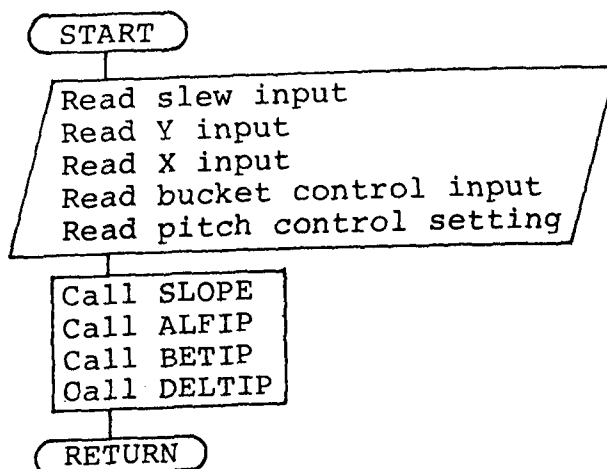


Fig. 11-15: Flowchart for Subroutine CONV

Subroutine COORD (Lines 1209 - 1308)

This subroutine calculates the output coordinates XO , YO , and $PSIO$ from the measured angles α , β , and δ . To increase the speed of calculation a second order polynomial is used to approximate the function $\gamma(\delta)$. In lines 1209 - 1240 XO is calculated, then YO is calculated in lines 1241 - 1274. The polynomial approximation to $\gamma(\delta)$, calculated in lines 1278 - 1294 gives a maximum error of 3% over the range of travel of the bucket, a level of accuracy found to be quite acceptable. The coefficients $GC0$, $GC1$, and $GC2$ were calculated in a separate program to give a least squares approximation to the analytical values of the function $\gamma(\delta)$. $PSII$ is then calculated in lines 1295 - 1307.

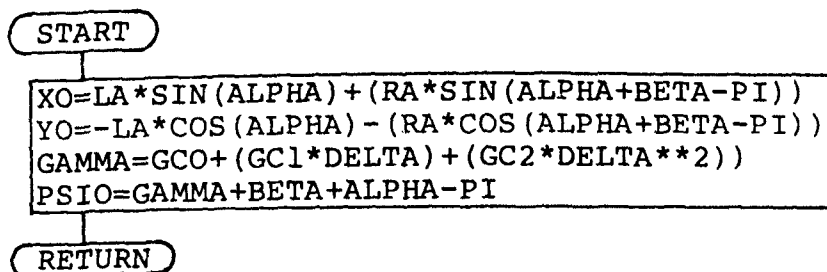


Fig. 11-16: Flowchart for Subroutine COORD

Subroutine IP1 (Lines 1438 - 1584)

This subroutine is called in Manual and Learn modes and is shown flowcharted in Figure 11-17. When bucket movement is selected by the operator the current bucket output angle, PSIO, is assigned to the variable PSII which is then used as the input to the bucket position control loop to keep the bucket angle constant when bucket movement is deselected. This is effected by lines 1438 - 1459.

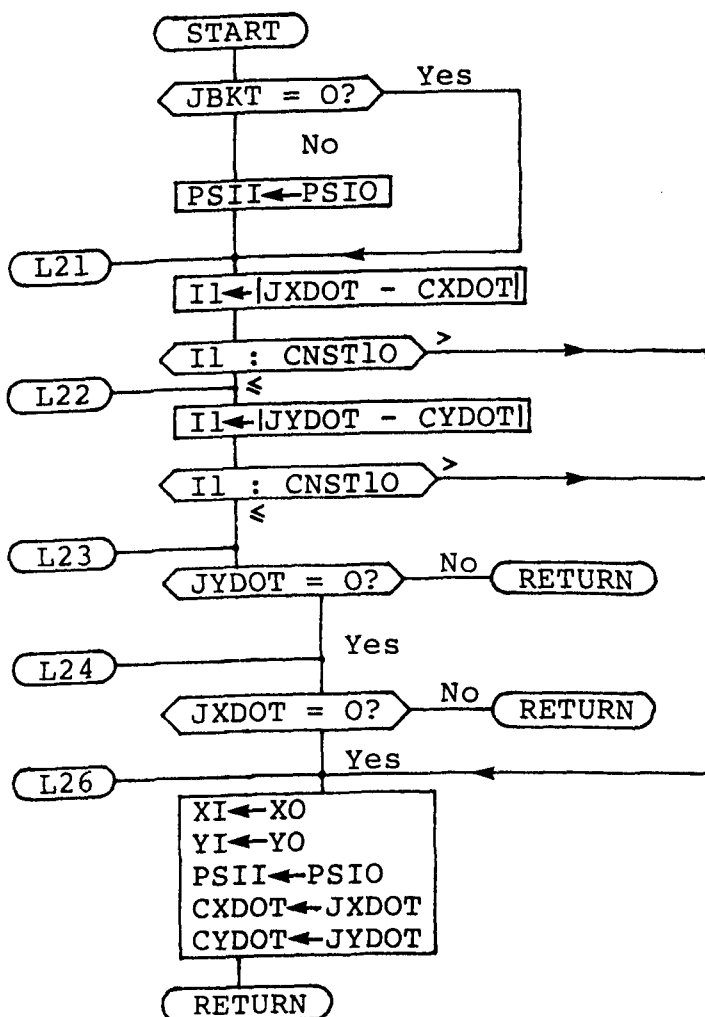


Fig. 11-17: Flowchart for Subroutine IP1

The current X and Y direction joystick input velocities are compared to the current input velocities to the control loop

(lines 1460 - 1519). If there is a significant difference in either ($>CONST10$) then the target point defined by (XI, YI, PSII) is set to the current output position and assigned a new velocity given by JXDOT and JYDOT (Lines 1554 - 1584).

Also if either of the joystick input velocities is set to zero the target point and control loop input velocities are reset (lines 1520 - 1553). This ensures that small changes or noise on the joystick input do not continually reset the target point and that the machine stops abruptly if the joysticks are released.

Subroutine EPOS (Lines 1321 - 1373)

This subroutine, flowcharted in Figure 11-18 calculates the positional errors of the machine in x, y, and ψ (lines 1321 - 1365). As this subroutine is called in all modes an execution timing test segment has been included in it. Byte TFLAG is complemented and output to port 08H so that by monitoring the status of any pin on the port the execution loop time may be measured as half the period of the observed rectangular wave.

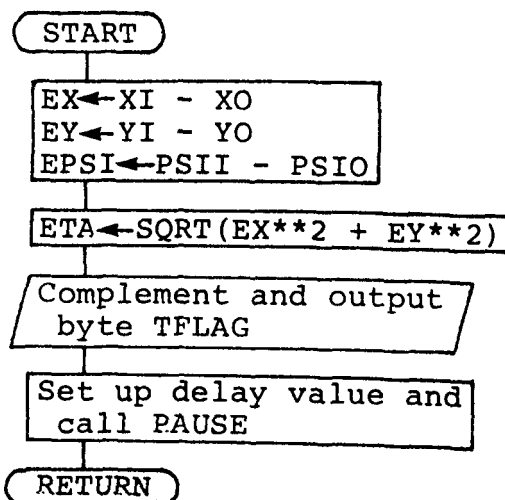


Fig. 11-18: Flowchart for Subroutine EPOS

Also a delay loop is included with a delay which may be set to zero to examine the effects of increased loop execution time. This enables a minimum specification of the hardware and software execution speed necessary for effective control to be achieved.

Subroutine SETEC (Lines 1399 - 1422)

When the position error ETA exceeds a critical value the position of the target point is frozen. Hence if the bucket motion is stalled by an immovable load the target point does not continue moving indefinitely. The maximum allowable error ECRIT is calculated in the routine such that ECRIT has a basic value of EDMIN (set to 0.1 m), increasing with the value of the demanded velocity.

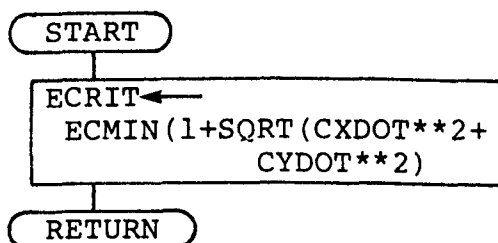


Fig. 11-19: Flowchart for Subroutine SETEC

Subroutine IP2 (Lines 1649 - 1903)

This subroutine (see Figure 11.20) is for updating the target point coordinates in each cycle of the main control loop. If the positional error of the bucket pivot ETA exceeds ECRIT then the target point coordinate is left unchanged. Otherwise the X and

Y input coordinates XI and YI are incremented according to their corresponding input velocities.

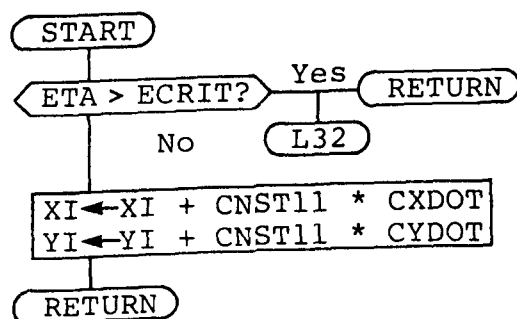


Fig. 11-20: Flowchart for Subroutine IP2

Subroutine FFD (Lines 1649 - 1903)

Subroutine FFD is the code segment which sets the fractional valve openings. The slew valve setting VVSLEW is assigned the value of the slew joystick input JSLEW (Lines 1649 - 1654). MODFLG is then checked to determine if the system is in Manual mode and if not the JXDOT and JYDOT joystick inputs are disregarded (Lines 1656 - 2658). If in manual mode and both joystick inputs are zero then subroutine FREEZE is called to set the lift and reach valve settings to zero (Lines 1661 - 1695). This is to ensure that the machine stops when the joysticks are in their central positions.

If motion of the bucket pivot is not to be frozen then the geometry of the machine is solved to derive the β and α values, BI and AI, required to position the bucket pivot at the target position (lines 1713 - 1774).

The error in α , EALPHA, is calculated and if the error is smaller than the quantisation level of the ADC input then the

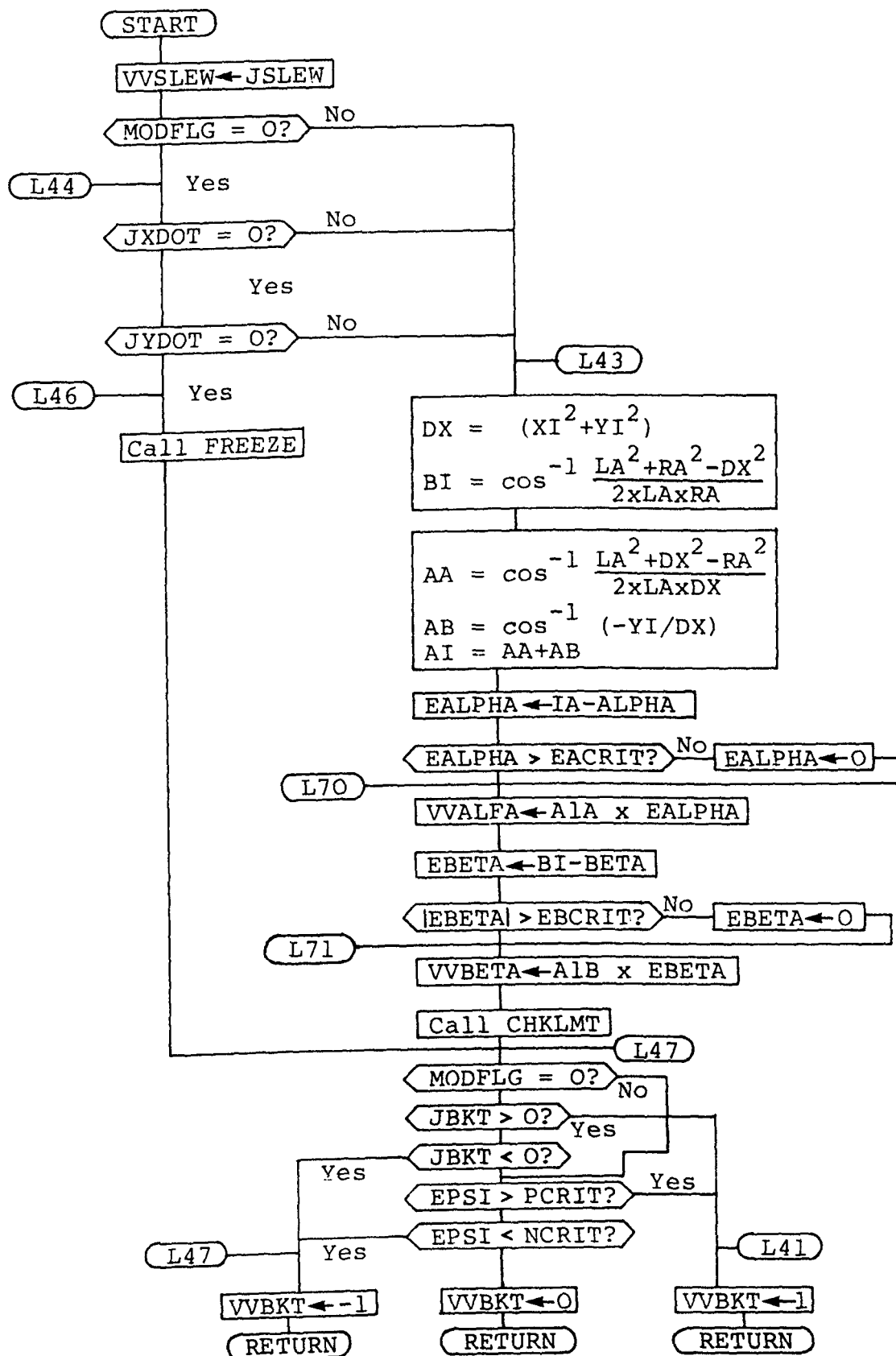


Fig. 11-21: Flowchart for Subroutine FFD

error is assigned the value zero. The value of the valve opening for the alpha valve is then the gain constant $A1A \times EALPHA$. A similar operation is then carried out to set the beta valve opening $VVBETA$ (Lines 1775 - 1810).

Subroutine $CHKLMT$ is called to check if the machine position and the valve setting are such as to try and make a ram move beyond the limit of its travel; if so then subroutine $FREEZE$ is called. The final part of the subroutine (Lines 1812 - 1903) is for determining the required bucket valve opening. If the system is in repeat mode then the joystick input is ignored (Lines 1812 -1814), if manual or learn mode the valve is set according to the joystick (Lines 1818-1849).

If the machine is in repeat mode or the joystick inputs are zero then the bucket valve setting is assigned a value according to the sign and magnitude of the angular positional error $EPSI$ (Lines 1850 - 1903); threshold values $PCRIT$ and $NCRIT$ are set just larger than the quantisation value of the bucket position input.

Subroutine XPXO (Lines 391 - 400)

This subroutine is called in Learn mode to copy the set of output coordinates $XO, Y, PSIO$ (memory locations 3064H thro' 306FH) to $XP, YP, PSIP$ (memory locations 3020H thro' 302BH). Register pair DE acts as the source data pointer and HL as the destination data pointer. Register B acts as the data counter. The routine is flowcharted in Fig. 11-22.

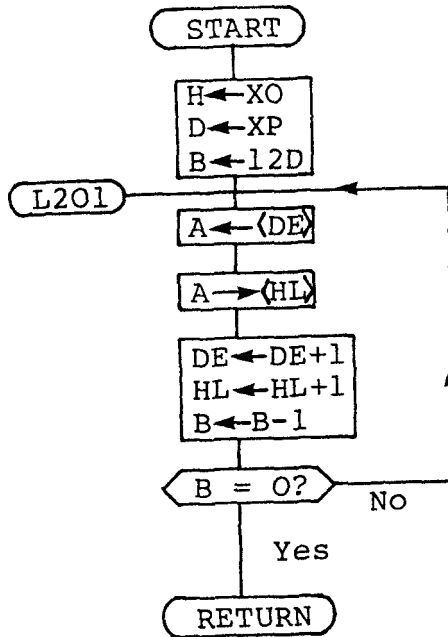


Fig. 11-22: Flowchart for Subroutine XPXO

Subroutine TPULL (Lines 414 - 426)

This subroutine, called in Repeat modes, pulls path coordinates from the stack and puts them in XI, YI, PSII. PPOINT contains the address of the top of the stack and register B acts as a byte counter.

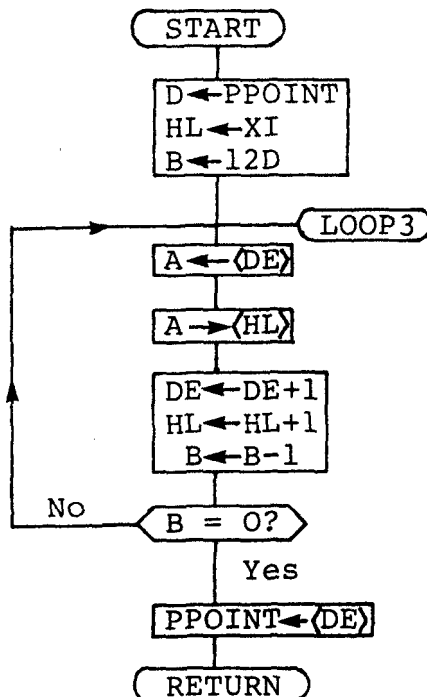


Fig. 11-23: Flowchart for Subroutine TPULL

Subroutine TPUSH (Lines 414 - 426)

This subroutine is used in Learn mode and pushes the output coordinates XO, YO, PSIO onto the path stack. PPOINT is the path stack pointer and the B register is a data counter to the 12 bytes transferred.

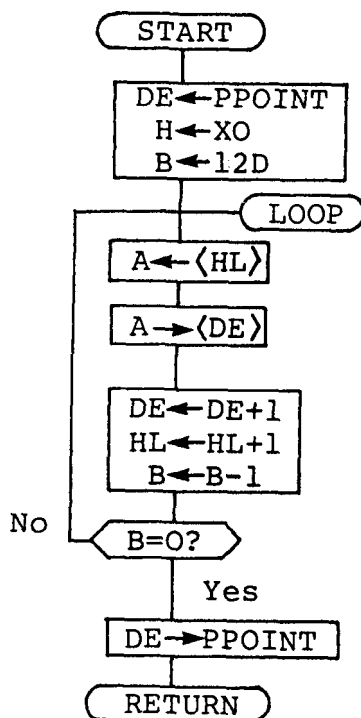


Fig. 11-24: Flowchart for Subroutine TPUSH

Subroutine ALFIP (Lines 855 - 880)

This subroutine (see Fig. 11-25) is for inputting the machine coordinates MCALFA, and ALPHA, the user coordinate lift arm angle, the two being related by the pitch angle selected on the control panel. The appropriate channel of the ADC is read and the result put on the top of the APU stack and converted to 32 bit floating point format. MCALFA is found using the scale factor MA and offset CA.

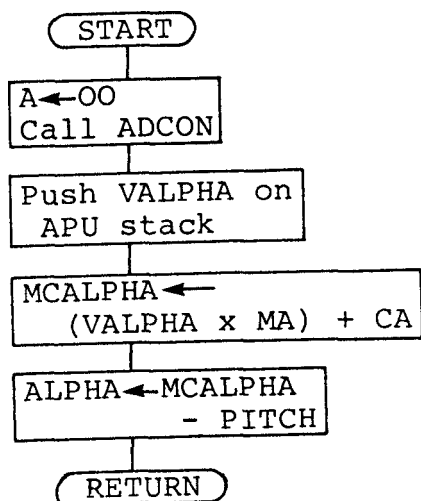


Fig. 11-25: Flowchart for Subroutine ALFIP

Subroutine BETIP (Lines 890 - 907)

Subroutine BETIP (see Fig. 11-26) inputs angle BETA between the reach and lift arms. The appropriate channel of the ADC is read to give VBETA which is then scaled and offset by MB and CB to give BETA.

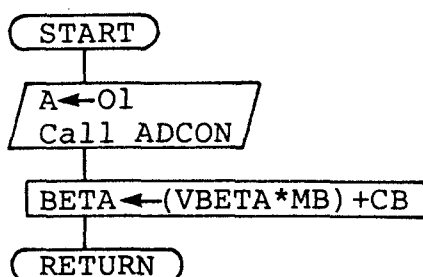


Fig. 11-26: Flowchart for Subroutine BETIP

Subroutine DELTIP (Lines 918 - 935)

Subroutine DELTIP (see Fig. 11-27) inputs the bucket linkage angle DELTA. The appropriate ADC input is read and the result, VDELTA, scaled and offset by MD and CD.

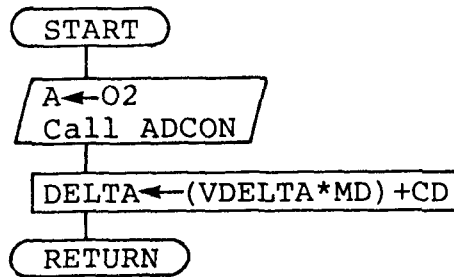


Fig. 11-27: Flowchart for Subroutine DELTIP

Subroutine SLOPE (Lines 1183 - 1198)

This subroutine, flowcharted in Figure 11-28 reads in the pitch angle from the knob on the control panel. The ADC input channel number is in the A register on calling and the result is put into the APU and scaled and offset by CNST13 and CNST14 to give the pitch angle in the range $-\pi/4$ to $+\pi/4$.

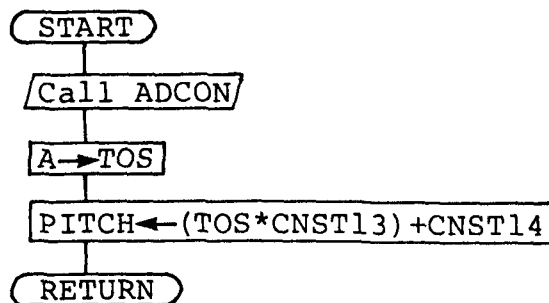


Fig. 11-28: Flowchart for Subroutine SLOPE

Subroutine RSETUP (Lines 569 - 604)

This routine is for setting up the necessary variables before repeating a stored path. NCOUNT, the counter for the number of control routine calls per point, is set to zero as is the repeat path point counter RCOUNT. The data pointer PPOINT is set to the base address of the FIFO path stack. Subroutine TPULL is called to pull the first path point and the X and Y offsets XOF and YOF, to be added to subsequent path points, are calculated.

The inputs to the position control loop are set equal to the outputs and subroutine EPOS is called, setting the positional errors in X and Y to zero.

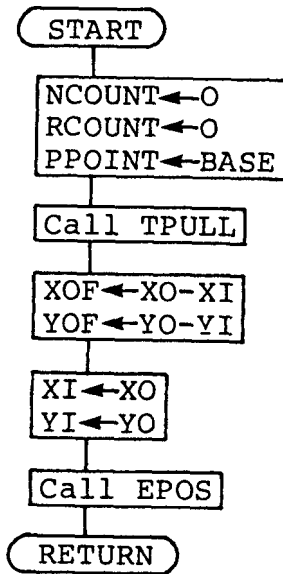


Fig. 11-29: Flowchart for Subroutine RSETUP

Subroutine CHKLMT (lines 1914 - 2048)

Subroutine CHKLMT (see Figure. 11-30) checks the machine position and valve setting to determine if an attempt is being made to move an arm beyond the limit of its travel. If so, subroutine FREEZE is called to set alpha and beta valve openings to zero.

Subroutine FREEZE (Lines 2058 - 2068)

Subroutine FREEZE (see figure 11-31) simply sets the alpha and beta valve openings VVALFA and VVBETA to zero.

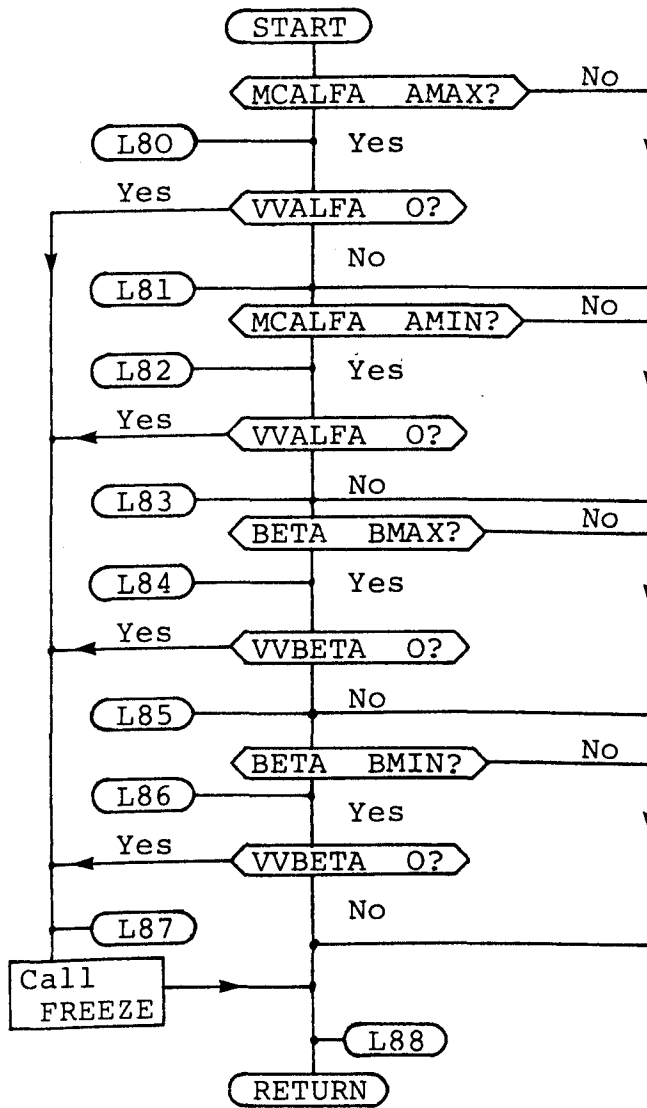


Fig. 11-30: Flowchart for Subroutine CHKLMT

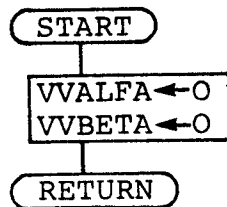


Fig. 11-31: Flowchart for Subroutine FREEZE

CHAPTER TWELVE

FIELDWORK AND SYSTEM EVALUATION

- 12.1 Introduction
- 12.2 Tuning of Control Parameters
- 12.3 Kinematic Evaluation
- 12.4 System Reliability
- 12.5 Functional Evaluation
- 12.6 Learn & Repeat Facility
- 12.7 Estimation of Cost

12.1 Introduction

This chapter deals with the experiments carried out and observations made to assess the technical and functional aspects of the system as built. Also considered are the economic factors influencing the viability of the system as a commercial product.

12.2 Tuning of Control Parameters

Having established the basically correct operation of the software with the digger fixed to the floor in the Mechanical Engineering Laboratories at Liverpool University, the electronic hardware and the transducers were taken to the premises of F.W.McConnel Ltd., Ludlow for adjustment and evaluation when used on a tractor mounted digger.

For experimental work and development, the facility for varying control parameters via the SDK-85 keyboard and monitor was found to be effective and simple to use. It was readily possible in the field to change parameters to determine their effect on system performance.

Valve Offsets

The code was originally written in such a way that different values of offset and maximum valve currents could be stored for each valve so that individually they could be operated over their linear region. In practice however it was found that this was unnecessary and that common values could be used for all valves. By setting the offset current of the valves sufficiently low it was found unnecessary to threshold angular errors in alpha and beta to their quantisation levels as the dead band on

the valves provided an automatic threshold. Also the hysteresis of typically 4 bits, and drift of the valve characteristic of a measured maximum of 16 bits, were overcome in this way.

Gains for Angular Position Control

The values of A1A and A1B were varied to find maximum stable values so that the highest possible speed of response could be obtained without any instability or overshoot. On the reach service the value of 5.1 rad/s/rad was used and on the lift service 2.6 rad/sec/rad (both these figures are equivalent to a fractional valve opening of 10/rad). It was found that values much higher than this gave overshoot, and lower values reduced the speed of movement, and so did not make the best use of available power.

Target Coordinate Increment Factor

Having set the gains for satisfactory control the Target Coordinate Increment Factor (CNST11 in the program code) was adjusted to give the maximum speed range over the full joystick travel. The parameter was set by increasing it until in general, at maximum joystick deflection, no oil would flow through the relief valve. Relief valve flow was detected by monitoring the supply line pressure and could also easily be heard.

12.3 Kinematic Evaluation

A series of experiments were carried out to test the accuracy of the straight line cutting of the bucket blade with the bucket moving in air and also when cutting ground.

The maximum deviation from a straight path when driven against an immovable obstacle was found to be $50 \text{ mm} \pm 5 \text{ mm}$ at the blade and was measured against a straight piece of wood laid alongside the path of the bucket. The angular accuracy of the machine was measured over the range of pitch settings and the mean error was found to be 3° with a maximum error of 6° .

The speed range with a pump flow rate of 0.28 l/s (4.5 g.p.m.) was from 0.14 m/s to a maximum of 0.44 m/s measured over 2 m horizontally in air above ground.

The system positional accuracy was measured by positioning the bucket at various places on its envelope of movement, measuring its position with a steel tape measure, and comparing it with the calculated values of XO and YO as displayed on the monitor display using a data inspection program. The pitch control was set to zero so the X and Y axes were horizontal and vertical respectively. The mean error was found to be 30 mm .

A summary of the kinematic evaluation results is give below:

Correctness of Manual, Learn, and Repeat algorithms
and code

Controllability of machine using single stage valves and
eight bit ADC resolution of position

Sampling frequency 33 Hz

Minimum workable sampling frequency 26 Hz

Maximum deviation from straight path 50 mm

Angular accuracy 3°

Speed range at 1200 r.p.m. engine speed $0.14 - 0.44$

m/s.

12.4 System Reliability

The evaluation phase of the project, carried out on the premises of F.W. McConnel Ltd., was conducted over a period of two months. The system construction was found to be such that very little time had to be spent finding and rectifying hardware faults arising, rather than fine tuning the software and conducting experiments. The problems which did arise however were as follows.

The weight of the transducers and the length of the screws used to secure the transducer bodies to the machine were such that vibration would tend to loosen the screws over a period of time despite the use of shake-proof washers. This is a design fault which could easily be rectified by using larger screws or by moulding the transducer body out of plastic. Vibration again caused a problem in the wiring of the junction box housing the power switching transistors for the solenoid valves when a screw came loose. The use of double nuts, shakeproof washers, or nut locking compound should eliminate the problem. A spring loaded fuse holder on the back of the main rack also gave some trouble with a bad connection due to slight tension in the internal wiring.

The system was used in the field in conditions of frost and drizzle giving no other hardware problems. Use in heavy rain was not possible as a tractor with an enclosed cab was not available for housing the main rack.

12.5 Functional Evaluation

A series of trials was carried out to determine the relative merits of the computerised system against a conventional control system. The evaluation objective was defined to determine the relative work rates and quality of work for both experienced and inexperienced users. A total of six subjects were used in the course of the evaluations, two of whom were expert users of diggers, evaluating systems for F.W. McConnel, Ltd., and three of whom had no experience of using a digger at all, the remaining subject having limited experience.

When the equipment was first constructed the layout of the controls did not conform to that of a standard machine and this made the system totally unacceptable to experienced operators running the system under program DIG. The system was modified and was then found to be quite comfortable and easy to use for extended periods but the lever loads, if anything, were too light to readily discriminate by feel between the two different axes, sometimes causing selection of the wrong service. To avoid any problem of different joystick handling characteristics it was possible to use the same joystick unit for both systems and just change the EPROM in the computer to change from one program to the other.

It was decided to assign simple, well-defined tasks to different users and measure the time taken to perform the tasks and the quality of finish achieved over a range of tasks. All the digging operations were carried out on the premises of F.W. McConnel, Ltd. on a piece of ground of uniform soil composition

and structure to eliminate any effects due to variation in terrain.

XY Control

With two of the novice users it was decided to attempt to reduce the effect of learning on performance evaluation of the two systems by having one subject run the system under program DIG then under MANCON, and the other subject in the reverse order. The actual digging process is a complex combination of vision, physical coordination, and judgement of how the material being dug behaves, as well as audible and visual cues from the machine. In view of this it was thought that whichever system a novice used first it may improve his performance on the second.

The experimental procedure taken was to explain the operation of the machine to the user, making sure that they fully understood the operation of the controls. For safety they were instructed to keep well out of reach of the machine but to stand wherever they wanted for visibility. The task to be performed was then explained and they were advised not to rush but to work steadily and get as good a finish as they reasonably could.

The first task was defined as to dig a rectangular hole the width of the bucket (1 m) and 2 m long and 60 cm deep, estimating the dimensions of the hole from the bucket. Two such holes were dug side by side to provide uniformity of

dimensions, one hole being dug under program DIG and the other under program MANCON, the times being noted for each. Without being given their times the operators were asked which system they would choose to use firstly to perform the task in minimum time, and secondly to perform the task as precisely as possible.

The second task was defined as filling up the original hole and levelling off the surface as flat as possible.

The times taken by the two novice users are given in the following table:

<u>User</u>	<u>Task</u>	<u>Mode</u>	<u>Time (Min.)</u>
A	Dig trench	XY	10
		Conventional	8
	Fill and level	Conventional	7
		XY	10
B	Dig trench	Conventional	22
		XY	22
	Fill and level	XY	20
		Conventional	30

Different users vary dramatically in their ability to learn to control the machine when fitted with conventional mechanical controls. It was not surprising therefore to find a considerable difference between the two novice users in the time taken to perform nominally the same task under program MANCON.

Both operators expressed a marked preference for the machine operating under program DIG i.e. X-Y control.

A timed trial was also carried out with one of the experienced operators in digging a similar trench and the times taken were 9 minutes for the conventional and 14 minutes for the XY control system.

The feature of XY control was found not in general to significantly increase the work rate, in fact the indications are to the contrary. However, for making the final precise cuts necessary for a straight bottom or side to a hole the XY mode was very effective and the operator could trim the pitch control to get exactly the desired angle of cut.

Ditching

The XY facility was found to be of little value for the digging part of the ditch construction but readily gave uniform slopes to the sides of the ditch once the bulk of the earth had been removed.

Trenching

As described above for digging, the cutting of flat bottomed trenches was greatly facilitated for novice users as the exact desired slope could be obtained from a single control lever by setting the pitch to the appropriate angle.

Leveling

Novice users were immediately able to achieve results similar

to those of experienced operators by setting the pitch to the horizontal and using the bottom of the bucket to spread the soil. The degree of coordination required to get a level surface with conventional controls takes a great deal of practice to acquire.

12.6 Learn & Repeat Facility

The Learn and Repeat algorithms and code were tested and operated as designed. One problem which presented itself in repeat mode was that of the bucket encountering an immovable obstacle and stalling i.e. being brought to a halt and with the relief valve blowing. It was found however that if the machine was set then to Manual Mode the bucket could almost invariably be freed by just opening and closing it through a small angle. This operation could be built into the software so that when the machine is stalled automatic corrective action is taken.

For digging and trenching the learn and repeat facility was not found to be particularly useful even allowing for the tendency of the machine to stall. In Repeat Mode the principal difficulty was to start the repeat trajectory at an appropriate point to make the machine do useful work as it has no sensitivity or response to how full or empty the bucket may be. The repeat slow mode was found to be of no value at all.

The learn and repeat facility was evaluated on the cutting of ditches by an experienced operator and by the author. A problem which arose was the large number of piecemeal preliminary cuts to form the basic ditch. A further problem was in estimating where to commence the repeat process. The actual

repeat cutting process itself was accurate and smooth, i.e. kinematically to specification.

12.7 Estimation of Cost

In order to assess any potential commercial viability of a microprocessor based system a specification of the hardware was given to the company Monolog for preliminary costing of a small batch of control units excluding the transducers. The price that they quoted was £1100 pounds per unit and the cost of the basic conventional digger is £3500 retail. Therefore very substantial performance gains have to be demonstrated to justify the extra cost on a functional basis.

The set of three transducers used in the experimental prototype were made by an apprentice and took one month. However, if the bodies and spindle block were cast out of a suitable plastic material or automatically machined, they could be made rapidly for a fraction of the cost.

CHAPTER THIRTEEN

DISCUSSION

- 13.1 Hardware
- 13.2 Software
- 13.3 Safety
- 13.4 Hydraulics
- 13.5 Functional Aspects
- 13.6 Commercial Considerations

13.1 Hardware

The system hardware as constructed was found to meet quite adequately the functional and experimental requirements for evaluation purposes. Inevitably there were some short-comings in the design, a number of which have been mentioned in the hardware chapters and some of a more general nature are discussed below. If the system were to be manufactured there are a number of modifications and additions which would have to be made.

Transducers

The principal fault with the transducers as produced was that of the securing screws working undone with vibration. This can be rectified by lengthening the screws and increasing their diameter. Access to the screws with allen keys was difficult and could be eased by the use of hexagonal headed bolts. Plastic film potentiometers were employed as the sensing elements and they have an extremely long life but if these were subject to wear they could be replaced by inductive potentiometers of appropriate resolution. The 'O' ring seal on the spindle block could also be replaced with a type better suited to rotation.

Computer

In terms of cost, speed, and I/O capabilities the combination of the SDK-85 and AM9511 Arithmetic Processor Unit were ideal, however as costs come down Intel 8086 and 8087 devices may become a viable alternative. The minimum satisfactory sampling frequency was found to be 26 Hz, corresponding to a loop cycle time of 38 ms. Throughout the program there is overkill in

precision of numerical computation which is almost exclusively carried out in 32-bit floating point format. However, even if the word length were halved, it is unlikely that the APU could be replaced with a sequence of software routines for mathematical operations and achieve a sufficiently short loop execution time. Relative times for APU computations and software computations on 32 bit floating point numbers given by AMD are:

	AM9511	Software
	(Times in microseconds)	
Multiply	200	7,000
SQRT	400	77,000
Sin(x)	2,000	118,000

Thus for a 32-bit word length, a single software square root takes over double the required minimum loop execution time. It is unlikely therefore that the software could be written to run effectively on a single 8-bit processor. Sine and cosine calculations could be done at high speed with a look-up table to eight bit accuracy but there are still over 70 basic arithmetic operations to be carried out in the main loop in manual mode.

I/O Capability

The keyboard and display are only necessary for developmental purposes and could be dispensed with on a commercial machine. Additional valve control circuitry should be used to replace the bang-bang valve on the bucket with a proportional valve. The bang-bang valve used at present gives rise to sharp pressure transients in the supply. For use on a

machine with changeable geometry a set of rotary thumbwheel switches are required to input data on the machine configuration being employed. The number of analogue input channels should be increased by one to allow the slew function to be incorporated in the Learn and Repeat facility and a certain amount of memory expansion to contain the additional slew position data would be required.

Controls

Better waterproofing of the mode selector switches could be achieved by using customised tactile pressure switches which are cheap and reliable. The joystick axis directional sense could also be improved by stronger springing to prevent accidental selection of the wrong service.

Circuitry

For a commercial machine the circuitry should be constructed on printed circuit boards and ideally built in a modular form so that whole assemblies may be replaced if a fault arises in the field. Self-diagnostics would be useful for this purpose provided that they did not add significantly to the cost. The packaging of the rack and control panel should also be made watertight. Waterproof connectors to the rack should also be used despite their price as they do provide weather-proofing.

13.2 Software

Very considerable simplifications could be made to the existing software to shorten it. The emphasis is the way it was written in the project has been on readability and convenience of coding

by extensive use of the APU. Also the data structure is such that program constants may be varied which is not necessary as optimal values are now obtained. A commercial system should have the control of the slew service incorporated into the learn and repeat facility which was omitted in the present system because there was not enough room to test this function in the laboratory. Also, different configurations of the machine, requiring different program constants, should be accommodated in any commercial system.

13.3 Safety

To be completely safe from any contact with the moving arms or the bucket the operator should at all times stand behind the machine, out of reach. However with a portable control panel the operator may walk forward to improve his visibility of the bucket. The potential dangers of slipping on wet ground and falling in the path of the bucket or in the hole being dug are lethal. The dangers may be reduced by the use of an emergency stop button on the front of the control panel as included on the circuit built and the use of a mercury switch internally to disable the power supply if the box should be tilted as the operator falls or drops it.

Besides the danger of the operator straying or falling into the path of the machine there is the danger of a circuit malfunction causing some erratic or unexpected behaviour of the machine thereby also endangering the operator or any other person within range.

The Health and Safety Executive recommendations on operating procedures for microprocessor controlled manipulators³⁴ state that safety should be ensured by either ensuring the operator cannot come within the range of the machine or that a working procedure be adopted which guarantees against any dangers from machine malfunction. In an agricultural environment the only way to ensure this is to have the control panel mounted in the tractor cab or on the machine itself.

13.4 Hydraulics

The question may be asked as to whether the machine work rate may not be increased by raising the supply pressure and hence the system speed and cutting force. There is however a limit to the acceleration which can be tolerated without material spilling from the bucket and also, particularly in the case of the slewing service, the angular momentum which is imparted to the machine may cause overshoot under manual control.

The IWT and tilt functions necessary for the later model of machine should be incorporated into the electronic design so that all function may be operated from one control panel. Also a proportional valve for operating the bucket would improve the smoothness of response of the system by eliminating the sharp pressure transients imposed on the supply by the opening and closing of the bang-bang valve.

13.5 Functional Aspects

The trials carried out demonstrate that there is no consistent significant increase in work rate for new users. Despite the

effective rationalisation of the lever functions to bucket blade movements so that linear cuts may readily be obtained the overall digging process was not facilitated.

Part of the reason for this may lie in the fact that the movement produced by the deflection of a particular lever is not obvious from the geometry of the machine. On the conventional control system the effect of each control axis is to operate a particular ram so by viewing the geometry of the machine it is clear which rams need to be activated to move the bucket in particular directions. With the XY control system a single joystick axis in conjunction with the pitch control will give any straight cut but the path has to be visualised and is not determined from the machine geometry.

In the levelling process however, and in cutting smooth planes, the XY control is extremely effective. To get a planar cut with conventional controls it is necessary to continuously vary the bucket, lift, and reach valve openings as against operating one lever with appropriate pitch setting.

Another problem for the novice user is that of selecting the appropriate joystick axis for the movement required: this still has to be learned even though the number of simultaneous selections is reduced.

The lack of workrate increase for experienced operators must be attributed to their optimal use of conventional control so that maximum power is used from the machine in all operation and no

wrong service selections are made. Having to unlearn the ingrained experience of conventional machine use may detract from their performance in the XY system.

More detailed trials on a larger number of subjects would yield more insight into the different factors of the complex man-machine interaction such as error rates and learning effects. However conditions and time constraints did not allow for more numerous and detailed investigations.

13.6 Commercial Considerations

To evaluate the microprocessor based system as a potential product it is necessary to weigh up the various pros and cons comparing it with the conventional mechanical system which is tried and tested. The functional advantages include the improved accuracy and control for novice users, the facility for cutting at defined inclinations, ease of installation in the cab, and reduced lever loads giving less fatigue. It also has a definite technological gimmick value for those susceptible to such things! The novice users preferred it both for speed and precision even though for speed there was no gain.

However, cost, reliability, based on the number of parts to fail, and also possible servicing, count heavily against the system. The technological and manpower investment necessary to launch commercially into the development and support of such a high technology device could only be justified on the grounds of very significant functional advantages, far greater than the marginal benefits shown by the experimental system produced in

this project. In addition there may be a certain amount of technological resistance, which would have to be assessed, from those having to start dealing in a new technology be it from salesmen, dealers, or customers.

The mechanical control systems currently employed have evolved over a period of years to a high degree of reliability. Commercial experience with functionally relatively simple electric valve controllers for hedge cutters working bang-bang valves has shown that exceedingly high standards of design and manufacture are necessary to make the product a success. With a functionally much more complex system the task can be no easier.

The case for the commercial development of the simpler electronic controller described in its basic form in Chapter 3 is much stronger however, as the system is much simpler electronically and offers the advantages of ease of installation and light lever loads. Ease of installation is important as the digger may frequently be attached to and detached from the tractor, and mechanical cables can be difficult to accommodate and to feed into the cab; they also impose higher lever loads on the operator than levers mounted on the valve block.

CHAPTER FOURTEEN

CONCLUSIONS & FURTHER WORK

- 14.1 Conclusions
- 14.2 Further Work

14.1 Conclusions

The work carried out shows that the solenoid operated proportional valves can be effectively used for both manual open loop control of the machine and computer closed loop control. The open loop controller is functionally advantageous over the conventional mechanical control system with cables for in-cab operation. It is both easier to install and reduces the lever loads resulting from spool return springs and the connecting cables, which can become tiring.

The algorithm developed for control of the machine effectively converts the control functions from individual rams to those of velocity control in a Cartesian framework with an accuracy sufficient for all digging operations. The pitch control allows control of the angle of cut to an accuracy of $\pm 3^\circ$. The learn and repeat software functioned as designed allowing any profile once taught to the machine to be repeated from any new starting point at any angle selected on the pitch control.

The computer hardware and the transducers functioned reliably and as designed. With a few modifications given in the Discussion the hardware could be put into production if desired. The work demonstrates the technical feasibility of producing a closed loop microprocessor based control system at a cost commensurate with that of the machine.

Evaluation trials, carried out with both experienced and inexperienced digger operators, however showed that there was no consistent significant increase of work rate using the

computer control system in either its manual or learn and repeat modes of operation. The operations of making straight cuts and levelling were facilitated for both classes of user and novice operators were able to achieve results otherwise impossible without extensive practice.

In the light of these results it may be said that the benefits to the operator are not such as to justify development of the existing prototype computerised system for commercial production. However, the open loop electronic controller, provided a sufficiently reliable and robust design and construction are employed, is a far more viable product.

14.2 Further Work

It has been shown that the automation of the cutting of straight lines does not effectively increase work throughput, a necessary condition for a viable product. The decision making stage in lever selection is not eliminated. However this does suggest that a telechiric type of system with the control handle mounted on a miniature linkage similar to that of the digger may prove more successful. If the manually imposed troques at the pivots of the control linkage are sensed and used to operate the corresponding valves, while at the same time the position of the control inkage is sevoed by say d.c. motors to correspond to that of the machine then a sense of feel would also result. The digger would automatically mimic the movements of the control handle and the operator would not have to consciously control individual rams.

Tractor mounted hedge cutters are limited in their speed of operation by the rate at which the operator can adjust the inclination of the head to the hedge and tractor position. It may be possible to apply a control regime, as here developed for a digger, to obtain independent control of up-and-down and in-and-out movement from two levers. The hardware built for the digger could readily be re-programmed to operate a hedge cutter if appropriate transducers were fitted and either using a similar control regime or resolved rate motion.

If successful, simplification could then be made to the mechanical construction of the machine offsetting the cost of the electronics and transducers. Automation of control of the cutter to compensate for varying tractor-hedge distance as well as variations in tractor inclination would be extremely complex and expensive. The principal problem is to find a suitable reference line in the hedge being cut from which the cutter can be positioned. A further possibility would be to employ a telechiric system for hedge cutter control.

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APPENDIX A

PROGRAM MANCON

LOC	OBJ	LINE	SOURCE STATEMENT
		1	%MOD85 MACROFILE
3000		2	ORG 3000H
		3	
		4	
		5	
		6	
		7	
		8	
		9	
		10	
		11	
		12	
		13	
		14	
		15	
		16	
3000		17	JXDOT: DS 4
3004		18	JYDOT: DS 4
3008		19	JSLEW: DS 4
300C		20	JBKT: DS 4
3010		21	I1: DS 4
3014		22	I2: DS 4
3018		23	STATUS: DS 1
3019		24	S: DS 4
301D		25	V1: DS 4
3021		26	V2: DS 4
3025		27	VVSLEW: DS 4
3029		28	VVALFA: DS 4
302D		29	VVBETA: DS 4
3031		30	VVBKT: DS 4
3035		31	VS: DS 1
3036		32	VL: DS 1
3037		33	VR: DS 1
3038		34	VB: DS 1
3039		35	FVO: DS 4
		36	
303D		37	ASTR: DS 1
303E		38	OFFSET: DS 1
303F		39	MAX: DS 1
3040		40	POF: DS 1
3041		41	NOF: DS 1
3042		42	PMAX: DS 1
3043		43	NMAX: DS 1
3044		44	APOF: DS 1
3045		45	APMAX: DS 1
3046		46	ANOF: DS 1
3047		47	ANMAX: DS 1
3048		48	BPOF: DS 1
3049		49	BPMAX: DS 1
304A		50	BNOF: DS 1
304B		51	BNMAX: DS 1
304C		52	SPOF: DS 1
304D		53	SPMAX: DS 1
304E		54	SNOF: DS 1


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UNIVERSITY OF LIVERPOOL
DEPARTMENT OF ELECTRICAL ENGINEERING
AND ELECTRONICS
E.R.I. DEANE
THIS IS AN ASSEMBLY LANGUAGE PROGRAM
FOR MANUAL CONTROL OF A PA6 DIGGER
CODE EDITED 1530 4TH JANUARY 1983
DISK: NO. 4 VERSION 2.6
** RAM LOCATIONS FOR PROGRAM VARIABLES **
JOYSTICK INPUT XDOT IN USER CO-ORDS
      "      " YDOT "      "
      "      " SLEW RATE
      "      " BUCKET MOVEMENT
INTERMEDIATE RESULT LOCATION
INTERMEDIATE RESULT LOCATION
STATUS OF APU
INTERMEDIATE RESULT LOCATION
LOCATION FOR IFF DATA TRANSFER
LOCATION FOR IFF DATA TRANSFER
SLEW VALVE SETTING (32 BIT FORMAT)
ALPHA VALVE "      "
BETA VALVE "      "
BUCKET VALVE "      "
SLEW VALVE SETTING (8 BIT FORMAT)
LIFT "      "
REACH "      "
BUCKET "      "
FRACTIONAL VALVE OPENING USED AS
A PARAMTER FOR SUBROUTINE VLIN
STORAGE LOCATION FOR A REGISTER
WORKSPACE FOR SUBROUTINE VLIN
      "      "
      "      "
      "      "
      "      "
ALPHA +VE OFFSET
ALPHA +VE SATN. O/P
ALPHA -VE OFFSET
ALPHA -VE SATN. O/P
BETA +VE OFFSET
BETA +VE SATN. O/P
BETA -VE OFFSET
BETA -VE SATN. O/P
SLEW +VE OFFSET
SLEW +VE SATN. O/P
SLEW -VE OFFSET
    
```

LOC	OBJ	LINE	SOURCE STATEMENT	
304F		55	SNMAX: DS 1	{SLEW -VE SATN. O/P
		56		{
8000		57	ORG 8000H	{** EPROM LOCATIONS CONTAINING
		58		{ PROGRAM DATA **
		59		{
		60		{DEFAULT VALUES FOR VALVE OFFSETS
8000	C0	61	XAPDF: DB 0C0H	
8001	FF	62	XAPMAX: DB 0FFH	
8002	40	63	XANOF: DB 40H	
8003	7F	64	XANMAX: DB 7FH	
8004	40	65	XBPDF: DB 40H	
8005	7F	66	XBPMAX: DB 7FH	
8006	C0	67	XBNOF: DB 0C0H	
8007	FF	68	XBNMAX: DB 0FFH	
8008	C0	69	XSPDF: DB 0C0H	
8009	FF	70	XSPMAX: DB 0FFH	
800A	40	71	XSNDF: DB 40H	
800B	7F	72	XSNMAX: DB 7FH	
		73		{PROGRAM CONSTANTS
800C	00	74	TEN: DB 00H,00H,0A0H,04H	{10D
800D	00			
800E	A0			
800F	04			
8010	00	75	TWO: DB 00H,00H,80H,02H	{2D
8011	00			
8012	80			
8013	02			
8014	00	76	H87: DB 00H,00H,87H,08H	{87H = 135D
8015	00			
8016	87			
8017	08			
8018	00	77	H79: DB 00H,00H,0F2H,07H	{79H = 121D
8019	00			
801A	F2			
801B	07			
801C	00	78	ZERD: DB 00H,00H,00H,00H	{0D
801D	00			
801E	00			
801F	00			
8020	00	79	ONE: DB 00H,00H,80H,01H	{1D
8021	00			
8022	80			
8023	01			
8024	FE	80	HALF: DB 0FEH,0FFH,0FFH,7FH	{0.5D
8025	FF			
8026	FF			
8027	7F			
8028	00	81	MINONE: DB 00H,00H,80H,81H	{-1D
8029	00			
802A	80			
802B	81			
802C	00	82	D14: DB 00H,00H,0E0H,04H	{14D
802D	00			
802E	E0			
802F	04			

LOC	OBJ	LINE	SOURCE STATEMENT	
8030	00	83	CNST20: DB 00H,00H,0F0H,06H	{3CH=60D
8031	00			
8032	F0			
8033	06			
8034	00	84	CNST21: DB 00H,00H,98H,07H	{4CH=76D
8035	00			
8036	98			
8037	07			
8038	00	85	H255: DB 00H,00H,0FFH,08H	{FFH=255D
8039	00			
803A	FF			
803B	09			
80D0		86		{
		87	ORG 80D0H	{** MAIN PROGRAM **
		88		{
		89		{APU STACK PUSH MACRO
		90	PSH MACRO XYZ	
-		91	LXI D,XYZ	
-		92	CALL PSHT	
		93	ENDM	
		94		{APU STACK POP MACRO
		95	PLL MACRO PQR	
-		96	LXI D,PQR	
-		97	CALL PLLT	
		98	ENDM	
		99		{
80D0	060C	100	MVI B,0CH	{SET UP DEFAULT VALVE CONSTANTS
80D2	110080	101	LXI D,XAPDF	
80D5	214430	102	LXI H,APDF	
80D8	1A	103	DLOOP: LDAX D	{LOOP TO COPY DEFAULT OFFSET
80D9	77	104	MOV M,A	{ VALUES FROM ROM TO RAM
80DA	13	105	INX D	
80DB	23	106	INX H	
80DC	05	107	DCR B	
80DD	C2D880	108	JNZ DLOOP	
		109		{
80E0	3EF8	110	MVI A,0FH	{UNMASK AND DISABLE INTERRUPTS
80E2	30	111	SIM	
80E3	F3	112	DI	
		113		{
80E4	31C220	114	LXI SP,20C2H	{SET STACK POINTER
		115		{
80E7	CD2B81	116	CALL INIT	{INITIALISE SYSTEM
		117		{
80EA	3ECF	118	MVI A,0CFH	{SET UP VECTORED INTERRUPT RESET
80EC	32CE20	119	STA 20CEH	{ INSTRUCTION BY LOADING LOCATION
		120		{ 20CEH WITH 0CFH
		121		{
		122		{** MAIN CONTROL LOOP **
		123		{
80EF	CD3A81	124	LOOP: CALL CONV	{SUBROUTINE CONV READS IN CONTROL
		125		{ SETTINGS JXDOT, JYDOT, JBKT
		126		{ AND JSLEW
		127		{
		128	PSH JXDOT	{ASSIGN TO EACH VALVE SETTING THE

LOC	OBJ	LINE	SOURCE	STATEMENT
80F2	110030	129+	LXI	D,JXDOT
80F3	CD9481	130+	CALL	PSHT
		131	PLL	VVBETA
80F8	112D30	132+	LXI	D,VVBETA
80FB	CDAE81	133+	CALL	PLLT
		134	PSH	JYDOT
80FE	110430	135+	LXI	D,JYDOT
8101	CD9481	136+	CALL	PSHT
		137	PLL	VVALFA
8104	112930	138+	LXI	D,VVALFA
8107	CDAE81	139+	CALL	PLLT
		140	PSH	JBKT
810A	110C30	141+	LXI	D,JBKT
810D	CD9481	142+	CALL	PSHT
		143	PLL	VVBKT
8110	113130	144+	LXI	D,VVBKT
8113	CDAE81	145+	CALL	PLLT
		146	PSH	JSLEW
8116	110830	147+	LXI	D,JSLEW
8119	CD9481	148+	CALL	PSHT
		149	PLL	VVSLEW
811C	112530	150+	LXI	D,VVSLEW
811F	CDAE81	151+	CALL	PLLT
		152		
8122	CDB782	153	CALL	OUTPUT
		154		
		155		
8125	FB	156	EI	
8126	00	157	NOP	
8127	F3	158	DI	
		159		
8128	C3EF80	160	JMP	LOOP
		161		
		162		
		163		
		164		
		165		
		166		
		167		
		168		
		169		
		170		
		171		
		172		
		173		
		174		
		175		
		176		
		177		
		178		
		179		
		180		
		181	IFF	MACRO ID1,OP,ID2,LABL
-		182	PSH	ID1
-		183	PLL	V1

{ CORRESPONDING JOYSTICK DEFLECTION

{
 {OUTPUT DATA TO VALVE CONTROL
 { INTERFACE
 {
 {ALLOW INTERRUPT FROM KEYBOARD

{
 {** MACRO FOR CONDITIONAL JUMPS **
 {
 { THIS MACRO GENERATES CODE FOR MAKING
 {CONDITIONAL JUMPS DEPENDING ON THE VALUES
 {OF TWO FLOATING POINT VARIABLES ID1 AND ID2
 {
 {IF ID1 GTHAN:GEQUAL:EQUALS:NEQUAL:LEQUAL:LTHAN ID2
 { THEN GOTO LABL
 { ELSE CONTINUE
 {
 {REGISTERS AFFECTED: A,D,E,STATUS
 {
 { DATA IS PASSED TO SUBROUTINE OP IN TEMPORARY
 { VARIABLES V1 AND V2. THE RESULT IS RETURNED
 { IN THE ACC.} 1=TRUE, 0=FALSE. THE RESULT OF
 { OP IS CHECKED AND CONTROL JUMPS OR CONTINUES
 { ACCORDINGLY.
 {

LOC	OBJ	LINE	SOURCE STATEMENT
-		184	PSH ID2
-		185	PLL V2
-		186	CALL OP
-		187	ANI 01H
-		188	JNZ LABL
		189	ENDM
		190	
		191	
		192	
		193	
		194	
		195	
		196	*** SUBROUTINE INIT **
		197	
		198	! SETS UP I/O PORT DATA DIRECTION
		199	! REGISTERS
		200	
		201	!REGISTERS AFFECTED: A
		202	
812B	3E0F	203	INIT: MVI A,0FH
812D	D320	204	OUT 20H
812F	3EFF	205	MVI A,0FFH
8131	D302	206	OUT 02H
8133	D303	207	OUT 03H
8135	3E0C	208	MVI A,0CH
8137	D328	209	OUT 28H
8139	C9	210	RET
		211	
		212	*** SUBROUTINE CONV **
		213	
		214	! READS IN CONTROL JOYSTICK SETTINGS:
		215	!JSLEW, JYDOT, JXDOT, JBKT
		216	
		217	!REGISTERS AFFECTED: A,D,E,H,L,STATUS
		218	
813A	3E05	219	CONV: MVI A,05H
		220	
813C	CD7381	221	CALL ADCON
813F	CD2E82	222	CALL JOYSTK
		223	
		224	
		225	PLL JSLEW
8142	110830	226+	LXI D,JSLEW
8145	CDAE81	227+	CALL PLLT
8148	3E04	228	MVI A,04H
814A	CD7381	229	CALL ADCON
814D	CD2E82	230	CALL JOYSTK
		231	PLL JYDOT
8150	110430	232+	LXI D,JYDOT
8153	CDAE81	233+	CALL PLLT
8156	3E05	234	MVI A,05H
8158	CD7381	235	CALL ADCON
815B	CD2E82	236	CALL JOYSTK
		237	PLL JXDOT
815E	110030	238+	LXI D,JXDOT

LOC	OBJ	LINE	SOURCE STATEMENT	
8161	CDAE81	239+	CALL PLLT	
8164	3E06	240	MVI A,06H	{READ BUCKET VELOCITY INPUT FROM
8166	CD7381	241	CALL ADCON	{ JOYSTICK
8169	CD2E82	242	CALL JOYSTK	
		243	PLL JBKT	
816C	110C30	244+	LXI D,JBKT	
816F	CDAE81	245+	CALL PLLT	
8172	C9	246	RET	
		247		{
		248		{
		249		{
		250		{** SUBROUTINE ADCON **
		251		{
		252		{OPERATES THE ANALOGUE TO DIGITAL
		253		{ CONVERTER. THE CHANNEL NUMBER
		254		{ IS IN THE A REGISTER ON CALLING
		255		{ AND THE RESULT AT RETURN
		256		{
		257		{REGISTERS AFFECTED: A,H,L,STATUS
		258		{
8173	D32B	259	ADCON: OUT 2BH	{OUTPUT CHANNEL NUMBER
8175	C608	260	ADI 08H	{LATCH CHANNEL NUMBER
8177	D32B	261	OUT 2BH	{
8179	AF	262	XRA A	{CLEAR CONTROL WORD
817A	D32B	263	OUT 2BH	
817C	211100	264	LXI H,0011H	{SET DELAY VALUE
817F	CD8D81	265	CALL PAUSE	{CALL DELAY ROUTINE
8182	3E10	266	MVI A,10H	{SET TRISTATE OUTPUT
8184	D32B	267	OUT 2BH	
8186	00	268	NOP	
8187	00	269	NOP	
8188	00	270	NOP	
8189	00	271	NOP	
818A	DB29	272	IN 29H	{READ RESULT
818C	C9	273	RET	
		274		{
		275		{
		276		{** PAUSE **
		277		{
		278		{SUBROUTINE FOR DELAY
		279		{ DECREMENTS INPUT IN HL
		280		{ REGISTER PAIR UNTIL ZERO
		281		{
		282		{REGISTERS AFFECTED: H,L,STATUS
		283		{
818D	2B	284	PAUSE: DCX H	
818E	7C	285	MOV A,H	
818F	B5	286	ORA L	
8190	C28D81	287	JNZ PAUSE	
8193	C9	288	RET	
		289		{
		290		{
		291		{
		292		{** SUBROUTINE PSHT **
		293		{

LOC	.OBJ	LINE	SOURCE STATEMENT	
		294		{PUSHES A 32-BIT FL. PT. VARIABLE
		295		{ ONTO THE APU STACK
		296		{ DE CONTAINS THE ADDRESS
		297		{ OF THE LS BYTE OF THE
		298		{ OPERAND ON CALLING
		299		{ AND OF THE MS BYTE AT
		300		{ RETURN
		301		{
		302		{REGISTERS AFFECTED: D,E
		303		{
8194	C5	304	PSHT: PUSH B	{PUSH ACC ON STACK
8195	47	305	MOV B+A	
8196	C5	306	PUSH B	
8197	1A	307	LDAX D	{LD ACC WITH LS BYTE
8198	320010	308	STA 1000H	{PUSH ACC TO APU
8198	13	309	INX D	{INCREMENT DATA POINTER
819C	1A	310	LDAX D	
819D	320010	311	STA 1000H	
81A0	13	312	INX D	
81A1	1A	313	LDAX D	
81A2	320010	314	STA 1000H	
81A5	13	315	INX D	
81A6	1A	316	LDAX D	
81A7	320010	317	STA 1000H	
81AA	C1	318	POP B	
81AB	78	319	MOV A,B	
81AC	C1	320	POP B	
81AD	C9	321	RET	
		322		{
		323		{
		324		{** SUBROUTINE PLLT **
		325		{
		326		{PULLS A 32-BIT FL. PT. VARIABLE
		327		{ FROM THE APU STACK
		328		{ DE CONTAINS ADDRESS OF LS
		329		{ BYTE ON CALLING AND MS
		330		{ BYTE AT RETURN
		331		{
		332		{REGISTERS AFFECTED: D,E
		333		{
81AE	C5	334	PLLT: PUSH B	
81AF	47	335	MOV B+A	
81B0	C5	336	PUSH B	
81B1	13	337	INX D	
81B2	13	338	INX D	
81B3	13	339	INX D	
81B4	3A0010	340	LDA 1000H	
81B7	12	341	STAX D	
81B8	18	342	DCX D	
81B9	3A0010	343	LDA 1000H	
81BC	12	344	STAX D	
81BD	18	345	DCX D	
81BE	3A0010	346	LDA 1000H	
81C1	12	347	STAX D	
81C2	18	348	DCX D	

LOC	OBJ	LINE	SOURCE	STATEMENT
81C3	JA0010	349	LDA	1000H
81C6	12	350	STAX	D
81C7	C1	351	POP	B
81C8	78	352	MOV	A,B
81C9	C1	353	POP	B
81CA	C9	354	RET	
		355		
		356		
		357		** SET OF SUBROUTINES FOR EVALUATING
		358		OPERATORS IN CONDITIONAL JUMPS **
		359		
		360		EACH SUBROUTINE RETURNS 01H IN THE
		361		ACCUMULATOR IF THE CONDITION IT TESTS IS VALID.
		362		
		363		REGISTERS AFFECTED A,D,E,STATUS
		364		
81CB	CD0882	365	GTHAN: CALL	EQUALS
		366		CALL EQ TO CHECK FOR EQUALITY AND
		367		SET SIGN BIT
81CE	E601	367	ANI	01H
81D0	CAD581	368	JZ	L2
81D3	AF	369	XRA	A
81D4	C9	370	RET	
81D5	JA1830	371	L2: LDA	STATUS
81D8	E640	372	ANI	40H
81DA	CADF81	373	JZ	L3
81DD	AF	374	XRA	A
81DE	C9	375	RET	
81DF	3E01	376	L3: MVI	A,01H
81E1	C9	377	RET	
		378		
		379		
81E2	CD0882	380	LTHAN: CALL	EQUALS
81E5	E601	381	ANI	01H
		382		CALL EQ TO CHECK FOR EQUALITY AND SET
		383		SIGN BIT OF APU FOR THE SUBTRACTION
81E7	CAEC81	383	JZ	L4
81EA	AF	384	XRA	A
81EB	C9	385	RET	
81EC	JA1830	386	L4: LDA	STATUS
81EF	E640	387	ANI	40H
81F1	C2F681	388	JNZ	L5
81F4	AF	389	XRA	A
81F5	C9	390	RET	
81F6	3E01	391	L5: MVI	A,01H
81F8	C9	392	RET	
		393		
		394		
81F9	CDE281	395	GEQUAL: CALL	LTHAN
81FC	2F	396	CMA	
81FD	C9	397	RET	
		398		
		399		
81FE	CDCB81	400	LEQUAL: CALL	GTHAN
8201	2F	401	CMA	
8202	C9	402	RET	
		403		
				CALL LT AND INVERT RESULT
				CALL GT AND INVERT RESULT

LOC	OBJ	LINE	SOURCE STATEMENT
8203	CD0882	404	NEQUAL: CALL EQUALS
8206	2F	405	CMA
8207	C9	406	RET
		407	
		408	
		409	EQUALS: PSH V1
8208	111D30	410+	LXI D,V1
8208	CD9481	411+	CALL PSHT
		412	PSH V2
820E	112130	413+	LXI D,V2
8211	CD9481	414+	CALL PSHT
8214	CDB584	415	CALL FSUB
8217	3A0011	416 L6:	LDA 1100H
821A	E680	417	ANI 80H
821C	C21782	418	JNZ L6
821F	3A0011	419	LDA 1100H
8222	321830	420	STA STATUS
8225	E620	421	ANI 20H
8227	C22882	422	JNZ L7
822A	C9	423	RET
822B	3E01	424 L7:	MVI A,01H
822D	C9	425	RET
		426	
		427	
		428	
		429	
		430	
		431	
		432	
		433	
		434	
		435	
		436	
		437	
		438	
822E	320010	439 JOYSTK:	STA 1000H
8231	AF	440	XRA A
8232	320010	441	STA 1000H
8235	CDA984	442	CALL FLTS
		443	PLL I1
8238	111030	444+	LXI D,I1
8238	CDAE81	445+	CALL PLLT
		446	IFF I1,GTHAN,H87,L50
		447+	PSH I1
823E	111030	448+	LXI D,I1
8241	CD9481	449+	CALL PSHT
		450+	PLL V1
8244	111030	451+	LXI D,V1
8247	CDAE81	452+	CALL PLLT
		453+	PSH H87
824A	111480	454+	LXI D,H87
824D	CD9481	455+	CALL PSHT
		456+	PLL V2
8250	112130	457+	LXI D,V2
8253	CDAE81	458+	CALL PLLT

```

;
;
;SUBTRACT V2 FROM V1
;
;
;WAIT TILL APU NOT BUSY
;
;TRANSFER APU STATUS TO CORE
;CHECK ZERO BIT
;RETURN 00 IN A REG INDICATING INEQUALTY
;RETURN 01 IN A REG INDICATING EQUALITY
;
;
;*** SUBROUTINE JOYSTK **
;
;THE JOYSTICK VOLTAGE IS IN THE A REGISTER
; ON CALLING. THE SUBROUTINE CONVERTS
; IT TO THE RANGE -1 TO +1 AND LEAVES
; THE RESULT ON TOP OF THE APU STACK
;
;REGISTERS AFFECTED: A,D,E,STATUS
;
;CONVERT JOYSTICK VOLTAGE TO 32 BIT
; FORMAT
;
;IF JOYSTICK VOLTAGE>87H THEN L50
    
```

LOC	OBJ	LINE	SOURCE STATEMENT	
8256	CDC881	459+	CALL GTHAN	
8259	E601	460+	ANI 01H	
825B	C28582	461+	JNZ L50	
		462	IFF I1,LTHAN,H79,L51	IF JOYSTICK VOLTAGE (79H THEN L51
		463+	PSH I1	
825E	111030	464+	LXI D,I1	
8261	CD9481	465+	CALL PSHT	
		466+	PLL V1	
8264	111030	467+	LXI D,V1	
8267	CDAE81	468+	CALL PLLT	
		469+	PSH H79	
826A	111880	470+	LXI D,H79	
826D	CD9481	471+	CALL PSHT	
		472+	PLL V2	
8270	112130	473+	LXI D,V2	
8273	CDAE81	474+	CALL PLLT	
8276	CDE281	475+	CALL LTHAN	
8279	E601	476+	ANI 01H	
827B	C29E82	477+	JNZ L51	
		478	PSH ZERO	JOYSTICK IN CENTRAL DEAD BAND:
827E	111C60	479+	LXI D,ZERO	
8281	CD9481	480+	CALL PSHT	
8284	C9	481	RET	RETURN ZERO RESULT
		482 L50:	PSH I1	OFFSET AND SCALE JOYSTICK VOLTAGE
8285	111030	483+	LXI D,I1	
8288	CD9481	484+	CALL PSHT	
		485	PSH H87	FOR POSITIVE DEFLECTION
828B	111480	486+	LXI D,H87	
828E	CD9481	487+	CALL PSHT	
8291	CDB584	488	CALL FSUB	
		489	PSH D14	PUSH 14 BASE 10
8294	112C80	490+	LXI D,D14	
8297	CD9481	491+	CALL PSHT	
829A	CDC184	492	CALL FDIV	
829D	C9	493	RET	
		494 L51:	PSH I1	OFFSET AND SCALE JOYSTICK VOLTAGE
829E	111030	495+	LXI D,I1	
82A1	CD9481	496+	CALL PSHT	
		497	PSH H79	FOR NEGATIVE DEFLECTION
82A4	111880	498+	LXI D,H79	
82A7	CD9481	499+	CALL PSHT	
82AA	CDB584	500	CALL FSUB	
		501	PSH D14	
82AD	112C80	502+	LXI D,D14	
82B0	CD9481	503+	CALL PSHT	
82B3	CDC184	504	CALL FDIV	
82B6	C9	505	RET	
		506		}
		507		}
		508		}
		509		}
		510		}
		511		** SUBROUTINE OUTPUT **
		512		}
		513		OPERATES CUT-OFF, OFFSETS

LOC	OBJ	LINE	SOURCE STATEMENT	
		514		AND OUTPUTS VOLTAGES TO
		515		VALVES
		516		
		517		REGISTERS AFFECTED: A,D,E,STATUS
		518		
		519	OUTPUT: PSH VVSLEW	SET SLEW VALVE
82B7	112530	520+	LXI D,VVSLEW	
82BA	CD9481	521+	CALL PSHT	
		522		SET UP PARAMETERS FOR SUBROUTINE
		523		VLIN WHICH CONVERTS 32 BIT VALVE
		524		SETTING VVSLEW TO 8 BIT CONTROL BYTE
		525		TO BE OUTPUT TO THE VALVE DRIVER
		526		CIRCUIT
		527		
		528	PLL FVO	FVO=VVSLEW
82BD	113930	529+	LXI D,FVO	
82C0	CDAE81	530+	CALL PLLT	
82C3	3A4C30	531	LDA SPOF	
82C6	324030	532	STA POF	POF=SPOF
82C9	3A4E30	533	LDA SNOF	
82CC	324130	534	STA NOF	NOF=SNOF
82CF	3A4D30	535	LDA SPMAX	
82D2	324230	536	STA PMAX	PMAX=SPMAX
82D5	3A4F30	537	LDA SNMAX	
82D8	324330	538	STA NMAX	NMAX=SNMAX
82DB	CDA883	539	CALL VLIN	SUBROUTINE VLIN RETURNS RESULT
		540		IN A REGISTER
82DE	323530	541	STA VS	
82E1	D300	542	OUT 00H	OUTPUT DATA TO SLEW VALVE DRIVER
		543	L52: PSH VVALFA	SET LIFT VALVE
82E3	112930	544+	LXI D,VVALFA	
82E6	CD9481	545+	CALL PSHT	
		546	PLL FVO	
82E9	113930	547+	LXI D,FVO	
82EC	CDAE81	548+	CALL PLLT	
82EF	3A4430	549	LDA APOF	
82F2	324030	550	STA POF	
82F5	3A4630	551	LDA ANOF	
82F8	324130	552	STA NOF	
82FB	3A4530	553	LDA APMAX	
82FE	324230	554	STA PMAX	
8301	3A4730	555	LDA ANMAX	
8304	324330	556	STA NMAX	
8307	CDA883	557	CALL VLIN	
830A	323630	558	STA VL	
830D	D301	559	OUT 01H	
		560	L53: PSH VVBETA	SET REACH VALVE
830F	112D30	561+	LXI D,VVBETA	
8312	CD9481	562+	CALL PSHT	
		563	PLL FVO	
8315	113930	564+	LXI D,FVO	
8318	CDAE81	565+	CALL PLLT	
831B	3A4830	566	LDA BPOF	
831E	324030	567	STA POF	
8321	3A4A30	568	LDA BNOF	

LOC	OBJ	LINE	SOURCE STATEMENT
8324	324130	569	STA NOF
8327	3A4930	570	LDA BPMAX
832A	324230	571	STA PMAX
832D	3A4B30	572	LDA BNMAX
8330	324330	573	STA NMAX
8333	CDAB83	574	CALL VLIN
8336	323730	575	STA VR
8339	D321	576	OUT 21H
		577 L54:	IFF VVBKT,EQUALS,ZERO,L55 ISET BUCKET SWITCH
		578+	PSH VVBKT
833B	113130	579+	LXI D,VVBKT
833E	CD9481	580+	CALL PSHT
		581+	PLL V1
8341	111D30	582+	LXI D,V1
8344	CDAE81	583+	CALL PLLT
		584+	PSH ZERO
8347	111C80	585+	LXI D,ZERO
834A	CD9481	586+	CALL PSHT
		587+	PLL V2
834D	112130	588+	LXI D,V2
8350	CDAE81	589+	CALL PLLT
8353	CD0882	590+	CALL EQUALS
8356	E601	591+	ANI 01H
8358	C27E83	592+	JNZ L55
		593	IFF VVBKT,GTHAN,ZERO,L56
		594+	PSH VVBKT
835B	113130	595+	LXI D,VVBKT
835E	CD9481	596+	CALL PSHT
		597+	PLL V1
8361	111D30	598+	LXI D,V1
8364	CDAE81	599+	CALL PLLT
		600+	PSH ZERO
8367	111C80	601+	LXI D,ZERO
836A	CD9481	602+	CALL PSHT
		603+	PLL V2
836D	112130	604+	LXI D,V2
8370	CDAE81	605+	CALL PLLT
8373	CDCB81	606+	CALL GTHAN
8376	E601	607+	ANI 01H
8378	C28683	608+	JNZ L56
837B	C38E83	609	JMP L57
837E	JECO	610 L55:	MVI A,00COH ISEGMENT FOR STATIC BUCKET
8380	323830	611	STA VB
8383	D322	612	OUT 22H
8385	C9	613	RET
8386	3E80	614 L56:	MVI A,80H ISEGMENT FOR OPENING BUCKET
8388	323830	615	STA VB
838B	D322	616	OUT 22H
838D	C9	617	RET
838E	3E40	618 L57:	MVI A,40H ISEGMENT FOR CLOSING BUCKET
8390	323830	619	STA VB
8393	D322	620	OUT 22H
8395	C9	621	RET
		622	
		623	

LOC	OBJ	LINE	SOURCE STATEMENT
		624	! ** SUBROUTINE FLOAT **
		625	!
		626	! PUTS CONTENTS OF A REGISTER
		627	! ON TOP OF APU STACK
		628	!
		629	! REGISTERS AFFECTED: A
		630	!
8396	320010	631	FLOAT: STA 1000H
8399	AF	632	XRA A
839A	320010	633	STA 1000H
839D	CDA984	634	CALL FLTS
83A0	C9	635	RET
		636	!
		637	!
		638	! ** SUBROUTINE FIX **
		639	!
		640	! PUTS 32-BIT TOS OF APU
		641	! IN THE A REGISTER
		642	!
		643	! REGISTERS AFFECTED: A
		644	!
83A1	CDCD84	645	FIX: CALL FIXS
83A4	3A0010	646	LDA 1000H
83A7	3A0010	647	LDA 1000H
83AA	C9	648	RET
		649	!
		650	!
		651	! ** SUBROUTINE VLIN **
		652	!
		653	! VALVE OPENING IN NOMINAL RANGE -1 TO
		654	! +1 IS PASSED IN FVO.
		655	! SUBROUTINE CALCULATES BYTE TO
		656	! BE OUTPUT TO THE DRIVER CIRCUIT
		657	! USING DATA POS, PMAX, NOS, & NMAX.
		658	!
		659	! REGISTERS AFFECTED: A,D,E,STATUS
		660	!
		661	VLIN: IFF FVO,GTHAN,ZERO,L61
		662+	PSH FVO
83AB	113930	663+	LXI D,FVO
83AE	CD9481	664+	CALL PSHT
		665+	PLL V1
83B1	111D30	666+	LXI D,V1
83B4	CDAE81	667+	CALL PLLT
		668+	PSH ZERO
83B7	111C80	669+	LXI D,ZERO
83BA	CD9481	670+	CALL PSHT
		671+	PLL V2
83BD	112130	672+	LXI D,V2
83C0	CDAE81	673+	CALL PLLT
83C3	CDCB81	674+	CALL GTHAN
83C6	E601	675+	ANI 01H
83C8	C2ED83	676+	JNZ L61
		677	IFF FVO,LTHAN,ZERO,L62
		678+	PSH FVO

LOC	OBJ	LINE	SOURCE STATEMENT
83CB	113930	679+	LXI D,FV0
83CE	CD9481	680+	CALL PSHT
		681+	PLL V1
83D1	111D30	682+	LXI D,V1
83D4	CDAE81	683+	CALL PLLT
		684+	PSH ZERO
83D7	111C80	685+	LXI D,ZERO
83DA	CD9481	686+	CALL PSHT
		687+	PLL V2
83DD	112130	688+	LXI D,V2
83E0	CDAE81	689+	CALL PLLT
83E3	CDE281	690+	CALL LTHAN
83E6	E601	691+	ANI 01H
83E8	C22184	692+	JNZ L62
83EB	AF	693	XRA A
83EC	C9	694	RET
		695 L61:	IFF FV0,LTHAN,ONE,L63
		696+	PSH FV0
83ED	113930	697+	LXI D,FV0
83F0	CD9481	698+	CALL PSHT
		699+	PLL V1
83F3	111D30	700+	LXI D,V1
83F6	CDAE81	701+	CALL PLLT
		702+	PSH ONE
83F9	112080	703+	LXI D,ONE
83FC	CD9481	704+	CALL PSHT
		705+	PLL V2
83FF	112130	706+	LXI D,V2
8402	CDAE81	707+	CALL PLLT
8405	CDE281	708+	CALL LTHAN
8408	E601	709+	ANI 01H
840A	C21184	710+	JNZ L63
840D	3A4230	711	LDA PMAX
8410	C9	712	RET
8411	3A4030	713 L63:	POF
8414	323E30	714	STA OFFSET
8417	3A4230	715	LDA PMAX
841A	323F30	716	STA MAX
841D	C36084	717	JMP L64
8420	C9	718	RET
		719 L62:	FV0,GTHAN,MINONE,L65
		720+	PSH FV0
8421	113930	721+	LXI D,FV0
8424	CD9481	722+	CALL PSHT
		723+	PLL V1
8427	111D30	724+	LXI D,V1
842A	CDAE81	725+	CALL PLLT
		726+	PSH MINONE
842D	112880	727+	LXI D,MINONE
8430	CD9481	728+	CALL PSHT
		729+	PLL V2
8433	112130	730+	LXI D,V2
8436	CDAE81	731+	CALL PLLT
8439	CDCB81	732+	CALL GTHAN
843C	E601	733+	ANI 01H

1 SEGMENT FOR FV0=0

1 SEGMENT FOR FV0) PMAX

1 SEGMENT FOR 0 (FV0 (1

LOC	OBJ	LINE	SOURCE STATEMENT
843E	C24584	734+	JNZ L65
8441	3A4330	735	LDA NMAX
8444	C9	736	RET
8445	3A4130	737 L65:	LDA NOF
8448	323E30	738	STA OFFSET
844B	3A4330	739	LDA NMAX
844E	323F30	740	STA MAX
		741	PSH FVO
8451	113930	742+	LXI D,FVO
8454	CD9481	743+	CALL PSHT
8457	CD9D84	744	CALL CHSF
		745	PLL FVO
845A	113930	746+	LXI D,FVO
845D	CDAE81	747+	CALL PLLT
8460	3A3E30	748 L64:	LDA OFFSET
8463	CD9683	749	CALL FLOAT
8466	CDE584	750	CALL PTOF
8469	3A3F30	751	LDA MAX
846C	CD9683	752	CALL FLOAT
846F	CD3985	753	CALL XCHF
8472	CDB584	754	CALL FSUB
		755	PSH FVO
8475	113930	756+	LXI D,FVO
8478	CD9481	757+	CALL PSHT
847B	CD9184	758	CALL FMUL
847E	CD8584	759	CALL FADD
8481	CDA183	760	CALL FIX
8484	C9	761	RET
		762	
		763	
		764	! ** MATHS SUBROUTINES MACRO **
		765	!
		766	!REGISTERS AFFECTED: NONE
		767	!
		768 MATHS	MACRO FNCTN, CODE
-		769 FNCTN:	STA ASTR
-		770	MVI A, CODE
-		771	STA 1100H
-		772	LDA ASTR
-		773	RET
		774	ENDM
		775	
		776	
		777	!MATHS MACRO CALLS
		778	!
		779	!ALL OPERANDS ARE 32 BIT FLOATING POINT
		780	! UNLESS OTHERWISE SPECIFIED
		781	!
		782	!TOS=TOS+NOS
8485	323D30	783+FADD:	STA ASTR
8488	3E10	784+	MVI A, 10H
848A	320011	785+	STA 1100H
848D	3A3D30	786+	LDA ASTR
8490	C9	787+	RET
		788	MATHS FMUL, 12H
			!TOS=TOS+NOS

LOC	OBJ	LINE	SOURCE STATEMENT	
8491	323D30	789+FMUL:	STA ASTR	
8494	3E12	790+	MVI A,12H	
8496	320011	791+	STA 1100H	
8499	3A3D30	792+	LDA ASTR	
849C	C9	793+	RET	
		794	MATHS CHSF,15H	ITOS--TOS
849D	323D30	795+CHSF:	STA ASTR	
84A0	3E15	796+	MVI A,15H	
84A2	320011	797+	STA 1100H	
84A5	3A3D30	798+	LDA ASTR	
84A8	C9	799+	RET	
		800	MATHS FLTS,1DH	ICONVERT 16 BIT TOS TO 32 BIT FL. PT.
84A9	323D30	801+FLTS:	STA ASTR	
84AC	3E1D	802+	MVI A,1DH	
84AE	320011	803+	STA 1100H	
84B1	3A3D30	804+	LDA ASTR	
84B4	C9	805+	RET	
		806	MATHS FSUB,11H	ITOS=NOS-TOS
84B5	323D30	807+FSUB:	STA ASTR	
84B8	3E11	808+	MVI A,11H	
84BA	320011	809+	STA 1100H	
84BD	3A3D30	810+	LDA ASTR	
84C0	C9	811+	RET	
		812	MATHS FDIV,13H	ITOS=NOS/TOS
84C1	323D30	813+FDIV:	STA ASTR	
84C4	3E13	814+	MVI A,13H	
84C6	320011	815+	STA 1100H	
84C9	3A3D30	816+	LDA ASTR	
84CC	C9	817+	RET	
		818	MATHS FIXS,1FH	ICONVERT 32 BIT FL. PT. TOS TO 16 BIT
84CD	323D30	819+FIXS:	STA ASTR	
84D0	3E1F	820+	MVI A,1FH	
84D2	320011	821+	STA 1100H	
84D5	3A3D30	822+	LDA ASTR	
84D8	C9	823+	RET	
		824	MATHS PTOS,77H	ICOPY 16 BIT TOS ONTO STACK
84D9	323D30	825+PTOS:	STA ASTR	
84DC	3E77	826+	MVI A,77H	
84DE	320011	827+	STA 1100H	
84E1	3A3D30	828+	LDA ASTR	
84E4	C9	829+	RET	
		830	MATHS PTOF,17H	ICOPY 32 BIT TOS ONTO STACK
84E5	323D30	831+PTOF:	STA ASTR	
84E8	3E17	832+	MVI A,17H	
84EA	320011	833+	STA 1100H	
84ED	3A3D30	834+	LDA ASTR	
84F0	C9	835+	RET	
		836	MATHS POPF,18H	IRotate TOS TO BOTTOM OF STACK
84F1	323D30	837+POPF:	STA ASTR	
84F4	3E18	838+	MVI A,18H	
84F6	320011	839+	STA 1100H	
84F9	3A3D30	840+	LDA ASTR	
84FC	C9	841+	RET	
		842	MATHS PUPI,1AH	IPUSH PI ONTO TOS
84FD	323D30	843+PUPI:	STA ASTR	

LOC	OBJ	LINE	SOURCE STATEMENT
8500	3E1A	844+	MVI A,1AH
8502	320011	845+	STA 1100H
8505	3A3D30	846+	LDA ASTR
8508	C9	847+	RET
		848	MATHS SIN,02H
8509	323D30	849+SIN:	STA ASTR
850C	3E02	850+	MVI A,02H
850E	320011	851+	STA 1100H
8511	3A3D30	852+	LDA ASTR
8514	C9	853+	RET
		854	MATHS ASIN,05H
8515	323D30	855+ASIN:	STA ASTR
8518	3E05	856+	MVI A,05H
851A	320011	857+	STA 1100H
851D	3A3D30	858+	LDA ASTR
8520	C9	859+	RET
		860	MATHS COS,03H
8521	323D30	861+COS:	STA ASTR
8524	3E03	862+	MVI A,03H
8526	320011	863+	STA 1100H
8529	3A3D30	864+	LDA ASTR
852C	C9	865+	RET
		866	MATHS ACOS,06H
852D	323D30	867+ACOS:	STA ASTR
8530	3E06	868+	MVI A,06H
8532	320011	869+	STA 1100H
8535	3A3D30	870+	LDA ASTR
8538	C9	871+	RET
		872	MATHS XCHF,19H
8539	323D30	873+XCHF:	STA ASTR
853C	3E19	874+	MVI A,19H
853E	320011	875+	STA 1100H
8541	3A3D30	876+	LDA ASTR
8544	C9	877+	RET
		878	MATHS SQRT,01H
8545	323D30	879+SQRT:	STA ASTR
8548	3E01	880+	MVI A,01H
854A	320011	881+	STA 1100H
854D	3A3D30	882+	LDA ASTR
8550	C9	883+	RET
		884	END

PUBLIC SYMBOLS

EXTERNAL SYMBOLS

USER SYMBOLS

ACOS	A 852D	ADCON	A 8173	ANMAX	A 3047	ANOF	A 3046	APMAX	A 3045	APOF	A 3044	ASIN	A 8515
ASTR	A 303D	BNMAX	A 3048	ENOF	A 304A	BPMAX	A 3049	BPOF	A 3048	CHSF	A 849D	CNST20	A 8030
CNST21	A 8034	CONV	A 813A	COS	A 8521	D14	A 802C	DLOOP	A 80D8	EQUALS	A 8208	FADD	A 8485
FDIV	A 84C1	FIX	A 83A1	FIXS	A 84CD	FLOAT	A 8396	FLTS	A 84A9	FMUL	A 8491	FSUB	A 8485
FVD	A 3039	GEDUAL	A 81F9	GTHAN	A 81CB	H255	A 8038	H79	A 8018	H87	A 8014	HALF	A 8024

I1	A 3010	I2	A 3014	IFF	+ 0002	INIT	A 812B	JBKT	A 300C	JOYSTK	A 822E	JSLEW	A 3008
JXDOT	A 3000	JYDOT	A 3004	L2	A 8105	L3	A 810F	L4	A 81EC	L5	A 81F6	L50	A 8285
L51	A 829E	L52	A 82E3	L53	A 830F	L54	A 833B	L55	A 837E	L56	A 8386	L57	A 838E
L6	A 8217	L61	A 83ED	L62	A 8421	L63	A 8411	L64	A 8460	L65	A 8445	L7	A 822B
LEQUAL	A 81FE	LOOP	A 80EF	LTHAN	A 81E2	MATHS	+ 0003	MAX	A 303F	MINONE	A 8028	NEQUAL	A 8203
NMAX	A 3043	NOF	A 3041	OFFSET	A 303E	ONE	A 8020	OUTPUT	A 82B7	PAUSE	A 818D	PLL	+ 0001
PLLT	A 81AE	PMAX	A 3042	POF	A 3040	POPF	A 84F1	PSH	+ 0000	PSHT	A 8194	PTOF	A 84E5
PTOS	A 8409	PUPI	A 84FD	S	A 3019	SIN	A 8509	SNMAX	A 304F	SNOF	A 304E	SPMAX	A 304D
SPOF	A 304C	SQRT	A 8545	STATUS	A 3018	TEN	A 800C	TWO	A 8010	V1	A 3010	V2	A 3021
VB	A 3038	VL	A 3036	VLIN	A 83AB	VR	A 3037	VS	A 3035	VVALFA	A 3029	VVBETA	A 302D
VVBKT	A 3031	VVSLEW	A 3025	XANMAX	A 8003	XANOF	A 8002	XAPMAX	A 8001	XAPOF	A 8000	XBNMAX	A 8007
XBNOF	A 8006	XBPMAX	A 8005	XBPOF	A 8004	XCHF	A 8539	XSNMAX	A 800B	XSNDF	A 800A	XSPMAX	A 8009
XSPDF	A 8008	ZERO	A 801C										

ASSEMBLY COMPLETE, NO ERRORS

APPENDIX B

PROGRAM DIG

LOC	OBJ	LINE	SOURCE STATEMENT
		1	*MOD85 MACROFILE
3000		2	ORG 3000H
		3	
		4	
		5	
		6	
		7	
		8	
		9	
		10	
		11	
		12	
		13	
		14	
		15	
		16	
		17	
3000		18	MODFLG: DS 1
3001		19	DX: DS 4
3005		20	AI: DS 4
3009		21	BI: DS 4
300D		22	AA: DS 4
3011		23	AB: DS 4
3015		24	XOF: DS 4
3019		25	YOF: DS 4
301D		26	MODE: DS 1
301E		27	PPPOINT: DS 2
3020		28	XP: DS 4
3024		29	YP: DS 4
3028		30	PSIP: DS 4
302C		31	DIST: DS 4
3030		32	DPSI: DS 4
3034		33	PCOUNT: DS 1
3035		34	RCOUNT: DS 1
3036		35	NCOUNT: DS 1
3037		36	TFLAG: DS 1
		37	
3039		38	JXDOT: DS 4
303C		39	JYDOT: DS 4
3040		40	JSLEW: DS 4
3044		41	JBKT: DS 4
3048		42	I1: DS 4
304C		43	I2: DS 4
3050		44	CXDOT: DS 4
3054		45	CYDOT: DS 4
3058		46	XI: DS 4
305C		47	YI: DS 4
3060		48	PSII: DS 4
3064		49	XO: DS 4
3068		50	YO: DS 4
306C		51	PSIO: DS 4
3070		52	EX: DS 4
3074		53	EY: DS 4
3078		54	EPSI: DS 4


```

;UNIVERSITY OF LIVERPOOL
;DEPARTMENT OF ELECTRICAL ENGINEERING
; AND ELECTRONICS
;
;E.R.I. DEANE
;
;THIS IS AN ASSEMBLY LANGUAGE PROGRAM
; FOR "X-Y" CONTROL OF A PA6 DIGGER
; WITH A LEARN AND REPEAT FACILITY
;
;CODE EDITED 1600 5TH JANUARY 1983
; DISK: NO. 4 VER 5.33
;
; ** RAM LOCATIONS FOR PROGRAM VARIABLES **
;
;BYTE TO REGISTER MODE
;DISTANCE FROM ALPHA PIVOT TO BUCKET PIVOT
;INPUT TO ALPHA CONTROL LOOP
;INPUT TO BETA CONTROL LOOP
;INTERMEDIATE RESULT IN CALCULATING AI
;INTERMEDIATE RESULT IN CALCULATING AI
;X OFFSET USED IN REPEAT MODE
;Y OFFSET USED IN REPEAT MODE
;IMAGE OF DATA FROM MODE SWITCHES
;PATH STACK POINTER
;VARIABLE FOR LEARN ROUTINE
; " " " "
; " " " "
; " " " "
; " " " "
;
;PATH POINT COUNTER FOR LEARN
;COUNTS PATH POINTS FOR REPEAT
;COUNTS CONTROL ROUTINE CALLS FOR REPEAT
;IMAGE OF DATA SENT TO PORT 2A FOR
; MEASURING LOOP EXECUTION TIME
;JOYSTICK INPUT XDOT IN USER CO-ORDS
; " " " YDOT " " "
; " " " SLEW RATE
; " " " BUCKET MOVEMENT
;INTERMEDIATE RESULT LOCATION
;INTERMEDIATE RESULT LOCATION
;XDOT INPUT TO CONTROL LOOP
;YDOT INPUT TO CONTROL LOOP
;X INPUT TO CONTROL LOOP
;Y INPUT TO CONTROL LOOP
;PSI INPUT TO CONTROL LOOP
;X OUTPUT POSITION
;Y OUTPUT POSITION
;PSI OUTPUT VALUE
;X POSITIONAL ERROR = XI-XO
;Y POSITIONAL ERROR = YI-YO
;PSI POSITIONAL ERROR = PSII-PSIO
    
```


LOC	OBJ	LINE	SOURCE STATEMENT	
3105		110	AMAX: DS 4	{MAXIMUM ALPHA VALUE
3109		111	BMIN: DS 4	{MINIMUM BETA VALUE
310D		112	BMAX: DS 4	{MAXIMUM BETA VALUE
3111		113	BASE: DS 1	{BASE LOCATION OF RAM FOR PATH STORAGE
		114		{
		115		{** ROM LOCATIONS CONTAINING DEFAULT
		116		{ VALUES OF PROGRAM CONSTANTS **
		117		{
8000		118	ORG 8000H	
8000	CO	119	XAPCF: DB 0C0H	{ALPHA +VE OFFSET
8001	FF	120	XAPMAX: DB OFFH	{ALPHA +VE SATN. 0/P
8002	40	121	XANCF: DB 40H	{ALPHA -VE OFFSET
8003	7F	122	XANMAX: DB 7FH	{ALPHA -VE SATN. 0/P
8004	40	123	XBPCF: DB 40H	{BETA +VE OFFSET
8005	7F	124	XBPMAX: DB 7FH	{BETA +VE SATN. 0/P
8006	CO	125	XBNOF: DB 0C0H	{BETA -VE OFFSET
8007	FF	126	XBNMAX: DB OFFH	{BETA -VE SATN. 0/P
8008	CO	127	XSPCF: DB 0C0H	{SLEW +VE OFFSET
8009	FF	128	XSPMAX: DB OFFH	{SLEW +VE SATN. 0/P
800A	40	129	XSNCF: DB 40H	{SLEW -VE OFFSET
800B	7F	130	XSNMAX: DB 7FH	{SLEW -VE SATN. 0/P
800C	00	131	XA1A: DB 00H,00H,0A0H,05H	{ALPHA FEEDFORWARD GAIN = 20
800D	00			
800E	A0			
800F	05			
8010	00	132	XA1B: DB 00H,00H,0A0H,05H	{BETA FEEDFORWARD GAIN = 5
8011	00			
8012	A0			
8013	03			
8014	4A	133	XPCRT: DB 4AH,0F3H,8EH,7DH	{PCRT = BKT ERROR MARGIN = 0.07
8015	F3			
8016	8E			
8017	7D			
8018	4A	134	XNCRT: DB 4AH,0F3H,8EH,0FDH	{NCRT = -BKT ERROR MARGIN = -0.07
8019	F3			
801A	8E			
801B	FD			
801C	CC	135	XEMIN: DB 0CCH,0CCH,0CCH,7DH	{CRITICAL X OR Y ERROR = 0.1m
801D	CC			
801E	CC			
801F	7D			
8020	02	136	XEACRT: DB 02H,42H,0B2H,78H	{CRIT. ALPHA ERROR = 0.00272
8021	42			
8022	B2			
8023	78			
8024	C2	137	XEBCRT: DB 0C2H,16H,82H,79H	{CRIT. BETA ERROR = 0.00397
8025	16			
8026	82			
8027	79			
8028	00	138	XCST10: DB 00H,00H,80H,7FH	{CRIT. CHANGE IN JOYSTK READING = 0.25
8029	00			
802A	80			
802B	7F			
802C	06	139	XCST11: DB 06H,0D7H,0A3H,78H	{TARGET COORD INCREMENT FACTOR = 0.02
802D	D7			

LOC	OBJ	LINE	SOURCE STATEMENT	
802E	A3			
802F	7B			
8030	CC	140	XDCRIT: DB OCCH,OCCH,OCCH,7DH	!PATH POINT SPACING = 0.1m
8031	CC			
8032	CC			
8033	7D			
8034	4A	141	XDPCRT: DB 4AH,OF3H,8EH,7EH	!ANGULAR PATH POINT SPACING = 0.140 RAD
8035	F3			
8036	EE			
8037	7E			
8038	01	142	XFFAST: DB 01H	!NO. OF CONTROL CALLS BETWEEN PATH POINTS
		143		! FOR REPEAT FAST
8039	0C	144	XFSLOW: DB 0CH	!NO. OF CONTROL CALLS BETWEEN PATH POINTS
		145		! FOR REPEAT SLOW
803A	01	146	XDELAY: DB 01H,00H	
803B	00			
803C	40	147	XAMIN: DB 40H,3EH,9EH,01H	!MIN ALPHA VALUE = 1.19 rad
803D	3E			
803E	98			
803F	01			
8040	A8	148	XAMAX: DB 0A6H,OF1H,0A2H,02H	!MAX ALPHA VALUE = 2.55 rad
8041	F1			
8042	A2			
8043	02			
8044	C2	149	XBMIN: DB 0C2H,0FEH,92H,00H	!MIN BETA VALUE = 0.574 rad
8045	FE			
8046	92			
8047	00			
8048	F2	150	XBMAX: DB 0F2H,0FDH,9CH,02H	!MAX BETA VALUE = 2.45 rad
8049	FD			
804A	9C			
804B	02			
804C	FF	151	MAXPTS: DB 0FFH	!MAXIMUM NUMBER OF POINTS IN STORED TRAJECTORY
804D	00	152	TEN: DB 00H,00H,0A0H,04H	!10D
804E	00			
804F	A0			
8050	04			
8051	00	153	TWO: DB 00H,00H,80H,02H	!2D
8052	00			
8053	80			
8054	02			
8055	A2	154	MA: DB 0A2H,30H,0B6H,79H	!ALPHA SCALE FACTOR = 0.00556 rad/bit
8056	30			
8057	B6			
8058	79			
8059	CC	155	CA: DB 0CCH,OF7H,93H,01H	!ALPHA OFFSET = 1.16 rad
805A	F7			
805B	93			
805C	01			
805D	40	156	MB: DB 40H,50H,0FCH,79H	!BETA SCALE FACTOR = 0.0077 rad/bit
805E	50			
805F	FC			
8060	79			
8061	00	157	CB: DB 00H,2BH,87H,00H	!BETA OFFSET = 0.528 rad
8062	2B			

LOC	OBJ	LINE	SOURCE STATEMENT	
8063	87			
8064	00			
8065	32	158 MD:	DB 32H,15H,0A9H,79H	!VDelta SCALE FACTOR = 0.00516 rad/bit
8066	13			
8067	A9			
8068	79			
8069	EA	159 CD:	DB 0EAH,051H,0F8H,7FH	!VDelta OFFSET = 0.485 rad
806A	51			
806B	FB			
806C	7F			
806D	84	160 LA:	DB 84H,0EBH,91H,02H	!LENGTH OF LIFT ARM = 2.28m
806E	EB			
806F	91			
8070	02			
8071	CO	161 RA:	DB 0COH,0F5H,0C8H,01H	!LENGTH OF REACH ARM = 1.57m
8072	F3			
8073	C8			
8074	01			
8075	00	162 H87:	DB 00H,00H,087H,08H	!87H = 135D
8076	00			
8077	87			
8078	08			
8079	00	163 H79:	DB 00H,00H,0F2H,07H	!79H = 121D
807A	00			
807B	F2			
807C	07			
807D	00	164 ZERO:	DB 00H,00H,00H,00H	!0D
807E	00			
807F	00			
8080	00			
8081	00	165 ONE:	DB 00H,00H,80H,01H	!1D
8082	00			
8083	80			
8084	01			
8085	FE	166 HALF:	DB 0FEH,0FFH,0FFH,7FH	!0.5D
8086	FF			
8087	FF			
8088	7F			
8089	00	167 MINONE:	DB 00H,00H,80H,81H	!-1D
808A	00			
808B	80			
808C	81			
808D	14	168 MU:	DB 14H,0AEH,97H,02H	! = 2.37 rad
808E	AE			
808F	97			
8090	02			
8091	CA	169 ZETA:	DB 0CAH,0CCH,0CCH,7CH	! = 0.05 rad
8092	CC			
8093	CC			
8094	7C			
8095	0E	170 GC0:	DB 0EH,58H,0E9H,02H	!COEFFICIENTS FOR GAMMA(Delta)
8096	58			
8097	E9			
8098	02			
8099	F2	171 GC1:	DB 0F2H,0B9H,0DAH,0FFH	

LOC	OBJ	LINE	SOURCE STATEMENT
809A	B9		
809B	DA		
809C	FF		
809D	44	172 GC2:	DB 44H,50H,8CH,80H
809E	50		
809F	8C		
80A0	80		
80A1	C0	173 CNST1:	DB 0C0H,39H,0F5H,03H ;LA**2+RA**2 = 7.66 m**2
80A2	39		
80A3	F5		
80A4	03		
80A5	28	174 CNST2:	DB 28H,18H,0E5H,03H ;2*LA*RA = 7.16 m**2
80A6	18		
80A7	E5		
80A8	03		
80A9	A8	175 CNST3:	DB 0A8H,0F1H,0AEH,02H ;LA**2-RA**2 = 2.73 m**2
80AA	F1		
80AB	AE		
80AC	02		
80AD	84	176 CNST4:	DB 84H,0EBH,91H,03H ;2*LA = 4.56m
80AE	EB		
80AF	91		
80B0	03		
80B1	0C	177 CNST9:	DB 0CH,0C7H,0BAH,7CH ;k*1 = 0.0456 m**2
80B2	C7		
80B3	BA		
80B4	7C		
80B5	CE	178 CNST13:	DB 0CEH,0D9H,0C9H,79H ;SLOPE SCALE FACTOR = 0.00616 rad/bit
80B6	D9		
80B7	C9		
80B8	79		
80B9	F6	179 CNST14:	DB 0F6H,0FH,0C9H,80H ;SLOPE OFFSET = -0.785 rad
80BA	0F		
80BB	C9		
80BC	80		
80BD	00	180 CNST20:	DB 00H,00H,0F0H,06H ;3CH = 60D
80BE	00		
80BF	F0		
80C0	06		
80C1	00	181 CNST21:	DB 00H,00H,98H,07H ;4CH = 76D
80C2	00		
80C3	98		
80C4	07		
80C5	00	182 D14:	DB 00H,00H,0E0H,04H ;14D
80C6	00		
80C7	E0		
80C8	04		
80C9	00	183 H255:	DB 00H,00H,0FFH,08H ;FFH = 255D
80CA	00		
80CB	FF		
80CC	08		
		184	;
		185	;
		186	;** MAIN PROGRAM **
		187	;
			INITIALISE SYSTEM

LOC	OBJ	LINE	SOURCE STATEMENT	
		188		
80D0		189	ORG 80D0H	
80D0 0644		190	MVI B,68D	SET UP DEFAULT CONSTANTS IN RAM
80D2 110080		191	LXI D,XAPDF	
80D5 21CD30		192	LXI H,APDF	
80D8 1A		193	DLOOP: LDAX D	LOOP TO TRANSFER DATA FROM ROM INTO RAM
80D9 77		194	MOV M,A	
80DA 13		195	INX D	
80DB 23		196	INX H	
80DC 05		197	DCR B	
80DD C2D880		198	JNZ DLOOP	
		199		
		200		
80E0 3EFS		201	MVI A,0F8H	UNMASK AND DISABLE INTERRUPTS
80E2 30		202	SIM	
80E3 F3		203	DI	
80E4 3ECF		204	MVI A,0CFH	LOAD LOCATION 20CE WITH 0CFH
80E6 32CE20		205	STA 20CEH	FOR VECTORED INTERRUPT HANDLING
		206		
		207		
80E9 31C220		208	LXI SP,20C2H	SET STACK POINTER
80EC CDFE83		209	CALL INIT	CALL ROUTINE FOR SETTING UP
		210		I/O PORT DATA DIRECTION REGISTERS
		211		
		212		
		213		
		214		SEGMENT FOR MODE SELECTION
80EF AF		215	XRA A	
80F0 320030		216	STA MODFLG	
80F3 D300		217	MLOOP: OUT 00H	TURN OFF VALVES
80F5 D301		218	OUT 01H	
80F7 D321		219	OUT 21H	
80F9 2F		220	CMA	
80FA D322		221	OUT 22H	
80FC DB2A		222	L100: IN 2AH	READ SWITCHES FOR MODE SELECTION
80FE 47		223	MOV B,A	
80FF C5		224	PUSH B	PUT INPUT ON TOS
8100 21FF00		225	LXI H,00FFH	CALL DELAY ROUTINE
8103 CD9787		226	CALL PAUSE	
8106 DB2A		227	IN 2AH	READ SWITCHES
8108 C1		228	POP B	COMPARE WITH PREVIOUS INPUT
8109 B8		229	CMP B	
810A C2FC80		230	JNZ L100	
810D 321D30		231	STA MODE	
8110 21FF00		232	L101: LXI H,00FFH	WAIT FOR SWITCH TO BE RELEASED
8113 CD9787		233	CALL PAUSE	
8116 DB2A		234	IN 2AH	
8118 FE00		235	CPI 00H	
811A C21081		236	JNZ L101	
811D 21FF00		237	LXI H,00FFH	
8120 CD9787		238	CALL PAUSE	
8123 DB2A		239	IN 2AH	
8125 FE00		240	CPI 00H	
8127 C21081		241	JNZ L101	
812A 3A1D30		242	LDA MODE	CALL ROUTINE ACCORDING TO MODE &

LOC	OBJ	LINE	SOURCE STATEMENT	
812D	E604	243	ANI 06H	{ JUMP ON RETURN TO START OF LOOP
812F	FE06	244	CPI 06H	
8131	C24881	245	JNZ L102	
8134	3A0030	246	LDA MODFLG	{IF MODFLG = REPEAT SLOW THEN CALL RFCOM
8137	FE01	247	CPI 01H	{ ELSE CALL RFAST
8139	CA4281	248	JZ L108	
813C	CDC083	249	CALL RFAST	
813F	C3F380	250	JMP MLOOP	
8142	CDCA83	251	CALL L108: RFCOM	
8145	C3F380	252	JMP MLOOP	
8148	3A1D30	253	LDA L102: MODE	
814B	E605	254	ANI 05H	
814D	FE05	255	CPI 05H	
814F	C26681	256	JNZ L103	
8152	3A0030	257	LDA MODFLG	{IF MODFLG = REPEAT FAST CALL RSCON
8155	FE01	258	CPI 01H	{ ELSE CALL RSLW
8157	CA6081	259	JZ L109	
815A	CDE183	260	CALL RSLW	
815D	C3F380	261	JMP MLOOP	
8160	CDEB83	262	CALL L109: RSCON	
8163	C3F380	263	JMP MLOOP	
8166	3A1D30	264	LDA L103: MODE	
8169	E602	265	ANI 02H	
816B	FE02	266	CPI 02H	
816D	C27681	267	JNZ L104	
8170	CDE681	268	CALL LEARN	
8173	C3F380	269	JMP MLOOP	
8176	CD7C81	270	CALL L104: MANUAL	
8179	C3F380	271	JMP MLOOP	
		272		{
		273		{
		274		{** SUBROUTINE MANUAL **
		275		{
		276		{SUBROUTINE FOR MANUAL MODE OPERATION
		277		{
		278		{REGISTERS AFFECTED: A,D,E,H,L,STATUS
		279		{
		280	MANUAL: XRA A	{INDICATE MODE
817C	AF	281	STA MODFLG	
817D	320030	282	OUT 23H	
8180	D323	283	CALL LOOP1: XY	{CALL ROUTINE FOR XY CONTROL
8182	CD9081	284	IN 2AH	{CHECK MODE SWITCHES
8185	D82A	285	CPI 00H	
8187	FE00	286	RNZ	
8189	C0	287	EI	{ALLOW INTERRUPT
818A	FB	288	NOP	
818B	00	289	DI	
818C	F3	290	JMP LOOP1	
818D	C38281	291		{
		292		{
		293		{** SUBROUTINE XY **
		294		{
		295		{THIS SUBROUTINE IS THE MAIN
		296		{ CONTROL ROUTINE FOR LINEAR X-Y
		297		{ MOVEMENT OF THE BUCKET BLADE AND

LOC	OBJ	LINE	SOURCE STATEMENT	
		298		{ IS USED IN MANUAL AND LEARN MODES
		299		{
		300		{REGISTERS AFFECTED: A,D,E,H,L,STATUS
		301		{
		302		{
8190	CD1384	303	XY: CALL CONV	{READS IN CONTROL SETTINGS AND
		304		{ OUTPUT POSITIONS
8193	CD3F86	305	CALL COORD	{CALCULATES OUTPUT POSITIONS IN
		306		{ USER COORDINATES
8196	CDD587	307	CALL IP1	{CALCULATES CHANGES IN CONTROL
		308		{ SETTINGS AND DEFINES CONTROL LOOP
		309		{ INPUT VELOCITIES
8199	CD2487	310	CALL EPOS	{CALCULATES POSITIONAL ERRORS
		311		{ IN X AND Y, AND TOTAL ERROR MAGNITUDE ETA
819C	CD9E87	312	CALL SETEC	{SET ECRIT ACCORDING TO INPUT VELOCITIES
819F	CD0284	313	CALL IP2	{IF ETA IS GREATER THAN ECRIT THEN
		314		{ FREEZE TARGET POSITION ELSE ASSIGN
		315		{ NEW TARGET POSITION ACCORDING TO
		316		{ INPUT VELOCITIES
81A2	CD5F89	317	CALL FFD	{CALCULATE VALVE SETTINGS
81A3	CD968C	318	CALL OUTPUT	{OUTPUT VALVE CONTROL BYTES
81A8	C9	319	RET	
		320		{
		321		{
		322		{
		323		{** APU STACK PUSH MACRO **
		324		{
		325		{THIS MACRO GENERATES CODE FOR
		326		{ PUSHING A 32 BIT OPERAND FROM
		327		{ MEMORY ONTO THE APU STACK
		328		{
		329		{REGISTERS AFFECTED: D,E
		330		{
-	-	331	PSH MACRO XYZ	
-	-	332	LXI D,XYZ	
-	-	333	CALL PSHT	
		334	ENDM	
		335		{
		336		{
		337		{** APU STACK POP MACRO **
		338		{
		339		{MACRO FOR POPPING A 32 BIT
		340		{ OPERAND FROM THE APU STACK
		341		{ INTO MEMORY
		342		{
		343		{REGISTERS AFFECTED: D,E
		344		{
-	-	345	PLL MACRO PDR	
-	-	346	LXI D,PDR	
-	-	347	CALL PLLT	
		348	ENDM	
		349		{
		350		{
		351		{
		352		{** MACRO FOR CONDITIONAL JUMPS **

LOC	OBJ	LINE	SOURCE STATEMENT
		353	
		354	
		355	
		356	
		357	
		358	
		359	
		360	
		361	
		362	
		363	
		364	
		365	
		366	
		367	
		368	
		369	
		370	
		371	
		372	
		373	IFF MACRO ID1,OP,ID2,LABL
-		374	PSH ID1
-		375	PLL V1
-		376	PSH ID2
-		377	PLL V2
-		378	CALL OP
-		379	ANI 01H
-		380	JNZ LABL
		381	ENDM
		382	
		383	
		384	
		385	
		386	
		387	
		388	
		389	
		390	
		391	XPXD: LXI H, XD
81A9	216430	392	LXI D, XP
81AC	112030	393	MVI B, 0CH
81AF	040C	394	L201: MOV A, M
81B1	7E	395	STAX D
81B2	12	396	INX H
81B3	23	397	INX D
81B4	13	398	DCR B
81B5	05	399	JNZ L201
81B6	C2B181	400	RET
81B9	C9	401	
		402	
		403	
		404	
		405	
		406	
		407	

```

|
| THIS MACRO GENERATES CODE FOR MAKING
| CONDITIONAL JUMPS DEPENDING ON THE
| VALUES OF TWO 32 BIT FLOATING POINT
| VARIABLES ID1 AND ID2
|
| IF ID1 GTHAN:GEQUAL:EQUALS:NEQUAL:
| LEQUAL:LTHAN ID2
| THEN GOTO LABL
| ELSE CONTINUE
|
| REGISTERS AFFECTED: A,D,E,STATUS
|
| DATA IS PASSED TO SUBROUTINE OP IN
| TEMPORARY VARIABLES V1 AND V2. THE
| RESULT IS RETURNED IN THE A REGISTER.
| 1=TRUE, 0=FALSE. THE RESULT OF OP IS
| CHECKED AND CONTROL JUMPS OR CONTINUES
| ACCORDINGLY
|
|
|
|
| ** ROUTINES FOR LEARN AND REPEAT FUNCTIONS **
|
| ** SUBROUTINE XPXD **
|
| REGISTERS AFFECTED: A,B,D,E,H,L,STATUS
|
| THIS ROUTINE COPIES THE CURRENT OUTPUT
| COORDINATES XD, YD & PSID TO XP, YP
| AND PSIP RESPECTIVELY
|
|
|
| ** SUBROUTINE TPULL **
|
| THIS ROUTINE PULLS A CO-ORDINATE
| FROM THE PATH STACK USING POINTER PPOINT.
| 12 BYTES ARE PULLED, REGISTER B ACTING AS

```

LOC	OBJ	LINE	SOURCE STATEMENT	
		408		{ THE BYTE COUNTER. HL POINTS TO THE
		409		{ DESTINATION ADDRESS AND DE TO THE SOURCE
		410		{ ADDRESS.
		411		{
		412		{REGISTERS AFFECTED: A,B,D,E,H,L,STATUS
		413		{
81BA	2A1E30	414	TPULL: LHL D PPOINT	
81BD	EB	415	XCHG	
81BE	060C	416	MVI B,0CH	
81C0	215830	417	LXI H,XI	
81C3	1A	418	LOOP3: LDAX D	
81C4	77	419	MOV M,A	
81C5	23	420	INX H	
81C6	13	421	INX D	
81C7	05	422	DCR B	
81C8	C2C381	423	JNZ LOOP3	
81C9	EB	424	XCHG	
81CC	221E30	425	SHLD PPOINT	
81CF	C9	426	RET	
		427		{
		428		{
		429		{
		430		{** SUBROUTINE TPUSH **
		431		{
		432		{THIS ROUTINE PUSHES XO, YO, AND PSIO
		433		{ ONTO THE PATH STACK USING DATA
		434		{ POINTER PPOINT. 12 BYTES ARE TO BE
		435		{ TRANSFERRED, REGISTER B IS THE BYTE
		436		{ COUNTER. HL POINTS TO THE SOURCE ADD-
		437		{ RESS AND DE TO THE DESTINATION ADDRESS.
		438		{
		439		{REGISTERS AFFECTED: A,B,D,E,H,L,STATUS
		440		{
		441		{
81D0	2A1E30	442	TPUSH: LHL D PPOINT	{LOAD DE WITH CONTENTS OF PPOINT
81D3	EB	443	XCHG	
81D4	060C	444	MVI B,0CH	{B=12D
81D6	216430	445	LXI H,XO	
81D9	7E	446	LOOP: MOV A,M	
81DA	12	447	STAX D	
81DB	23	448	INX H	
81DC	13	449	INX D	
81DD	05	450	DCR B	
81DE	C2D981	451	JNZ LOOP	
81E1	EB	452	XCHG	{LOAD PPOINT WITH CONTENTS OF DE
81E2	221E30	453	SHLD PPOINT	
81E5	C9	454	RET	
		455		{
		456		{
		457		{** SUBROUTINE LEARN **
		458		{
		459		{ROUTINE FOR LEARNING A PATH
		460		{
		461		{REGISTERS AFFECTED: A,H,L,D,E,STATUS
		462		{

LOC	OBJ	LINE	SOURCE STATEMENT
81E6	3E01	463	LEARN: MVI A,01H ;INDICATE MODE
81E8	D323	464	DUT 23H
81EA	AF	465	XRA A ;ZERO PATH POINT COUNTER PCOUNT
81EB	323430	466	STA PCOUNT
81EE	211131	467	LXI H,BASE ;INITIALISE PPOINT TO BASE ADDRESS
81F1	221E30	468	SHLD PPOINT ; OF PATH STORAGE AREA
81F4	CD981	469	CALL XPXD ;SET XP = XO ETC.
81F7	CDD081	470	CALL TPUSH ;PUSH CURRENT OUTPUT POSITION ON STACK
81FA	CD9081	471	L206: CALL XY ;CALL XY ROUTINE
		472	PSH YO ;IF CURRENT XY COORDINATE)= DCRIT
81FD	116830	473+	LXI D,YO
8200	CD0185	474+	CALL PSHT
		475	PSH YP ; FROM LAST XY COORDINATE JMP L202
8203	112430	476+	LXI D,YP
8206	CD0185	477+	CALL PSHT
8209	CD948E	478	CALL FSUB ;DIST=SQRT((YO-YP)**2+(XO-XP)**2)
820C	CDC48E	479	CALL PTOF
820F	CD708E	480	CALL FMUL
		481	PSH XO
8212	116430	482+	LXI D,XO
8215	CD0185	483+	CALL PSHT
		484	PSH XP
8218	112030	485+	LXI D,XP
821B	CD0185	486+	CALL PSHT
821E	CD948E	487	CALL FSUB
8221	CDC48E	488	CALL PTOF
8224	CD708E	489	CALL FMUL
8227	CD648E	490	CALL FADD
822A	CD246F	491	CALL SORT
		492	PLL DIST
822D	112C30	493+	LXI D,DIST
8230	CD1785	494+	CALL PLLT
		495	IFF DIST,GEQUAL,DCRIT,L202
		496+	PSH DIST
8233	112C30	497+	LXI D,DIST
8236	CD0185	498+	CALL PSHT
		499+	PLL V1
8239	119530	500+	LXI D,V1
823C	CD1785	501+	CALL PLLT
		502+	PSH DCRIT
823F	11F530	503+	LXI D,DCRIT
8242	CD0185	504+	CALL PSHT
		505+	PLL V2
8245	119930	506+	LXI D,V2
8248	CD1785	507+	CALL PLLT
824B	CD5E85	508+	CALL GEQUAL
824E	E601	509+	ANI 01H
8250	C29182	510+	JNZ L202
		511	PSH PSIO ;IF CURRENT PSIO VALUE)= DPCRIT
8253	116C30	512+	LXI D,PSIO
8256	CD0185	513+	CALL PSHT
		514	PSH PSIP ; RECORD NEW PATH POINT ELSE JMP L205
8259	112830	515+	LXI D,PSIP
825C	CD0185	516+	CALL PSHT
825F	CD948E	517	CALL FSUB

LOC	OBJ	LINE	SOURCE STATEMENT
8262	CDC48E	518	CALL PTOF
8263	CD708E	519	CALL FMUL
8268	CD248F	520	CALL SQRT
		521	PLL DPSI
826B	113030	522+	LXI D,DPSI
826E	CD1785	523+	CALL PLLT
		524	IFF DPSI,LTHAN,DPCRIT,L205 ;(DPCRIT = 5 DEG. = 0.0873 RAD)
		525+	PSH DPSI
8271	113030	526+	LXI D,DPSI
8272	CD0185	527+	CALL PSHT
		528+	PLL V1
8277	119530	529+	LXI D,V1
827A	CD1785	530+	CALL PLLT
		531+	PSH DPCRIT
827D	11F930	532+	LXI D,DPCRIT
8280	CD0185	533+	CALL PSHT
		534+	PLL V2
8283	119930	535+	LXI D,V2
8286	CD1785	536+	CALL PLLT
8289	CD4785	537+	CALL LTHAN
828C	E601	538+	ANI 01H
828E	C2A482	539+	JNZ L205
8291	CDA981	540	L205: CALL XPX0 ;XP = X0 ETC.
8294	CDD081	541	CALL TPUSH ;PUT CURRENT O/P POSN ON PATH STACK
8297	3A3430	542	LDA PCOUNT ;INCREMENT PATH POINT COUNTER PCOUNT
829A	3C	543	INR A ; & TEST FOR FULL MEMORY
829B	323430	544	STA PCOUNT
829E	47	545	MOV B,A
829F	3A4C80	546	LDA MAXPTS
82A2	B8	547	CMP B
82A3	C8	548	RZ
82A4	DB2A	549	L205: IN 2AH ;IF INPUT FROM MODE SELECT SWITCHES # 0
82A6	FE00	550	CPI 00H ; THEN RETURN ELSE JUMP TO L206
82A8	CAFA81	551	JZ L206
82AB	C9	552	RET
		553	
		554	
		555	;** SEGMENTS FOR REPEATING A STORED
		556	PATH **
		557	
		558	
		559	;** SUBROUTINE RSETUP **
		560	
		561	THIS ROUTINE INITIALISES THE
		562	COUNTERS, THE DATA POINTER,
		563	AND OFFSETS. IT THEN READS THE
		564	FIRST PATH POINT FOR REPEATING
		565	THE STORED PATH AND CALCULATES
		566	THE OFFSETS XOF AND YOF. IT ALSO
		567	ASSIGNS XI=X0 AND YI=Y0
		568	
82AC	AF	569	RSETUP: XRA A ;ZERO NCOUNT AND RCOUNT
82AD	323630	570	STA NCOUNT ; WHICH COUNT CONTROL ROUTINE CALLS
82B0	323930	571	STA RCOUNT ; AND PATH POINTS RESPECTIVELY
82B3	211131	572	LXI H,BASE ;INITIALISE DATA POINTER

LOC	OBJ	LINE	SOURCE STATEMENT
82B6	221E30	573	SHLD PPOINT
82B9	CDBA81	574	CALL TPULL
		575	PSH XO
82BC	116430	576+	LXI D,XO
82BF	CD0185	577+	CALL PSHT
82C2	CDC48E	578	CALL PTOF
		579	PSH XI
82C5	115830	580+	LXI D,XI
82C8	CD0185	581+	CALL PSHT
82CB	CD948E	582	CALL FSUB
		583	PLL XOF
82CE	111530	584+	LXI D,XOF
82D1	CD1785	585+	CALL PLLT
		586	PLL XI
82D4	115830	587+	LXI D,XI
82D7	CD1785	588+	CALL PLLT
		589	PSH YO
82DA	116830	590+	LXI D,YO
82DD	CD0185	591+	CALL PSHT
82E0	CDC48E	592	CALL PTOF
		593	PSH YI
82E3	115C30	594+	LXI D,YI
82E6	CD0185	595+	CALL PSHT
82E9	CD948E	596	CALL FSUB
		597	PLL YOF
82EC	111930	598+	LXI D,YOF
82EF	CD1785	599+	CALL PLLT
		600	PLL YI
82F2	115C30	601+	LXI D,YI
82F5	CD1785	602+	CALL PLLT
82F8	CD2487	603	CALL EPOS
82FB	C9	604	RET
		605	
		606	
		607	*** SUBROUTINE REPEAT **
		608	
		609	{THIS ROUTINE PULLS SUCCESSIVE
		610	{ POINTS FROM THE PATH STACK AND
		611	{ CALLS THE CONTROL ROUTINES TO
		612	{ MAKE THE MACHINE FOLLOW THE
		613	{ STORED PATH.
		614	{
		615	{REGISTERS AFFECTED: A,B,D,E,H,L,STATUS
		616	{
		617	REPEAT: IFF ETA,GTHAN,ECRIT,L301
		618+	PSH ETA
82FC	117C30	619+	LXI D,ETA
82FF	CD0185	620+	CALL PSHT
		621+	PLL V1
8302	119530	622+	LXI D,V1
8305	CD1785	623+	CALL PLLT
		624+	PSH ECRIT
8308	11BE30	625+	LXI D,ECRIT
830B	CD0185	626+	CALL PSHT
		627+	PLL V2

LCC	OBJ	LINE	SOURCE STATEMENT
830E	119930	628+	LXI D,V2
8311	CD1785	629+	CALL PLLT
8314	CD3085	630+	CALL GTHAN
8317	E601	631+	ANI 01H
8319	C2A583	632+	JNZ L301
		633	
		634	PSH EPSI
831C	117830	635+	LXI D,EPSI
831F	CD0185	636+	CALL PSHT
8322	CD048E	637	CALL PTOF
8325	CD708E	638	CALL FMUL
8328	CD248F	639	CALL SQRT
		640	PLL I1
832B	114830	641+	LXI D,I1
832E	CD1785	642+	CALL PLLT
		643	I1,GTHAN,PCRT,L301
		644+	PSH I1
8331	114830	645+	LXI D,I1
8334	CD0185	646+	CALL PSHT
		647+	PLL V1
8337	119530	648+	LXI D,V1
833A	CD1785	649+	CALL PLLT
		650+	PSH PCRT
833D	11E130	651+	LXI D,PCRT
8340	CD0185	652+	CALL PSHT
		653+	PLL V2
8343	119930	654+	LXI D,V2
8346	CD1785	655+	CALL PLLT
8349	CD3085	656+	CALL GTHAN
834C	E601	657+	ANI 01H
834E	C2A583	658+	JNZ L301
8351	3A3630	659	LDA NCOUNT
8354	3C	660	INR A
8355	323630	661	STA NCOUNT
8358	47	662	MOV B,A
8359	3ABD30	663	LDA FCOUNT
835C	B8	664	CMP B
835D	C2A583	665	JNZ L301
8360	3A3430	666	LDA RCOUNT
8363	47	667	MOV B,A
8364	3A3530	668	LDA RCOUNT
8367	B8	669	CMP B
8368	C27083	670	JNZ L308
836B	AF	671	XRA A
836C	320030	672	STA MODFLG
836F	C9	673	RET
8370	3C	674	L308: INR A
8371	323530	675	STA RCOUNT
8374	AF	676	XRA A
8375	323630	677	STA NCOUNT
8378	CDBA81	678	CALL TPULL
		679	PSH XI
837B	115830	680+	LXI D,XI
837E	CD0185	681+	CALL PSHT
		682	PSH XOF

! OR (NCOUNT+1) (FCOUNT THEN JMP L301
! FIND :EPSI!

! INCREMENT NCOUNT & COMPARE WITH FCOUNT

! IF END OF PATH CLEAR MODFLG
! AND RETURN

! ELSE INCREMENT RCOUNT & RESET
! NCOUNT

! READ PATH POINT AND
! ADD OFFSET

LOC	OBJ	LINE	SOURCE STATEMENT	
8381	111530	683+	LXI D,XOF	
8384	CD0185	684+	CALL PSHT	
8387	CD648E	685	CALL FADD	
		686	PLL XI	
838A	115830	687+	LXI D,XI	
838D	CD1785	688+	CALL PLLT	
		689	PSH YI	
8390	115C30	690+	LXI D,YI	
8393	CD0185	691+	CALL PSHT	
		692	PSH YOF	
8396	111930	693+	LXI D,YOF	
8399	CD0185	694+	CALL PSHT	
839C	CD648E	695	CALL FADD	
		696	PLL YI	
839F	115C30	697+	LXI D,YI	
83A2	CD1785	698+	CALL PLLT	
83A5	CD1384	699 L301:	CALL CONV	{CALL CONTROL ROUTINES
83A8	CD3F86	700	CALL COORD	
83AB	CD2487	701	CALL EPDS	
83AE	CD5F89	702	CALL FFD	
83B1	CD968C	703	CALL OUTPUT	
83B4	DB2A	704	IN 2AH	{CHECK MODE SWITCH INPUTS
83B6	FE00	705	CPI 00H	
83B8	CO	706	RNZ	
		707		{
83B9	FB	708	EI	{ALLOW INTERRUPT
83BA	00	709	NOP	
83BB	F3	710	DI	
		711		{
83BC	C3FC82	712	JMP REPEAT	
83BF	C9	713	RET	
		714		{
		715		{
		716		{
		717		{** SUBROUTINE RFAST **
		718		{
		719		{SEGMENT FOR REPEAT FAST MODE.
		720		{ CONTROL NORMALLY ENTERS AT LABEL
		721		{ RFAST. HOWEVER IF THE MACHINE IS
		722		{ ALREADY IN REPEAT SLOW MODE CONTROL
		723		{ ENTERS AT RFDON. THIS ALLOWS THE
		724		{ REPEAT SPEED TO BE CHANGED WITHOUT
		725		{ RESTARTING THE TRAJECTORY.
		726		{
		727		{REGISTERS AFFECTED: A,B,D,E,H,L,STATUS
		728		{
83C0	3A3430	729 RFAST:	LDA PCOUNT	{RETURN IF NO PATH IN MEMORY
83C3	47	730	MOV B,A	
83C4	AF	731	XRA A	
83C5	B8	732	CMR B	
83C6	C8	733	RZ	
83C7	CDAC82	734	CALL RSETUP	
83CA	3E03	735 RFDON:	MVI A,03H	{INDICATE MODE
83CC	D323	736	OUT 23H	
83CE	3E02	737	MVI A,02H	

LOC	OBJ	LINE	SOURCE STATEMENT	
83D0	320030	738	STA MODFLG	
83D3	3AFD30	739	LDA FFAST	{SET UP NO. OF CONTROL ROUTINE
83D6	32BD30	740	STA FCOUNT	{ CALLS BETWEEN POINTS
83D9	AF	741	XRA A	{CLEAR NCOUNT
83DA	323630	742	STA NCOUNT	
83DD	CDFC82	743	CALL REPEAT	
83E0	C9	744	RET	
		745		{
		746		{
		747		{** SUBROUTINE RSLW **
		748		{
		749		{SEGMENT FOR REPEAT SLOW MODE
		750		{
		751		{CONTROL NORMALLY ENTERS THE
		752		{ ROUTINE AT LABEL RSLW. HOWEVER
		753		{ IF THE SYSTEM IS ALREADY IN
		754		{ REPEAT FAST MODE THEN CONTROL
		755		{ ENTERS AT LABEL RSCON. THIS
		756		{ ALLOWS THE REPEAT SPEED TO BE
		757		{ CHANGED WITHOUT RESTARTING THE
		758		{ TRAJECTORY.
		759		{
		760		{REGISTERS AFFECTED: A,B,D,E,H,L,STATUS
		761		{
83E1	3A3430	762	RSLW: LDA PCOUNT	{RETURN IF NO PATH IN MEMORY
83E4	47	763	MOV B,A	
83E5	AF	764	XRA A	
83E6	B8	765	CMP B	
83E7	C8	766	RZ	
83E8	CDAC82	767	CALL RSETUP	
83E9	3E02	768	RSCON: MVI A,02H	{INDICATE MODE
83ED	D323	769	OUT 23H	
83EF	3E01	770	MVI A,01H	
83F1	320030	771	STA MODFLG	
83F4	3AFE30	772	LDA FSLW	
83F7	32BD30	773	STA FCOUNT	
83FA	CDFC82	774	CALL REPEAT	
83FD	C9	775	RET	
		776		{
		777		{
		778		{
		779		{** SUBROUTINE INIT **
		780		{
		781		{THIS ROUTINE SETS UP THE I/O
		782		{ PORT DATA DIRECTION REGISTERS
		783		{
		784		{REGISTERS AFFECTED: A
		785		{
83FE	3E0F	786	INIT: MVI A,0FH	{SET PORTS 21,22,23 FOR OUTPUT
8400	D320	787	OUT 20H	
8402	3EFF	788	MVI A,0FFH	
8404	D302	789	OUT 02H	
8406	D303	790	OUT 03H	
8408	D30A	791	OUT 0AH	
840A	3E0C	792	MVI A,0CH	

LOC	OBJ	LINE	SOURCE STATEMENT	
840C	D328	793	DUT 28H	
840E	AF	794	XRA A	{ZERO PATH POINT COUNTER
840F	323430	795	STA PCOUNT	
8412	C9	796	RET	
		797		{
		798		{
		799		{
		800		{** SUBROUTINE CONV **
		801		{
		802		{THIS SUBROUTINE READS IN THE JOYSTICK
		803		{ AND PITCH CONTROL SETTINGS AND THE
		804		{ MACHINE POSITION
		805		{
		806		{REGISTERS AFFECTED: A,D,E,H,L,STATUS
		807		{
8413	3E03	808	CONV: MVI A,03H	{LOAD A WITH JOYSTICK SLEW CONTROL
		809		{CHANNEL NUMBER
8415	CDE784	810	CALL ADCON	
8418	CD9385	811	CALL JOYSTK	{TRANSFORMS JOYSTICK VOLTAGE
		812		{ TO RANGE -1 TO +1 (RESULT ON TOS)
		813	PLL JSLEW	
8418	114030	814+	LXI D,JSLEW	
841E	CD1785	815+	CALL PLLT	
8421	3E04	816	MVI A,04H	{READ YDOT INPUT FROM JOYSTICK
8423	CDE784	817	CALL ADCON	
8426	CD9385	818	CALL JOYSTK	
		819	PLL JYDOT	
8429	113C30	820+	LXI D,JYDOT	
842C	CD1785	821+	CALL PLLT	
842F	3E05	822	MVI A,05H	{READ XDOT INPUT FROM JOYSTICK
8431	CDE784	823	CALL ADCON	
8434	CD9385	824	CALL JOYSTK	
		825	PLL JXDOT	
8437	113830	826+	LXI D,JXDOT	
843A	CD1785	827+	CALL PLLT	
843D	3E06	828	MVI A,06H	{READ BUCKET VELOCITY INPUT FROM
843F	CDE784	829	CALL ADCON	{ JOYSTICK
8442	CD9385	830	CALL JOYSTK	
		831	PLL JBKT	
8445	114430	832+	LXI D,JBKT	
8448	CD1785	833+	CALL PLLT	
844B	3E07	834	MVI A,07H	{PITCH
844D	CDE784	835	CALL ADCON	
8450	CD1C86	836	CALL SLOPE	{CALCULATE INPUT PITCH ANGLE
		837		{ FROM CONTROL KNOB VOLTAGE
		838		{
		839		{READ IN VOLTAGES FROM POTENTIOMETERS
		840		{ ON MACHINE PIVOTS AND CALCULATE ARM
		841		{ ANGLES
8453	CD5D84	842	CALL ALFIP	{INPUT ALPHA AND SUBTRACT PITCH
8456	CD9784	843	CALL BETIP	{INPUT BETA
8459	CDBF84	844	CALL DELTIP	{INPUT DELTA
845C	C9	845	RET	
		846		{
		847		{

LOC	OBJ	LINE	SOURCE STATEMENT	
		848		{** SUBROUTINE ALFIP **
		849		{
		850		{INPUTS ALPHA VOLTAGE, SCALES IT,
		851		{ ADDS OFFSET, AND SUBTRACTS PITCH
		852		{
		853		{REGISTERS AFFECTED: A,D,E,H,L,STATUS
		854		{
845D	3E00	855	ALFIP: MVI A,00H	{A=ALPHA CHANNEL NUMBER
845F	CDE784	856	CALL ADCON	
8462	320010	857	STA 1000H	{PUSH VALPHA ONTO APU STACK
8465	AF	858	XRA A	
8466	320010	859	STA 1000H	
8469	CD888E	860	CALL FLTS	{CONVERT RESULT TO 32-BIT FL. PT. FORMAT
		861	PSH MA	{PUSH SCALE FAC & MPY
846C	115580	862+	LXI D,MA	
846F	CD0185	863+	CALL PSHT	
8472	CD708E	864	CALL FMUL	
		865	PSH CA	{PUSH OFFSET AND ADD
8475	115980	866+	LXI D,CA	
8478	CD0185	867+	CALL PSHT	
847B	CD648E	868	CALL FADD	
847E	CDCA8E	869	CALL PTOF	{PULL LIFT ARM ANGLE
		870	PLL MCALFA	
8481	118030	871+	LXI D,MCALFA	
8484	CD1785	872+	CALL PLLT	
		873	PSH PITCH	{SUBTRACT PITCH
8487	119D30	874+	LXI D,PITCH	
848A	CD0185	875+	CALL PSHT	
848D	CD948E	876	CALL FSUB	
		877	PLL ALPHA	
8490	118430	878+	LXI D,ALPHA	
8493	CD1785	879+	CALL PLLT	
8496	C9	880	RET	
		881		{
		882		{
		883		{** SUBROUTINE BETIP **
		884		{
		885		{INPUTS VBETA, SCALES IT, AND ADDS
		886		{ OFFSET
		887		{
		888		{REGISTERS AFFECTED: A,D,E,H,L,STATUS
		889		{
8477	3E01	890	BETIP: MVI A,01H	{A=BETA CHANNEL NUMBER
8479	CDE784	891	CALL ADCON	
847C	320010	892	STA 1000H	{CONVERT TO 32-BIT FL. PT. FORMAT
847F	AF	893	XRA A	
84A0	320010	894	STA 1000H	
84A3	CD888E	895	CALL FLTS	
		896	PSH MB	{MPY BY SCALE FAC
84A6	115D80	897+	LXI D,MB	
84A9	CD0185	898+	CALL PSHT	
84AC	CD708E	899	CALL FMUL	
		900	PSH CB	{PUSH OFFSET AND ADD
84AF	116180	901+	LXI D,CB	
84B2	CD0185	902+	CALL PSHT	

LOC	OBJ	LINE	SOURCE STATEMENT
84B5	CD646E	903	CALL FADD
		904	PLL BETA
84B8	118E30	905+	LXI D,BETA
84BB	CD1785	906+	CALL PLLT
84BE	C9	907	RET
		908	
		909	
		910	
		911	
		912	
		913	
		914	
		915	
		916	
		917	
84BF	3E02	918	DELTP: MVI A,02H
84C1	CDE784	919	CALL ADCDN
84C4	320010	920	STA 1000H
84C7	AF	921	XRA A
84C8	320010	922	STA 1000H
84CB	CD888E	923	CALL FLTS
		924	FSH MD
84CE	116580	925+	LXI D,MD
84D1	CD0185	926+	CALL PSHT
84D4	CD708E	927	CALL FMUL
		928	PSH CD
84D7	116980	929+	LXI D,CD
84DA	CD0185	930+	CALL PSHT
84DD	CD646E	931	CALL FADD
		932	PLL DELTA
84E0	118C30	933+	LXI D,DELTA
84E3	CD1785	934+	CALL PLLT
84E6	C9	935	RET
		936	
		937	
		938	
		939	
		940	
		941	
		942	
		943	
		944	
		945	
		946	
		947	
84E7	D32B	948	ADCON: OUT 2BH
84E9	C608	949	ADI 08H
84EB	D32B	950	OUT 2BH
84ED	AF	951	XRA A
84EE	D32B	952	OUT 2BH
84F0	211100	953	LXI H,0011H
84F3	CD9787	954	CALL PAUSE
84F6	3E10	955	MVI A,10H
84F8	D32B	956	OUT 2BH
84FA	00	957	NOP

```

|
|
|** SUBROUTINE DELTIP **
|
|INPUTS VDELTA, SCALES IT, AND
| ADDS OFFSET
|
|REGISTERS AFFECTED: A,D,E,H,L,STATUS
|
|
|CONVERT INPUT TO 32-BIT FL. PT.
|
|MULTIPLY BY SCALE FACTOR
|
|ADD OFFSET
|
|
|
|** SUBROUTINE ADCDN **
|
|THIS ROUTINE OPERATES THE
| ANALOGUE TO DIGITAL CONVERTER.
| THE CHANNEL NUMBER IS IN THE
| A REGISTER ON CALLING AND
| THE RESULT AT RETURN
|
|REGISTERS AFFECTED: A,H,L,STATUS
|
|OUTPUT CHANNEL NUMBER
|LATCH CHANNEL NUMBER
|CLEAR CONTROL WORD
|SET DELAY
|CALL DELAY ROUTINE
|SET TRISTATE OUTPUT
    
```


LDC	OBJ	LINE	SOURCE STATEMENT
	84FB 00	958	NOP
	84FC 00	959	NOP
	84FD 00	960	NOP
	84FE DB29	961	IN 29H
	8500 C9	962	RET
		963	
		964	
		965	
		966	
		967	
		968	
		969	
		970	
		971	
		972	
		973	
		974	
		975	
		976	
	8501 F5	977	PSHT: PUSH PSW
	8502 1A	978	LDAX D
	8503 320010	979	STA 1000H
	8506 13	980	INX D
	8507 1A	981	LDAX D
	8508 320010	982	STA 1000H
	8509 13	983	INX D
	850C 1A	984	LDAX D
	850D 320010	985	STA 1000H
	8510 13	986	INX D
	8511 1A	987	LDAX D
	8512 320010	988	STA 1000H
	8515 F1	989	POP PSW
	8516 C9	990	RET
		991	
		992	
		993	
		994	
		995	
		996	
		997	
		998	
		999	
		1000	
		1001	
	8517 F5	1002	PLLT: PUSH PSW
	8518 13	1003	INX D
	8519 13	1004	INX D
	851A 13	1005	INX D
	851B 3A0010	1006	LDA 1000H
	851E 12	1007	STAX D
	851F 1B	1008	DCX D
	8520 3A0010	1009	LDA 1000H
	8523 12	1010	STAX D
	8524 1B	1011	DCX D
	8525 3A0010	1012	LDA 1000H

{READ RESULT

{
 {
 {** SUBROUTINE PSHT **
 {
 {PUSHES A 32-BIT FL. PT. VARIABLE
 { ONTO THE APU STACK.
 { DE CONTAINS THE ADDRESS
 { OF THE LS BYTE OF THE
 { OPERAND ON CALLING
 { AND OF THE MS BYTE AT
 { RETURN
 {
 {REGISTERS AFFECTED: D,E
 {

{LD ACC WITH LS BYTE
 {PUSH ACC TO APU
 {INCREMENT DATA POINTER

{
 {
 {** SUBROUTINE PLLT **
 {
 {PULLS A 32-BIT FL. PT. VARIABLE
 { FROM THE APU STACK
 { DE CONTAINS ADDRESS OF LS
 { BYTE ON CALLING AND MS
 { BYTE AT RETURN
 {
 {REGISTERS AFFECTED: D,E

LOC	OBJ	LINE	SOURCE STATEMENT
8528	12	1013	STAX D
8529	1B	1014	DCX D
852A	3A0010	1015	LDA 1000H
852D	12	1016	STAX D
852E	F1	1017	POP PSW
852F	C9	1018	RET
		1019	
		1020	
		1021	*** SET OF SUBROUTINES FOR EVALUATING
		1022	OPERATORS IN CONDITIONAL JUMPS **
		1023	
		1024	EACH SUBROUTINE RETURNS 01H IN THE
		1025	ACCUMULATOR IF THE CONDITION IS VALID
		1026	
		1027	REGISTERS AFFECTED: A,D,E,STATUS
		1028	
8530	CD6D85	1029	GTHAN: CALL EQUALS
		1030	
		1031	
8533	E601	1032	ANI 01H
8535	CA3A85	1033	JZ L2
8538	AF	1034	XRA A
8539	C9	1035	RET
853A	3A9030	1036	L2: LDA STATUS
853D	E640	1037	ANI 40H
853F	CA4485	1038	JZ L3
8542	AF	1039	XRA A
8543	C9	1040	RET
8544	3E01	1041	L3: MVI A,01H
8546	C9	1042	RET
		1043	
		1044	
8547	CD6D85	1045	LTHAN: CALL EQUALS
854A	E601	1046	ANI 01H
854C	CA5185	1047	JZ L4
854F	AF	1048	XRA A
8550	C9	1049	RET
8551	3A9030	1050	L4: LDA STATUS
8554	E640	1051	ANI 40H
8556	C25B85	1052	JNZ L5
8559	AF	1053	XRA A
855A	C9	1054	RET
855B	3E01	1055	L5: MVI A,01H
855D	C9	1056	RET
		1057	
		1058	
855E	CD4785	1059	GEQUAL: CALL LTHAN
8561	2F	1060	CMA
8562	C9	1061	RET
		1062	
		1063	
8563	CD3085	1064	LEQUAL: CALL GTHAN
8566	2F	1065	CMA
8567	C9	1066	RET
		1067	

LOC	OBJ	LINE	SOURCE STATEMENT
8568	CD6DS5	1068	NEQUAL: CALL EQUALS
856B	2F	1069	CMA
856C	C9	1070	RET
		1071	
		1072	
		1073	EQUALS: PSH V1
856D	119530	1074+	LXI D,V1
8570	CD0185	1075+	CALL PSHT
		1076	PSH V2
8573	119930	1077+	LXI D,V2
8576	CD0185	1078+	CALL PSHT
8579	CD948E	1079	CALL FSUB
857C	3A0011	1080 L6:	LDA 1100H
857F	E680	1081	ANI 80H
8581	C27C85	1082	JNZ L6
8584	3A0011	1083	LDA 1100H
8587	329030	1084	STA STATUS
858A	E620	1085	ANI 20H
858C	C29085	1086	JNZ L7
858F	C9	1087	RET
		1088	
8590	3E01	1089 L7:	MVI A,01H
8592	C9	1090	RET
		1091	
		1092	
		1093	
		1094	
		1095	
		1096	
		1097	
		1098	
		1099	
		1100	
		1101	
		1102	
		1103	
8593	320010	1104 JOYSTK:	STA 1000H
8596	AF	1105	XRA A
8597	320010	1106	STA 1000H
859A	CD888E	1107	CALL FLTS
		1108	PLL I1
859D	114830	1109+	LXI D,I1
85A0	CD1785	1110+	CALL PLLT
		1111	IFF I1,GTHAN,H87,L50
		1112+	PSH I1
85A3	114830	1113+	LXI D,I1
85A6	CD0185	1114+	CALL PSHT
		1115+	PLL V1
85A9	119530	1116+	LXI D,V1
85AC	CD1785	1117+	CALL PLLT
		1118+	PSH H87
85AF	117580	1119+	LXI D,H87
85B2	CD0185	1120+	CALL PSHT
		1121+	PLL V2
85B5	119930	1122+	LXI D,V2

```

;
;
;SUBTRACT V2 FROM V1
;
;
;WAIT TILL APU NOT BUSY
;
;TRANSFER APU STATUS TO CORE
;CHECK ZERO BIT
;RETURN 00 IN A REG INDICATING INEQUALTY
;
;RETURN 01 IN A REG INDICATING EQUALITY
;
;
;
; ** SUBROUTINE JOYSTK **
;
;JOYSTICK VOLTAGE IS IN 'A' REGISTER
; ON CALLING, THE SUBROUTINE TRANS-
; FORMS IT TO THE RANGE -1 TO +1 AND
; LEAVES THE RESULT ON THE TOS
;
;REGISTERS AFFECTED A,D,E,STATUS
;
;CONVERT JOYSTICK VOLTAGE TO 32 BIT
; FORMAT
;
; IF JOYSTICK VOLTAGE > 87H THEN L50

```

LOC	OBJ	LINE	SOURCE STATEMENT
8588	CD1785	1123+	CALL PLLT
858B	CD3085	1124+	CALL GTHAN
858E	E601	1125+	ANI 01H
85C0	C2EA85	1126+	JNZ L50
		1127	IFF I1,LTHAN,H79;L51
		1128+	PSH I1
85C3	114830	1129+	LXI D,I1
85C6	CD0185	1130+	CALL PSHT
		1131+	PLL V1
85C9	119530	1132+	LXI D,V1
85CC	CD1785	1133+	CALL PLLT
		1134+	PSH H79
85CF	117980	1135+	LXI D,H79
85D2	CD0185	1136+	CALL PSHT
		1137+	PLL V2
85D5	119930	1138+	LXI D,V2
85D8	CD1785	1139+	CALL PLLT
85DB	CD4785	1140+	CALL LTHAN
85DE	E601	1141+	ANI 01H
85E0	C20386	1142+	JNZ L51
		1143	PSH ZERO
85E3	117D80	1144+	LXI D,ZERO
85E6	CD0185	1145+	CALL PSHT
85E9	C9	1146	RET
		1147 L50:	PSH I1
85EA	114830	1148+	LXI D,I1
85ED	CD0185	1149+	CALL PSHT
		1150	PSH H87
85F0	117580	1151+	LXI D,H87
85F3	CD0185	1152+	CALL PSHT
85F6	CD948E	1153	CALL FSUB
		1154	PSH D14
85F9	11C580	1155+	LXI D,D14
85FC	CD0185	1156+	CALL PSHT
85FF	CDA08E	1157	CALL FDIV
8602	C9	1158	RET
		1159 L51:	PSH I1
8603	114830	1160+	LXI D,I1
8606	CD0185	1161+	CALL PSHT
		1162	PSH H79
8609	117980	1163+	LXI D,H79
860C	CD0185	1164+	CALL PSHT
860F	CD948E	1165	CALL FSUB
		1166	PSH D14
8612	11C580	1167+	LXI D,D14
8615	CD0185	1168+	CALL PSHT
8618	CDA08E	1169	CALL FDIV
861B	C9	1170	RET
		1171	
		1172	
		1173	** SUBROUTINE SLOPE **
		1174	
		1175	THIS ROUTINE CALCULATES THE
		1176	PITCH ANGLE FROM THE PITCH
		1177	CONTROL VOLTAGE. THE VOLTAGE

LOC	OBJ	LINE	SOURCE STATEMENT	
		1178		{ IS IN THE 'A' REGISTER ON CALLING
		1179		{ AND THE RESULT ON THE TOS AT RETURN
		1180		{
		1181		{REGISTERS AFFECTED: A,D,E
		1182		{
861C	320010	1183	SLOPE: STA 1000H	{CONVERT VOLTAGE TO 32 BIT FORMAT
861F	AF	1184	XRA A	
8620	320010	1185	STA 1000H	
8623	CD888E	1186	CALL FLTS	
		1187	PSH CNST13	{PSH 8.18 E-03
8626	118580	1188+	LXI D,CNST13	
8629	CD0185	1189+	CALL PSHT	
862C	CD708E	1190	CALL FMUL	
		1191	PSH CNST14	{PSH -1.047
862F	118980	1192+	LXI D,CNST14	
8632	CD0185	1193+	CALL PSHT	
8635	CD648E	1194	CALL FADD	
		1195	PLL PITCH	
8638	119D30	1196+	LXI D,PITCH	
863B	CD1785	1197+	CALL PLLT	
863E	C9	1198	RET	
		1199		{
		1200		{
		1201		{** SUBROUTINE COORD **
		1202		{
		1203		{CALCULATES OUTPUT COORDINATES XO,
		1204		{ YO, AND PSIO, FROM ALPHA, BETA,
		1205		{ AND DELTA
		1206		{
		1207		{REGISTERS AFFECTED: D,E
		1208		{
		1209	COORD: PSH ALPHA	{CALCULATE X-COORDINATE OF BUCKET PIVOT
863F	118430	1210+	LXI D,ALPHA	
8642	CD0185	1211+	CALL PSHT	
8645	CDE88E	1212	CALL SIN	{ IN USER DEFINED AXES
		1213	PSH LA	{XO=L*SIN(ALPHA)+R*SIN(ALPHA+BETA-PI)
8648	116D80	1214+	LXI D,LA	
864B	CD0185	1215+	CALL PSHT	
864E	CD708E	1216	CALL FMUL	
		1217	PLL I1	
8651	114830	1218+	LXI D,I1	
8654	CD1785	1219+	CALL PLLT	
		1220	PSH ALPHA	
8657	118430	1221+	LXI D,ALPHA	
865A	CD0185	1222+	CALL PSHT	
		1223	PSH BETA	
865D	118830	1224+	LXI D,BETA	
8660	CD0185	1225+	CALL PSHT	
8663	CD648E	1226	CALL FADD	
8666	CDDC8E	1227	CALL PUPI	
8669	CD948E	1228	CALL FSUB	
866C	CDE88E	1229	CALL SIN	
		1230	PSH RA	
866F	117180	1231+	LXI D,RA	
8672	CD0185	1232+	CALL PSHT	

LOC	OBJ	LINE	SOURCE STATEMENT
8675	CD708E	1233	CALL FMUL
		1234	PSH I1
8678	118830	1235+	LXI D,I1
8678	CD0185	1236+	CALL PSHT
867E	CD648E	1237	CALL FADD
		1238	PLL XO
8681	116430	1239+	LXI D,XO
8684	CD1785	1240+	CALL PLLT
		1241	PSH ALPHA
8687	118430	1242+	LXI D,ALPHA
868A	CD0185	1243+	CALL PSHT
868D	CD008F	1244	CALL COS
8690	CD7C8E	1245	CALL CHSF
		1246	PSH LA
8693	116D80	1247+	LXI D,LA
8696	CD0185	1248+	CALL PSHT
8699	CD708E	1249	CALL FMUL
		1250	PLL I1
869C	114830	1251+	LXI D,I1
869F	CD1785	1252+	CALL PLLT
		1253	PSH ALPHA
86A2	118430	1254+	LXI D,ALPHA
86A5	CD0185	1255+	CALL PSHT
		1256	PSH BETA
86A8	118830	1257+	LXI D,BETA
86AB	CD0185	1258+	CALL PSHT
86AE	CD648E	1259	CALL FADD
86B1	CDDC8E	1260	CALL PUPI
86B4	CD948E	1261	CALL FSUB
86B7	CD008F	1262	CALL COS
		1263	PSH RA
86BA	117180	1264+	LXI D,RA
86BD	CD0185	1265+	CALL PSHT
86C0	CD708E	1266	CALL FMUL
		1267	PSH I1
86C3	114830	1268+	LXI D,I1
86C6	CD0185	1269+	CALL PSHT
86C9	CD188F	1270	CALL XCHF
86CC	CD948E	1271	CALL FSUB
		1272	PLL YO
86CF	116830	1273+	LXI D,YO
86D2	CD1785	1274+	CALL PLLT
		1275	PSH DELTA
86D5	118C30	1276+	LXI D,DELTA
86D8	CD0185	1277+	CALL PSHT
86DB	CDCA8E	1278	CALL PTOF
86DE	CDCA8E	1279	CALL PTOF
86E1	CD708E	1280	CALL FMUL
		1281	PSH GC2
86E4	119D80	1282+	LXI D,GC2
86E7	CD0185	1283+	CALL PSHT
86EA	CD708E	1284	CALL FMUL
86ED	CD188F	1285	CALL XCHF
		1286	PSH GC1
86F0	119980	1287+	LXI D,GC1

!CALCULATE Y COORDINATE

!YO=-L*COS(ALPHA)-R*COS(ALPHA+BETA-PI)

!CALCULATE PSI

!CALCULATE GAMMA

! X=DELTA

! GAMMA=GC0+(GC1*X)+(GC2*X*X)

LOC	OBJ	LINE	SOURCE STATEMENT
86F3	CD0185	1288+	CALL PSHT
86F6	CD708E	1289	CALL FMUL
86F9	CD648E	1290	CALL FADD
		1291	PSH GCO
86FC	119580	1292+	LXI D,GCO
86FF	CD0185	1293+	CALL PSHT
8702	CD648E	1294	CALL FADD
		1295	PSH BETA
8705	118830	1296+	LXI D,BETA
8708	CD0185	1297+	CALL PSHT
870B	CD648E	1298	CALL FADD
		1299	PSH ALPHA
870E	118430	1300+	LXI D,ALPHA
8711	CD0185	1301+	CALL PSHT
8714	CD648E	1302	CALL FADD
8717	CDDC8E	1303	CALL PUPI
871A	CD948E	1304	CALL FSUB
		1305	PLL PSIO
871D	116C30	1306+	LXI D,PSIO
8720	CD1785	1307+	CALL PLLT
8723	C9	1308	RET
		1309	
		1310	
		1311	! ** SUBROUTINE EPOS **
		1312	!
		1313	! CALCULATES POSITIONAL ERRORS
		1314	! EX, EY, EPSI AND ETA. THE
		1315	! ROUTINE ALSO CONTAINS A DELAY
		1316	! SEGMENT TO VARY THE LOOP EXECUTION
		1317	! TIME FOR EXPERIMENTAL PURPOSES
		1318	!
		1319	! REGISTERS AFFECTED: A,D,E,H,L,STATUS
		1320	!
		1321	EPOS: PSH XI
8724	115830	1322+	LXI D,XI
8727	CD0185	1323+	CALL PSHT
		1324	PSH XO
872A	116430	1325+	LXI D,XO
872D	CD0185	1326+	CALL PSHT
8730	CD948E	1327	CALL FSUB
		1328	PLL EX
8733	117030	1329+	LXI D,EX
8736	CD1785	1330+	CALL PLLT
		1331	PSH YI
8739	115C30	1332+	LXI D,YI
873C	CD0185	1333+	CALL PSHT
		1334	PSH YO
873F	116830	1335+	LXI D,YO
8742	CD0185	1336+	CALL PSHT
8745	CD948E	1337	CALL FSUB
		1338	PLL EY
8748	117430	1339+	LXI D,EY
874B	CD1785	1340+	CALL PLLT
		1341	PSH PSII
874E	116030	1342+	LXI D,PSII

LOC	OBJ	LINE	SOURCE STATEMENT
8751	CD0185	1343+	CALL PSHT
		1344	PSH PSIO
8754	116C30	1345+	LXI D,PSIO
8757	CD0185	1346+	CALL PSHT
875A	CD946E	1347	CALL FSUB
		1348	PLL EPSI
875D	117830	1349+	LXI D,EPSI
8760	CD1785	1350+	CALL PLLT
		1351	PSH EX
			!CALCULATE ETA=SQRT(EX**2+EY**2)
8763	117030	1352+	LXI D,EX
8766	CD0185	1353+	CALL PSHT
8769	CDC48E	1354	CALL PTOF
876C	CD708E	1355	CALL FMUL
			PSH EY
876F	117430	1357+	LXI D,EY
8772	CD0185	1358+	CALL PSHT
8775	CDC48E	1359	CALL PTOF
8778	CD708E	1360	CALL FMUL
877B	CD648E	1361	CALL FADD
877E	CD248F	1362	CALL SQRT
		1363	PLL ETA
8781	117C30	1364+	LXI D,ETA
8784	CD1785	1365+	CALL PLLT
		1366	
			!TIMING SEGMENT
8787	3A3730	1367	LDA TFLAG
878A	2F	1368	CMA
878B	D308	1369	OUT OSH
878D	323730	1370	STA TFLAG
8790	2AFF30	1371	LHLD DELAY
8793	CD9787	1372	CALL PAUSE
8796	C9	1373	RET
		1374	!
		1375	!
		1376	!
		1377	! ** SUBROUTINE PAUSE **
		1378	!
		1379	! SUBROUTINE FOR DELAY DECREMENTS
		1380	! INPUT IN HL REGISTER UNTIL ZERO
		1381	!
		1382	! REGISTERS AFFECTED: A,H,L,STATUS
		1383	!
8797	2B	1384	PAUSE: DCX H
8798	7C	1385	MOV A,H
8799	85	1386	ORA L
879A	C29787	1387	JNZ PAUSE
879D	C9	1388	RET
		1389	!
		1390	!
		1391	!
		1392	! ** SUBROUTINE SETEC **
		1393	!
		1394	! CALCULATES ECRIT =
		1395	! ECRIT*(1+SQRT(CXDOT**2+CYDOT**2))
		1396	!
		1397	! REGISTERS AFFECTED: D,E

LDC	OBJ	LINE	SOURCE	STATEMENT
		1398		{
		1399	SETEC:	{
879E	115030	1400+	PSH	CXDOT
87A1	CD0185	1401+	LXI	D,CXDOT
87A4	CD248E	1402	CALL	PSHT
87A7	CD708E	1403	CALL	PTOF
		1404	CALL	FMUL
		1405+	PSH	CYDOT
87AA	115430	1406+	LXI	D,CYDOT
87AD	CD0185	1407	CALL	PSHT
87B0	CD248E	1408	CALL	PTOF
87B3	CD708E	1409	CALL	FMUL
87B6	CD648E	1410	CALL	FADD
87B9	CD248F	1411	CALL	SQRT
		1412+	PSH	ONE
87BC	118180	1413+	LXI	D,ONE
87BF	CD0185	1414	CALL	PSHT
87C2	CD648E	1415	CALL	FADD
		1416+	PSH	ECHIN
87C5	11E930	1417+	LXI	D,ECHIN
87C8	CD0185	1418	CALL	PSHT
87CB	CD708E	1419	CALL	FMUL
		1420+	PLL	ECRIT
87CE	11EE30	1421+	LXI	D,ECRIT
87D1	CD1785	1422	CALL	PLLT
87D4	C9	1423	RET	{
		1424		{
		1425		{
		1426		{** SUBROUTINE IP1 **
		1427		{
		1428		{IF INPUT BUCKET VELOCITY IS NON-ZERO
		1429		{ THEN PSII=PSIO
		1430		{ IF JXDOT OR JYDOT HAS CHANGED SIGNIF-
		1431		{ ICANTLY OR BOTH ARE EQUAL TO ZERO
		1432		{ THEN UPDATE CXDOT AND CYDOT AND SET
		1433		{ TARGET POSITION TO CURRENT OUTPUT
		1434		{ POSITION
		1435		{
		1436		{REGISTERS AFFECTED: A,D,E,STATUS
		1437		{
		1438	IP1:	{
		1439+	IFF	JBKT,EQUALS,ZERO,L21
		1440+	PSH	JBKT
87D5	114430	1441+	LXI	D,JBKT
87D8	CD0185	1442+	CALL	PSHT
		1443+	PLL	V1
87DB	119E30	1444+	LXI	D,V1
87DE	CD1785	1445+	CALL	PLLT
		1446+	PSH	ZERO
87E1	117D80	1447+	LXI	D,ZERO
87E4	CD0185	1448+	CALL	PSHT
		1449+	PLL	V2
87E7	119930	1450+	LXI	D,V2
87EA	CD1785	1451+	CALL	PLLT
87ED	CD6D85	1452+	CALL	EQUALS
87F0	E601		ANI	O1H

LOC	OBJ	LINE	SOURCE STATEMENT
87F2	C20188	1453+	JNZ L21
		1454	PSH PS10
			!SET PS11=PS10
87F5	116C30	1455+	LXI D,PS10
87F8	CD0185	1456+	CALL PSHT
		1457	PLL PS11
87F9	116030	1458+	LXI D,PS11
87FE	CD1785	1459+	CALL PLLT
		1460 L21:	PSH JXDOT
			!CALCULATE DIFFERENCE BETWEEN JXDOT
8801	113830	1461+	LXI D,JXDOT
8804	CD0185	1462+	CALL PSHT
		1463	PSH CXDOT
			! AND CXDOT
8807	115030	1464+	LXI D,CXDOT
880A	CD0185	1465+	CALL PSHT
880D	CD948E	1466	CALL FSUB
8810	CD48E	1467	CALL PTOF
8813	CD708E	1468	CALL FMUL
8816	CD248F	1469	CALL SQRT
		1470	PLL I1
8819	114830	1471+	LXI D,I1
881C	CD1785	1472+	CALL PLLT
		1473	IFF I1,LEQUAL,CNST10,L22
			!(CNST10=CRITICAL VALUE OF DIFFERENCE)
		1474+	PSH I1
881F	114830	1475+	LXI D,I1
8822	CD0185	1476+	CALL PSHT
		1477+	PLL V1
8825	119530	1478+	LXI D,V1
8828	CD1785	1479+	CALL PLLT
		1480+	PSH CNST10
882B	11ED30	1481+	LXI D,CNST10
882E	CD0185	1482+	CALL PSHT
		1483+	PLL V2
8831	119930	1484+	LXI D,V2
8834	CD1785	1485+	CALL PLLT
8837	CD6385	1486+	CALL LEQUAL
883A	E601	1487+	ANI 01H
883C	C24288	1488+	JNZ L22
883F	C3C588	1489	JMP L26
		1490 L22:	PSH JYDOT
			!CALCULATE DIFFERENCE BETWEEN JYDOT
8842	113C30	1491+	LXI D,JYDOT
8845	CD0185	1492+	CALL PSHT
		1493	PSH CYDOT
			! AND CYDOT
8848	115430	1494+	LXI D,CYDOT
884B	CD0185	1495+	CALL PSHT
884E	CD948E	1496	CALL FSUB
8851	CD48E	1497	CALL PTOF
8854	CD708E	1498	CALL FMUL
8857	CD248F	1499	CALL SQRT
		1500	PLL I1
885A	114830	1501+	LXI D,I1
885D	CD1785	1502+	CALL PLLT
		1503	IFF I1,LEQUAL,CNST10,L23
		1504+	PSH I1
8860	114830	1505+	LXI D,I1
8863	CD0185	1506+	CALL PSHT
		1507+	PLL V1

LOC	OBJ	LINE	SOURCE STATEMENT
8866	119530	1508+	LXI D,V1
8867	CD1785	1509+	CALL PLLT
		1510+	PSH CNST10
886C	11ED30	1511+	LXI D,CNST10
886F	CD0185	1512+	CALL PSHT
		1513+	PLL V2
8872	119930	1514+	LXI D,V2
8875	CD1785	1515+	CALL PLLT
8878	CD6385	1516+	CALL LEQUAL
887B	E601	1517+	ANI 01H
887D	C28388	1518+	JNZ L23
8880	C3C588	1519	JMP L26
		1520 L23:	IFF JYDOT,EQUALS,ZERO,L24
		1521+	PSH JYDOT
8883	113C30	1522+	LXI D,JYDOT
8886	CD0185	1523+	CALL PSHT
		1524+	PLL V1
8889	119530	1525+	LXI D,V1
888C	CD1785	1526+	CALL PLLT
		1527+	PSH ZERO
888F	117D80	1528+	LXI D,ZERO
8892	CD0185	1529+	CALL PSHT
		1530+	PLL V2
8895	119930	1531+	LXI D,V2
8898	CD1785	1532+	CALL PLLT
889B	CD6D85	1533+	CALL EQUALS
889E	E601	1534+	ANI 01H
88A0	C2A488	1535+	JNZ L24
88A3	C9	1536	RET
		1537 L24:	IFF JXDOT,EQUALS,ZERO,L26
		1538+	PSH JXDOT
88A4	113830	1539+	LXI D,JXDOT
88A7	CD0185	1540+	CALL PSHT
		1541+	PLL V1
88AA	119530	1542+	LXI D,V1
88AD	CD1785	1543+	CALL PLLT
		1544+	PSH ZERO
88B0	117D80	1545+	LXI D,ZERO
88B3	CD0185	1546+	CALL PSHT
		1547+	PLL V2
88B6	119930	1548+	LXI D,V2
88B9	CD1785	1549+	CALL PLLT
88BC	CD6D85	1550+	CALL EQUALS
88BF	E601	1551+	ANI 01H
88C1	C2C588	1552+	JNZ L26
88C4	C9	1553	RET
		1554 L26:	PSH X0
88C5	116430	1555+	LXI D,X0
88C8	CD0185	1556+	CALL PSHT
		1557	PLL XI
88CB	115830	1558+	LXI D,XI
88CE	CD1785	1559+	CALL PLLT
		1560	PSH Y0
88D1	116830	1561+	LXI D,Y0
88D4	CD0185	1562+	CALL PSHT

LOC	OBJ	LINE	SOURCE STATEMENT
		1563	PLL YI
88D7	115C30	1564+	LXI D,YI
88DA	CD1785	1565+	CALL PLLT
		1566	PSH PSIO
88DD	116C30	1567+	LXI D,PSIO
82E0	CD0185	1568+	CALL PSHT
		1569	PLL PSII
8EE3	116030	1570+	LXI D,PSII
88E6	CD1785	1571+	CALL PLLT
		1572	PSH JXDOT
8EE9	113830	1573+	LXI D,JXDOT
8EEC	CD0185	1574+	CALL PSHT
		1575	PLL CXDOT
8EEF	115030	1576+	LXI D,CXDOT
8EF2	CD1785	1577+	CALL PLLT
		1578	PSH JYDOT
8EF5	113C30	1579+	LXI D,JYDOT
8EF8	CD0185	1580+	CALL PSHT
		1581	PLL CYDOT
8EFB	115430	1582+	LXI D,CYDOT
8EFE	CD1785	1583+	CALL PLLT
8901	C9	1584	RET
		1585	
		1586	
		1587	*** SUBROUTINE IP2 **
		1588	
		1589	! IF POSITION ERROR IS BELOW THRESHOLD
		1590	! VALUE ECRIT THEN UPDATE XI AND YI
		1591	! ELSE RETURN
		1592	
		1593	! REGISTERS AFFECTED: A,D,E,S
		1594	
		1595 IP2:	! IF ETA>ECRIT THEN CONTINUE ELSE
		1596+	PSH ETA
8902	117C30	1597+	LXI D,ETA
8905	CD0185	1598+	CALL PSHT
		1599+	PLL V1
8908	119530	1600+	LXI D,V1
890B	CD1785	1601+	CALL PLLT
		1602+	PSH ECRIT
890E	118E30	1603+	LXI D,ECRIT
8911	CD0185	1604+	CALL PSHT
		1605+	PLL V2
8914	119930	1606+	LXI D,V2
8917	CD1785	1607+	CALL PLLT
891A	CD3065	1608+	CALL GTHAN
891D	E601	1609+	ANI 01H
891F	C25E89	1610+	JNZ L32
		1611	PSH CXDOT
8922	115030	1612+	LXI D,CXDOT
8925	CD0185	1613+	CALL PSHT
		1614	PSH CNST11
8928	11F130	1615+	LXI D,CNST11
892B	CD0185	1616+	CALL PSHT
892E	CD708E	1617	CALL FMUL

LOC	OBJ	LINE	SOURCE STATEMENT
		1618	PSH XI
8931	115830	1619+	LXI D,XI
8934	CD0185	1620+	CALL PSHT
8937	CD648E	1621	CALL FADD
		1622	PLL XI
893A	115830	1623+	LXI D,XI
893D	CD1785	1624+	CALL PLLT
		1625	PSH CYDOT
8940	115430	1626+	LXI D,CYDOT
8943	CD0185	1627+	CALL PSHT
		1628	PSH CNST11
8946	11F130	1629+	LXI D,CNST11
8949	CD0185	1630+	CALL PSHT
894C	CD708E	1631	CALL FMUL
		1632	PSH YI
894F	115C30	1633+	LXI D,YI
8952	CD0185	1634+	CALL PSHT
8955	CD648E	1635	CALL FADD
		1636	PLL YI
8958	115C30	1637+	LXI D,YI
895B	CD1785	1638+	CALL PLLT
895E	C9	1639 L32:	RET
		1640	
		1641	
		1642	*** SUBROUTINE FFD **
		1643	
		1644	!CALCULATES VALVE OPENINGS,
		1645	! RESULTS IN RANGE -1 TO +1
		1646	!
		1647	!REGISTERS AFFECTED: A,D,E,STATUS
		1648	!
		1649 FFD:	!SET SLEW VOLTAGE
895F	114030	1650+	PSH JSLEW
8962	CD0185	1651+	LXI D,JSLEW
		1652	CALL PSHT
8965	11A930	1653+	PLL VVSLEW
8968	CD1785	1654+	LXI D,VVSLEW
		1655	CALL PLLT
896B	3A0030	1656	LDA MODFLG
896E	FE00	1657	CPI 00H
8970	C2BF89	1658	JNZ L43
		1659	
		1660	
		1661	IFF JXDOT,EQUALS,ZERO,L44
		1662+	PSH JXDOT
8973	113830	1663+	LXI D,JXDOT
8976	CD0185	1664+	CALL PSHT
		1665+	PLL V1
8979	119530	1666+	LXI D,V1
897C	CD1785	1667+	CALL PLLT
		1668+	PSH ZERO
897F	117D80	1669+	LXI D,ZERO
8982	CD0185	1670+	CALL PSHT
		1671+	PLL V2
8985	119930	1672+	LXI D,V2

LOC	OBJ	LINE	SOURCE STATEMENT
8988	CD1785	1673+	CALL PLLT
898B	CD6D85	1674+	CALL EQUALS
898E	E601	1675+	ANI 01H
8990	C29689	1676+	JNZ L44
8993	C3BF89	1677	JMP L43
		1678 L44:	IFF JYDOT,EQUALS,ZERO,L46
		1679+	PSH JYDOT
8996	113C30	1680+	LXI D,JYDOT
8999	CD0185	1681+	CALL PSHT
		1682+	PLL V1
899C	119530	1683+	LXI D,V1
899F	CD1785	1684+	CALL PLLT
		1685+	PSH ZERO
89A2	117D80	1686+	LXI D,ZERO
89A5	CD0185	1687+	CALL PSHT
		1688+	PLL V2
89A8	119930	1689+	LXI D,V2
89AB	CD1785	1690+	CALL PLLT
89AE	CD6D85	1691+	CALL EQUALS
89B1	E601	1692+	ANI 01H
89B3	C2B989	1693+	JNZ L46
89B6	C3BF89	1694	JMP L43
89B9	CD808C	1695 L46:	CALL FREEZE
89BC	C3BB8A	1696	JMP L47
		1697 L43:	PSH XI
89BF	115830	1698+	LXI D,XI
89C2	CD0185	1699+	CALL PSHT
89C5	CDC48E	1700	CALL PTOF
89C8	CD708E	1701	CALL FMUL
		1702	PSH YI
89CB	115C30	1703+	LXI D,YI
89CE	CD0185	1704+	CALL PSHT
89D1	CDC48E	1705	CALL PTOF
89D4	CD708E	1706	CALL FMUL
89D7	CD648E	1707	CALL FADD
89DA	CD248F	1708	CALL SQRT
		1709	PLL DX
89DD	110130	1710+	LXI D,DX
89E0	CD1785	1711+	CALL PLLT
		1712	
		1713	PSH CNST1
89E3	11A180	1714+	LXI D,CNST1
89E6	CD0185	1715+	CALL PSHT
		1716	PSH DX
89E9	110130	1717+	LXI D,DX
89EC	CD0185	1718+	CALL PSHT
89EF	CDC48E	1719	CALL PTOF
89F2	CD708E	1720	CALL FMUL
89F5	CD948E	1721	CALL FSUB
		1722	PSH CNST2
89F8	11A580	1723+	LXI D,CNST2
89FB	CD0185	1724+	CALL PSHT
89FE	CDA08E	1725	CALL FDIV
8A01	CD0C8F	1726	CALL ACOS
		1727	PLL BI

! BI=ACOS((LA**2+RA**2-DX**2)/
! (2*LA*RA))

LOC	OBJ	LINE	SOURCE	STATEMENT
8A04	110930	1728+	LXI	D,BI
8A07	CD1785	1729+	CALL	PLLT
		1730		
		1731	PSH	CNST3
8A0A	11A980	1732+	LXI	D,CNST3
8A0D	CD0185	1733+	CALL	PSHT
		1734	PSH	DX
8A10	110130	1735+	LXI	D,DX
8A13	CD0185	1736+	CALL	PSHT
8A16	CDC48E	1737	CALL	PTOF
8A19	CD708E	1738	CALL	FMUL
8A1C	CD648E	1739	CALL	FADD
		1740	PSH	DX
8A1F	110130	1741+	LXI	D,DX
8A22	CD0185	1742+	CALL	PSHT
		1743	PSH	CNST4
8A25	11A080	1744+	LXI	D,CNST4
8A28	CD0185	1745+	CALL	PSHT
8A2B	CD708E	1746	CALL	FMUL
8A2E	CDA08E	1747	CALL	FDIV
8A31	CD0C8F	1748	CALL	ACOS
		1749	PLL	AA
8A34	110D30	1750+	LXI	D,AA
8A37	CD1785	1751+	CALL	PLLT
		1752		
		1753	PSH	YI
8A3A	115C30	1754+	LXI	D,YI
8A3D	CD0185	1755+	CALL	PSHT
8A40	CD7C8E	1756	CALL	CHSF
		1757	PSH	DX
8A43	110130	1758+	LXI	D,DX
8A46	CD0185	1759+	CALL	PSHT
8A49	CDA08E	1760	CALL	FDIV
8A4C	CD0C8F	1761	CALL	ACOS
		1762	PLL	AB
8A4F	111130	1763+	LXI	D,AB
8A52	CD1785	1764+	CALL	PLLT
		1765	PSH	AB
8A55	111130	1766+	LXI	D,AB
8A58	CD0185	1767+	CALL	PSHT
		1768	PSH	AA
8A5B	110D30	1769+	LXI	D,AA
8A5E	CD0185	1770+	CALL	PSHT
8A61	CD648E	1771	CALL	FADD
		1772	PLL	AI
8A64	110530	1773+	LXI	D,AI
8A67	CD1785	1774+	CALL	PLLT
		1775	PSH	AI
8A6A	110530	1776+	LXI	D,AI
8A6D	CD0185	1777+	CALL	PSHT
		1778	PSH	ALPHA
8A70	118430	1779+	LXI	D,ALPHA
8A73	CD0185	1780+	CALL	PSHT
8A76	CD948E	1781	CALL	FSUB
8A79	CDC48E	1782	CALL	PTOF

```

;
;AA=ACOS(((LA**2+DX**2-RA**2)/

```

```

; (2*LA*DX))

```

```

;
;AB=ACOS((-YI/DX)

```

```

;AI=AA+AB

```

```

;ALPHA=AI-ALPHA

```

LOC	OBJ	LINE	SOURCE STATEMENT
		1783	PLL EALPHA
8A7C	11A130	1784+	LXI D,EALPHA
8A7F	CD1785	1785+	CALL PLLT
		1786	PSH A1A
8A82	11D930	1787+	LXI D,A1A
8A85	CD0185	1788+	CALL PSHT
8A88	CD708E	1789	CALL FMUL
		1790	PLL VVALFA
8A8B	11AD30	1791+	LXI D,VVALFA
8A8E	CD1785	1792+	CALL PLLT
		1793	PSH BI
8A91	110930	1794+	LXI D,BI
8A94	CD0185	1795+	CALL PSHT
		1796	PSH BETA
8A97	118830	1797+	LXI D,BETA
8A9A	CD0185	1798+	CALL PSHT
8A9D	CD948E	1799	CALL FSUB
8AA0	CD48E	1800	CALL PTOF
		1801	PLL EBETA
8AA3	11A530	1802+	LXI D,EBETA
8AA6	CD1785	1803+	CALL PLLT
		1804	PSH A1B
8AA9	11DD30	1805+	LXI D,A1B
8AAC	CD0185	1806+	CALL PSHT
8AAF	CD708E	1807	CALL FMUL
		1808	PLL VVBETA
8AB2	11B130	1809+	LXI D,VVBETA
8AB5	CD1785	1810+	CALL PLLT
8AB8	CD6D8B	1811	CALL CHKLMT
8ABB	3A0030	1812 L47:	LDA MODFLB
8ABE	FE00	1813	CPI 00H
8AC0	C2038B	1814	JNZ L49
		1815	
		1816	
		1817	
		1818	IFF JBKT,GTHAN,ZERO,L41
		1819+	PSH JBKT
8AC3	11A430	1820+	LXI D,JBKT
8AC6	CD0185	1821+	CALL PSHT
		1822+	PLL V1
8AC9	119530	1823+	LXI D,V1
8ACC	CD1785	1824+	CALL PLLT
		1825+	PSH ZERO
8ACF	117D80	1826+	LXI D,ZERO
8AD2	CD0185	1827+	CALL PSHT
		1828+	PLL V2
8AD5	119930	1829+	LXI D,V2
8AD8	CD1785	1830+	CALL PLLT
8ADB	CD3085	1831+	CALL GTHAN
8ADE	E601	1832+	ANI 01H
8AE0	C2508B	1833+	JNZ L41
		1834	IFF JBKT,LTHAN,ZERO,L42
		1835+	PSH JBKT
8AE3	11A430	1836+	LXI D,JBKT
8AE6	CD0185	1837+	CALL PSHT

LOC	OBJ	LINE	SOURCE STATEMENT
		1838+	PLL V1
8AE9	119530	1839+	LXI D,V1
8AEC	CD1785	1840+	CALL PLLT
		1841+	PSH ZERO
8AEF	117D80	1842+	LXI D,ZERO
8AF2	CDO185	1843+	CALL PSHT
		1844+	PLL V2
8AF5	119930	1845+	LXI D,V2
8AF8	CD1785	1846+	CALL PLLT
8AFB	CD4785	1847+	CALL LTHAN
8AFE	E601	1848+	ANI 01H
8B00	C25D8B	1849+	JNZ L42
		1850 L49:	IFF EPSI,GTHAN,PCRIT,L41
		1851+	PSH EPSI
8B03	117830	1852+	LXI D,EPSI
8B06	CDO185	1853+	CALL PSHT
		1854+	PLL V1
8B09	119530	1855+	LXI D,V1
8B0C	CD1785	1856+	CALL PLLT
		1857+	PSH PCRIT
8B0F	11E130	1858+	LXI D,PCRIT
8B12	CDO185	1859+	CALL PSHT
		1860+	PLL V2
8B15	119930	1861+	LXI D,V2
8B18	CD1785	1862+	CALL PLLT
8B1B	CD3085	1863+	CALL GTHAN
8B1E	E601	1864+	ANI 01H
8B20	C2508B	1865+	JNZ L41
		1866	IFF EPSI,LTHAN,NCRIT,L42
		1867+	PSH EPSI
8B23	117830	1868+	LXI D,EPSI
8B26	CDO185	1869+	CALL PSHT
		1870+	PLL V1
8B29	119530	1871+	LXI D,V1
8B2C	CD1785	1872+	CALL PLLT
		1873+	PSH NCRIT
8B2F	11E530	1874+	LXI D,NCRIT
8B32	CDO185	1875+	CALL PSHT
		1876+	PLL V2
8B35	119930	1877+	LXI D,V2
8B38	CD1785	1878+	CALL PLLT
8B3B	CD4785	1879+	CALL LTHAN
8B3E	E601	1880+	ANI 01H
8B40	C25D8B	1881+	JNZ L42
		1882	PSH ZERO
8B43	117D80	1883+	LXI D,ZERO
8B46	CDO185	1884+	CALL PSHT
		1885	PLL VVBKT
8B49	118530	1886+	LXI D,VVBKT
8B4C	CD1785	1887+	CALL PLLT
8B4F	C9	1888	RET
		1889 L41:	PSH ONE
8B50	118180	1890+	LXI D,ONE
8B53	CDO185	1891+	CALL PSHT
		1892	PLL VVBKT

!EPSI=0: VVBKT=0

LDC	OBJ	LINE	SOURCE	STATEMENT
8B56	11B530	1893+	LXI	D,VVBKT
8B59	CD1785	1894+	CALL	PLLT
8B5C	C9	1895	RET	
		1896 L42:	PSH	ONE
8B5D	118180	1897+	LXI	D,ONE
8B60	CD0185	1898+	CALL	PSHT
8B63	CD7C8E	1899	CALL	CHSF
		1900	PLL	VVBKT
8B66	11B530	1901+	LXI	D,VVBKT
8B69	CD1785	1902+	CALL	PLLT
8B6C	C9	1903	RET	
		1904		
		1905		
		1906		** SUBROUTINE CHKLMT **
		1907		
		1908		FREEZES LIFT AND REACH ARM
		1909		MOVEMENT IF ATTEMPT IS MADE TO
		1910		EXCEED THE LIMIT OF RAM TRAVEL
		1911		
		1912		REGISTERS AFFECTED: A,D,E,STATUS
		1913		
		1914 CHKLMT:	IFF	MCALFA,GEQUAL,AMAX,L80
		1915+	PSH	MCALFA
8B6D	118030	1916+	LXI	D,MCALFA
8B70	CD0185	1917+	CALL	PSHT
		1918+	PLL	V1
8B73	119530	1919+	LXI	D,V1
8B76	CD1785	1920+	CALL	PLLT
		1921+	PSH	AMAX
8B79	110531	1922+	LXI	D,AMAX
8B7C	CD0185	1923+	CALL	PSHT
		1924+	PLL	V2
8B7F	119930	1925+	LXI	D,V2
8B82	CD1785	1926+	CALL	PLLT
8B85	CD5E85	1927+	CALL	GEQUAL
8B88	E601	1928+	ANI	01H
8B8A	C2908B	1929+	JNZ	L80
8B8D	C3B08B	1930	JMP	L81
		1931 L80:	IFF	VVALFA,GEQUAL,ZERO,L87
		1932+	PSH	VVALFA
8B90	11AD30	1933+	LXI	D,VVALFA
8B93	CD0185	1934+	CALL	PSHT
		1935+	PLL	V1
8B96	119530	1936+	LXI	D,V1
8B99	CD1785	1937+	CALL	PLLT
		1938+	PSH	ZERO
8B9C	117D60	1939+	LXI	D,ZERO
8B9F	CD0185	1940+	CALL	PSHT
		1941+	PLL	V2
8BA2	119930	1942+	LXI	D,V2
8BA5	CD1785	1943+	CALL	PLLT
8BA8	CD5E85	1944+	CALL	GEQUAL
8BA9	E601	1945+	ANI	01H
8BAD	C27C8C	1946+	JNZ	L87
		1947 L81:	IFF	MCALFA,LEQUAL,AMIN,L82

LOC	OBJ	LINE	SOURCE STATEMENT
		1948+	PSH MCALFA
8BB0	118030	1949+	LXI D,MCALFA
8BB3	CD0185	1950+	CALL PSHT
		1951+	PLL V1
8BB6	119530	1952+	LXI D,V1
8BB9	CD1785	1953+	CALL PLLT
		1954+	PSH AMIN
8BBC	110131	1955+	LXI D,AMIN
8BBF	CD0185	1956+	CALL PSHT
		1957+	PLL V2
8BC2	119930	1958+	LXI D,V2
8BC5	CD1785	1959+	CALL PLLT
8BC8	CD6385	1960+	CALL LEQUAL
8BCB	E601	1961+	ANI 01H
8BCD	C2D38B	1962+	JNZ L82
8BD0	C3F38B	1963	JMP L83
		1964 L82:	IFF VVALFA,LEQUAL,ZERO,L87
		1965+	PSH VVALFA
8BD3	11AD30	1966+	LXI D,VVALFA
8BD6	CD0185	1967+	CALL PSHT
		1968+	PLL V1
8BD9	119530	1969+	LXI D,V1
8BDC	CD1785	1970+	CALL PLLT
		1971+	PSH ZERO
8BDF	117D80	1972+	LXI D,ZERO
8BE2	CD0185	1973+	CALL PSHT
		1974+	PLL V2
8BE5	119930	1975+	LXI D,V2
8BE8	CD1785	1976+	CALL PLLT
8BED	CD6385	1977+	CALL LEQUAL
8BEE	E601	1978+	ANI 01H
8BF0	C27C8C	1979+	JNZ L87
		1980 L83:	IFF BETA,GEQUAL,BMAX,L84
		1981+	PSH BETA
8BF3	118830	1982+	LXI D,BETA
8BF6	CD0185	1983+	CALL PSHT
		1984+	PLL V1
8BF9	119530	1985+	LXI D,V1
8BFC	CD1785	1986+	CALL PLLT
		1987+	PSH BMAX
8BFF	110D31	1988+	LXI D,BMAX
8C02	CD0185	1989+	CALL PSHT
		1990+	PLL V2
8C05	119930	1991+	LXI D,V2
8C08	CD1785	1992+	CALL PLLT
8C0B	CD5E85	1993+	CALL GEQUAL
8C0E	E601	1994+	ANI 01H
8C10	C2168C	1995+	JNZ L84
8C13	C3368C	1996	JMP L85
		1997 L84:	IFF VVBETA,GEQUAL,ZERO,L87
		1998+	PSH VVBETA
8C16	11B130	1999+	LXI D,VVBETA
8C19	CD0185	2000+	CALL PSHT
		2001+	PLL V1
8C1C	119530	2002+	LXI D,V1

LOC	OBJ	LINE	SOURCE STATEMENT
8C1F	CD1785	2003+	CALL PLLT
8C22	117D80	2004+	PSH ZERO
8C23	CD0185	2005+	LXI D,ZERO
8C29	119330	2006+	CALL PSHT
8C2B	CD1785	2007+	PLL V2
8C2E	CD5E85	2008+	LXI D,V2
8C31	E601	2009+	CALL PLLT
8C33	C27C8C	2010+	CALL GEQUAL
8C36	118E30	2011+	ANI 01H
8C39	CD0185	2012+	JNZ L87
8C3C	CD0185	2013 L85I	JFF
8C3E	CD1785	2014+	PSH BETA,LEQUAL,BMIN,L86
8C42	110931	2015+	BETA
8C45	CD0185	2016+	LXI D,BETA
8C48	119330	2017+	CALL PSHT
8C49	CD1785	2018+	PLL V1
8C4E	CD5385	2019+	LXI D,V1
8C51	E601	2020+	CALL PLLT
8C53	C2598C	2021+	CALL BMIN
8C56	C37F8C	2022+	LXI D,BMIN
8C59	11B130	2023+	CALL PSHT
8C5C	CD0185	2024+	PLL V2
8C62	119330	2025+	LXI D,V2
8C66	CD1785	2026+	CALL PLLT
8C6A	CD6385	2027+	CALL LEQUAL
8C6D	CD1785	2028+	ANI 01H
8C71	CD6385	2029	JNZ L86
8C74	E601	2030 L86I	JMP
8C77	C27C8C	2031+	L88
8C7A	E601	2032+	JFF
8C7D	C27C8C	2033+	PSH VVBETA,LEQUAL,ZERO,L87
8C81	CD1785	2034+	LXI D,VVBETA
8C84	CD1785	2035+	CALL PSHT
8C87	CD1785	2036+	PLL V1
8C8A	CD1785	2037+	LXI D,V1
8C8D	CD1785	2038+	CALL PLLT
8C91	CD6385	2039+	CALL LEQUAL
8C94	CD1785	2040+	ANI 01H
8C97	CD1785	2041+	JNZ L87
8C9A	CD1785	2042+	L88
8C9D	CD1785	2043+	JMP L88
8CA1	CD6385	2044+	CALL LEQUAL
8CA4	CD1785	2045+	ANI 01H
8CA7	CD1785	2046	JNZ L87
8CAB	CD1785	2047 L87I	L88
8CAC	CD1785	2048 L88I	CALL LEQUAL
8CAD	CD1785	2049	RET
8CAE	CD1785	2050	
8CAF	CD1785	2051	
8CB1	CD6385	2052	
8CB4	CD1785	2053	
8CB7	CD1785	2054	
8CB9	CD1785	2055	
8CBB	CD1785	2056	
8CBE	CD1785	2057	

```

I
I
I
I** SUBROUTINE FREEZE **
I
I
I ASSIGNS VALUE ZERO TO ALPHA
I AND BETA VALVE SETTINGS
I
I REGISTERS AFFECTED: D,E
I

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LOC	OBJ	LINE	SOURCE STATEMENT
		2058	FREEZE: PSH ZERO
8C80	117D80	2059+	LXI D,ZERO
8C83	CD0185	2060+	CALL PSHT
8C86	CDC48E	2061	CALL PTDF
		2062	PLL VVALFA
8C89	11AD30	2063+	LXI D,VVALFA
8C8C	CD1785	2064+	CALL PLLT
		2065	PLL VVBETA
8C8F	11B130	2066+	LXI D,VVBETA
8C92	CD1785	2067+	CALL PLLT
8C95	C9	2068	RET
		2069	
		2070	
		2071	*** SUBROUTINE OUTPUT **
		2072	
		2073	! OPERATES CUT-OFF, OFFSETS
		2074	! AND OUTPUTS SIGNAL TO
		2075	! VALVE DRIVERS
		2076	!
		2077	!REGISTERS AFFECTED: A,D,E,S
		2078	!
		2079	OUTPUT: PSH VVSLEW
8C96	11A930	2080+	LXI D,VVSLEW
8C99	CD0185	2081+	CALL PSHT
		2082	PLL FVD
8C9C	11C230	2083+	LXI D,FVD
8CA2	3AD530	2084+	CALL PLLT
8CA5	32C930	2085	LDA SPOF
8CA8	3AD730	2086	STA POF
8CA9	32CA30	2087	LDA SNOF
8CAE	3AD630	2088	STA NOF
8CB1	32CB30	2089	LDA SPMAX
8CB4	3AD830	2090	STA PMAX
8CB7	32CC30	2091	LDA SNMAX
8CBA	CD8A8D	2092	STA NMAX
8CBD	32B930	2093	CALL VLIN
8CC0	D300	2094	STA VS
		2095	OUT OOH
		2096	LS2: PSH VVALFA
8CC2	11AD30	2097+	LXI D,VVALFA
8CC5	CD0185	2098+	CALL PSHT
		2099	PLL FVD
8CC8	11C230	2100+	LXI D,FVD
8CCB	CD1785	2101+	CALL PLLT
8CCE	3ACD30	2102	LDA APOF
8CD1	32C930	2103	STA POF
8CD4	3ACF30	2104	LDA ANOF
8CD7	32CA30	2105	STA NOF
8CDA	3ACE30	2106	LDA APMAX
8CDD	32CB30	2107	STA PMAX
8CE0	3AD030	2108	LDA ANMAX
8CE3	32CC30	2109	STA NMAX
8CE6	CD8A8D	2110	CALL VLIN
8CE9	32BA30	2111	STA VL
8CEC	D301	2112	OUT OIH

LOC	OBJ	LINE	SOURCE STATEMENT
		2113 L53:	PSH VVBETA ;SET REACH VALVE
8CEE	11B130	2114+	LXI D,VVBETA
8CF1	CD0185	2115+	CALL PSHT
		2116	PLL FV0
8CFA	11C230	2117+	LXI D,FV0
8CF7	CD1785	2118+	CALL PLLT
8CFA	3AD130	2119	LDA BPOF
8CFD	32C930	2120	STA POF
8D00	3AD330	2121	LDA BNOF
8D03	32CA30	2122	STA NOF
8D06	3AD230	2123	LDA BPMAX
8D09	32CB30	2124	STA PMAX
8D0C	3AD430	2125	LDA BNMAX
8D0F	32CC30	2126	STA NMAX
8D12	CD8A8D	2127	CALL VLIN
8D15	32BB30	2128	STA VR
8D18	D321	2129	OUT 21H
		2130 L54:	IFF VVBKT,EQUALS,ZERO,L55 ;SET BUCKET SWITCH
		2131+	PSH VVBKT
8D1A	11B530	2132+	LXI D,VVBKT
8D1D	CD0185	2133+	CALL PSHT
		2134+	PLL V1
8D20	119530	2135+	LXI D,V1
8D23	CD1785	2136+	CALL PLLT
		2137+	PSH ZERO
8D26	117D80	2138+	LXI D,ZERO
8D29	CD0185	2139+	CALL PSHT
		2140+	PLL V2
8D2C	119930	2141+	LXI D,V2
8D2F	CD1785	2142+	CALL PLLT
8D32	CD6D85	2143+	CALL EQUALS
8D35	E601	2144+	ANI 01H
8D37	C25D8D	2145+	JNZ L55
		2146	IFF VVBKT,GTHAN,ZERO,L56
		2147+	PSH VVBKT
8D3A	11B530	2148+	LXI D,VVBKT
8D3D	CD0185	2149+	CALL PSHT
		2150+	PLL V1
8D40	119530	2151+	LXI D,V1
8D43	CD1785	2152+	CALL PLLT
		2153+	PSH ZERO
8D46	117D80	2154+	LXI D,ZERO
8D49	CD0185	2155+	CALL PSHT
		2156+	PLL V2
8D4C	119930	2157+	LXI D,V2
8D4F	CD1785	2158+	CALL PLLT
8D52	CD3085	2159+	CALL GTHAN
8D55	E601	2160+	ANI 01H
8D57	C2658D	2161+	JNZ L56
8D5A	C36D8D	2162	JMP L57
8D5D	3E00	2163 L55:	MVI A,0COH ;SEGMENT FOR STATIC BUCKET
8D5F	32BC30	2164	STA VB
8D62	D322	2165	OUT 22H
8D64	C9	2166	RET
8D65	3E80	2167 L56:	MVI A,80H ;SEGMENT FOR OPENING BUCKET

LOC	OBJ	LINE	SOURCE STATEMENT
8D67	32BC30	2168	STA VB
8D6A	D322	2169	OUT 22H
8D6C	C9	2170	RET
8D6D	3E40	2171	MVI A,40H
8D6F	32BC30	2172	STA VB
8D72	D322	2173	OUT 22H
8D74	C9	2174	RET
		2175	
		2176	
		2177	
		2178	
		2179	
		2180	
		2181	
		2182	
		2183	
8D75	320010	2184	FLOAT: STA 1000H
8D78	AF	2185	XRA A
8D79	320010	2186	STA 1000H
8D7C	CD888E	2187	CALL FLTS
8D7F	C9	2188	RET
		2189	
		2190	
		2191	
		2192	
		2193	
		2194	
		2195	
		2196	
		2197	
8D80	CDAC8E	2198	FIX: CALL FIXS
8D83	3A0010	2199	LDA 1000H
8D86	3A0010	2200	LDA 1000H
8D89	C9	2201	RET
		2202	
		2203	
		2204	
		2205	
		2206	
		2207	
		2208	
		2209	
		2210	
		2211	
		2212	
		2213	
		2214	VLIN: IFF FVD,GTHAN,ZERO,L61
		2215+	PSH FVD
8D8A	11C230	2216+	LXI D,FVD
8D8D	CD0185	2217+	CALL PSHT
		2218+	PLL V1
8D90	119530	2219+	LXI D,V1
8D93	CD1785	2220+	CALL PLLT
		2221+	PSH ZERO
8D96	117D80	2222+	LXI D,ZERO

;SEGMENT FOR CLOSING BUCKET
 ;
 ;
 ;** SUBROUTINE FLOAT **
 ;
 ;PUTS CONTENTS OF 'A' REGISTER
 ; ON TOP OF APU STACK
 ;
 ;REGISTERS AFFECTED: A
 ;
 ;
 ;
 ;** SUBROUTINE FIX **
 ;
 ;PUTS 32-BIT TOS OF APU
 ; IN THE A REGISTER
 ;
 ;REGISTERS AFFECTED: A
 ;
 ;
 ;
 ;** SUBROUTINE VLIN **
 ;
 ;VALVE OPENING IN NOMINAL RANGE -1 TO
 ; +1 IS PASSED IN FVD.
 ; SUBROUTINE CALCUALATES BYTE OP TO
 ; BE OUTPUT TO THE DRIVER CIRCUIT
 ; USING DATA POS, PMAX, NOS, & NMAX.
 ;
 ;REGISTERS AFFECTED: A,D,E,STATUS
 ;

LOC	OBJ	LINE	SOURCE STATEMENT
8D99	CD0185	2223+	CALL PSHT
		2224+	PLL V2
8D9C	119930	2225+	LXI D,V2
8D9F	CD1785	2226+	CALL PLLT
8DA2	CD3085	2227+	CALL GTHAN
8DA5	E601	2228+	ANI 01H
8DA7	C2CC8D	2229+	JNZ L61
		2230	IFF FVD,LTHAN,ZERO,L62
		2231+	PSH FVD
SDAA	11C230	2232+	LXI D,FVD
SDAD	CD0185	2233+	CALL PSHT
		2234+	PLL V1
SDB0	119530	2235+	LXI D,V1
SDB3	CD1785	2236+	CALL PLLT
		2237+	PSH ZERO
8DB6	11D80	2238+	LXI D,ZERO
8DB9	CD0185	2239+	CALL PSHT
		2240+	PLL V2
8DBC	119930	2241+	LXI D,V2
8DBF	CD1785	2242+	CALL PLLT
8DC2	CD4785	2243+	CALL LTHAN
8DC5	E601	2244+	ANI 01H
8DC7	C2008E	2245+	JNZ L62
8DCA	AF	2246	XRA A
8DCB	C9	2247	RET
		2248 L61:	IFF FVD,LTHAN,ONE,L63
		2249+	PSH FVD
8DCC	11C230	2250+	LXI D,FVD
8DCF	CD0185	2251+	CALL PSHT
		2252+	PLL V1
8DD2	119530	2253+	LXI D,V1
8DD5	CD1785	2254+	CALL PLLT
		2255+	PSH ONE
8DD8	118180	2256+	LXI D,ONE
8DDB	CD0185	2257+	CALL PSHT
		2258+	PLL V2
8DDE	119930	2259+	LXI D,V2
8DE1	CD1785	2260+	CALL PLLT
8DE4	CD4785	2261+	CALL LTHAN
8DE7	E601	2262+	ANI 01H
8DE9	C3F08D	2263+	JNZ L63
8DEC	3ACB30	2264	LDA PMAX
8DEF	C9	2265	RET
8DF0	3AC930	2266 L63:	LDA POF
8DF3	32C730	2267	STA OFFSET
8DF6	3ACB30	2268	LDA PMAX
8DF9	32C830	2269	STA MAX
8DFC	C33F8E	2270	JMP L64
8DFF	C9	2271	RET
		2272 L62:	IFF FVD,GTHAN,MINONE,L65
		2273+	PSH FVD
8E00	11C230	2274+	LXI D,FVD
8E03	CD0185	2275+	CALL PSHT
		2276+	PLL V1
8E06	119530	2277+	LXI D,V1

!SEGMENT FOR FVD=0

!SEGMENT FOR FVD) PMAX

!SEGMENT FOR 0 (FVD (1

LOC	OBJ	LINE	SOURCE STATEMENT	
-		2333	RET	
		2334	ENDM	
		2335		
		2336		
		2337		** MATHS MACRO CALLS **
		2338		
		2339		ALL OPERANDS ARE 32 BIT FLOATING
		2340		POINT UNLESS OTHERWISE INDICATED
		2341		
		2342	MATHS FADD,10H	ADD TOS TO NOS, RESULT ON TOS
8E64	32C630	2343+FADD:	STA ASTR	
8E67	3E10	2344+	MVI A,10H	
8E69	320011	2345+	STA 1100H	
8E6C	3AC630	2346+	LDA ASTR	
8E6F	C9	2347+	RET	
		2348	MATHS FMUL,12H	MULTIPLY TOS AND NOS, RESULT ON TOS
8E70	32C630	2349+FMUL:	STA ASTR	
8E73	3E12	2350+	MVI A,12H	
8E75	320011	2351+	STA 1100H	
8E78	3AC630	2352+	LDA ASTR	
8E7B	C9	2353+	RET	
		2354	MATHS CHSF,15H	CHANGE SIGN OF TOS
8E7C	32C630	2355+CHSF:	STA ASTR	
8E7F	3E15	2356+	MVI A,15H	
8E81	320011	2357+	STA 1100H	
8E84	3AC630	2358+	LDA ASTR	
8E87	C9	2359+	RET	
		2360	MATHS FLTS,1DH	CONVERTS 16 BIT TOS TO 32 BIT FL. PT.
8E88	32C630	2361+FLTS:	STA ASTR	
8E8B	3E1D	2362+	MVI A,1DH	
8E8D	320011	2363+	STA 1100H	
8E90	3AC630	2364+	LDA ASTR	
8E93	C9	2365+	RET	
		2366	MATHS FSUB,11H	TOS=NOS-TOS
8E94	32C630	2367+FSUB:	STA ASTR	
8E97	3E11	2368+	MVI A,11H	
8E99	320011	2369+	STA 1100H	
8E9C	3AC630	2370+	LDA ASTR	
8E9F	C9	2371+	RET	
		2372	MATHS FDIV,13H	TOS=NOS/TOS
8EA0	32C630	2373+FDIV:	STA ASTR	
8EA3	3E13	2374+	MVI A,13H	
8EA5	320011	2375+	STA 1100H	
8EA8	3AC630	2376+	LDA ASTR	
8EAB	C9	2377+	RET	
		2378	MATHS FIXS,1FH	CONVERTS TOS TO 16 BIT FIXED PT
8EAC	32C630	2379+FIXS:	STA ASTR	
8EAF	3E1F	2380+	MVI A,1FH	
8EB1	320011	2381+	STA 1100H	
8EB4	3AC630	2382+	LDA ASTR	
8EB7	C9	2383+	RET	
		2384	MATHS PTOS,77H	COPY 16 BIT TOS ONTO STACK
8EB8	32C630	2385+PTOS:	STA ASTR	
8EBB	3E77	2386+	MVI A,77H	
8EBD	320011	2387+	STA 1100H	

LOC	OBJ	LINE	SOURCE STATEMENT
8EC0	3AC630	2388+	LDA ASTR
8EC3	C9	2389+	RET
8EC4	32C630	2390	MATHS PTOF,17H
8EC7	3E17	2391+PTOF:	STA ASTR
8EC9	320011	2392+	MVI A,17H
8ECC	3AC630	2393+	STA 1100H
8ECF	C9	2394+	LDA ASTR
8ED0	32C630	2395+	RET
8ED3	3E18	2396	MATHS POPF,18H
8ED5	320011	2397+POPF:	STA ASTR
8ED8	3AC630	2398+	MVI A,18H
8EDB	C9	2399+	STA 1100H
8EDC	32C630	2400+	LDA ASTR
8EDF	3E1A	2401+	RET
8EE1	320011	2402	MATHS PUPI,1AH
8EE4	3AC630	2403+PUPI:	STA ASTR
8EE7	C9	2404+	MVI A,1AH
8EE8	32C630	2405+	STA 1100H
8EEB	3E02	2406+	LDA ASTR
8EED	320011	2407+	RET
8EF0	3AC630	2408	MATHS SIN,02H
8EF3	C9	2409+SIN:	STA ASTR
8EF4	32C630	2410+	MVI A,02H
8EF7	3E05	2411+	STA 1100H
8EF9	320011	2412+	LDA ASTR
8EFC	3AC630	2413+	RET
8EFF	C9	2414	MATHS ASIN,05H
8F00	32C630	2415+ASIN:	STA ASTR
8F03	3E03	2416+	MVI A,05H
8F05	320011	2417+	STA 1100H
8F08	3AC630	2418+	LDA ASTR
8F0B	C9	2419+	RET
8F0C	32C630	2420	MATHS COS,03H
8F0F	3E06	2421+COS:	STA ASTR
8F11	320011	2422+	MVI A,03H
8F14	3AC630	2423+	STA 1100H
8F17	C9	2424+	LDA ASTR
8F18	32C630	2425+	RET
8F1B	3E19	2426	MATHS ACOS,06H
8F1D	320011	2427+ACOS:	STA ASTR
8F20	3AC630	2428+	MVI A,06H
8F23	C9	2429+	STA 1100H
8F24	32C630	2430+	LDA ASTR
8F27	3E01	2431+	RET
8F29	320011	2432	MATHS XCHF,19H
8F2C	3AC630	2433+XCHF:	STA ASTR
		2434+	MVI A,19H
		2435+	STA 1100H
		2436+	LDA ASTR
		2437+	RET
		2438	MATHS SQRT,01H
		2439+SQRT:	STA ASTR
		2440+	MVI A,01H
		2441+	STA 1100H
		2442+	LDA ASTR

{COPY 32 BIT TOS ONTO STACK

{ROTATE TOS TO BOTTOM OF STACK

{PUSH PI ONTO TOS

{TOS=SIN(TOS)

{TOS=ASIN(TOS)

{TOS=COS(TOS)

{TOS=ACOS(TOS)

{EXCHANGE TOS AND NOS

{TOS=SQRT TOS

```

LOC OBJ          LINE          SOURCE STATEMENT
 8F2F C9          2443+          RET
                   2444 END
    
```

PUBLIC SYMBOLS

EXTERNAL SYMBOLS

USER SYMBOLS

A1A	A 30D9	A1B	A 30DD	AA	A 300D	AB	A 3011	ACOS	A 8F0C	ADCON	A 84E7	AI	A 3005
ALFIP	A 845D	ALPHA	A 3084	AMAX	A 3105	AMIN	A 3101	ANMAX	A 30D0	ANOF	A 30CF	APMAX	A 30CE
APOF	A 30CD	ASIN	A 8EF4	ASTR	A 30C6	BASE	A 3111	BETA	A 3088	BETIP	A 8497	BI	A 3009
BMAX	A 310D	BMIN	A 3109	BNMAX	A 30D4	BNOF	A 30D3	BPMAX	A 30D2	BPOF	A 30D1	CA	A 8059
CB	A 8061	CD	A 8069	CHKLMT	A 8B6D	CHSF	A 8E7C	CNST1	A 80A1	CNST10	A 30ED	CNST11	A 30F1
CNST13	A 80B5	CNST14	A 80B9	CNST2	A 80A5	CNST20	A 80BD	CNST21	A 80C1	CNST3	A 80A9	CNST4	A 80AD
CNST9	A 80B1	CONV	A 8413	COORD	A 863F	COS	A 8F00	CXDOT	A 3050	CYDOT	A 3054	D14	A 80C5
DCRIT	A 30F5	DELAY	A 30FF	DELTA	A 308C	DELTIP	A 84BF	DIST	A 302C	DLOOP	A 80D8	DPSCRIT	A 30F9
DPSI	A 3030	DX	A 3001	EALPHA	A 30A1	EBETA	A 30A5	ECMIN	A 30E9	ECRIT	A 30BE	EPDS	A 8724
EPSI	A 3078	EQUALS	A 856D	ETA	A 307C	EX	A 3070	EY	A 3074	FADD	A 8E64	FCOUNT	A 30BD
FDIV	A 8E40	FFAST	A 30FD	FFD	A 895F	FIX	A 8D80	FIXS	A 8EAC	FLOAT	A 8D75	FLTS	A 8E88
FMUL	A 8E70	FREEZE	A 8C80	FSLOW	A 30FE	FSUB	A 8E94	FVD	A 30C2	GCO	A 8095	GC1	A 8099
GC2	A 809D	GEQUAL	A 855E	GTHAN	A 8530	H253	A 80C9	H79	A 8079	H87	A 8075	HALF	A 8085
I1	A 3048	I2	A 304C	IFF	+ 0002	INIT	A 82FE	IP1	A 87D5	IP2	A 8902	JBKT	A 3044
JOYSTK	A 8593	JSLEW	A 3040	JXDOT	A 3038	JYDOT	A 303C	L100	A 80FC	L101	A 8110	L102	A 8148
L103	A 8166	L104	A 8174	L108	A 8142	L109	A 8160	L2	A 853A	L201	A 81B1	L202	A 8291
L205	A 82A4	L206	A 81FA	L21	A 8801	L22	A 8842	L23	A 8883	L24	A 88A4	L26	A 88C5
L3	A 8544	L301	A 83A5	L308	A 8370	L32	A 895E	L4	A 8551	L41	A 8B50	L42	A 8B5D
L43	A 898F	L44	A 8996	L46	A 89B9	L47	A 8ABB	L49	A 8B03	L5	A 855B	L50	A 85EA
L51	A 8603	L52	A 8CC2	L53	A 8CEE	L54	A 8D1A	L55	A 8D5D	L56	A 8D65	L57	A 8D6D
L6	A 857C	L61	A 8DC0	L62	A 8E00	L63	A 8DF0	L64	A 8E3F	L65	A 8E24	L7	A 8590
L80	A 8B90	L81	A 8BB0	LS2	A 8BD3	L83	A 8BF3	L84	A 8C16	L85	A 8C36	L86	A 8C59
L87	A 8C7C	L88	A 8C7F	LA	A 806D	LEARN	A 81E6	LEQUAL	A 8563	LOOP	A 81D9	LOOP1	A 8182
LOOP3	A 81C3	LTHAN	A 8547	MA	A 8055	MANUAL	A 817C	MATHS	+ 0003	MAX	A 30C8	MAXPTS	A 804C
MB	A 805D	MCALFA	A 3080	MD	A 8065	MINDONE	A 8089	MLODP	A 80F3	MODE	A 301D	MODFLG	A 3000
MU	A 806D	NCDUNT	A 3036	NCRIT	A 30E5	NEQUAL	A 8568	NMAX	A 30CC	NDF	A 30CA	OFFSET	A 30C7
ONE	A 8081	OUTPUT	A 8C96	PAUSE	A 8797	PCOUNT	A 3034	PCRIT	A 30E1	PITCH	A 309D	PLL	+ 0001
PLLT	A 8517	PMAX	A 30CB	POF	A 30C9	POPF	A 8ED0	PPDINT	A 301E	PSH	+ 0000	PSHT	A 8501
PSII	A 3060	PSIO	A 306C	PSIP	A 3028	PTOF	A 8EC4	PTOS	A 8EB8	PUPI	A 8EDC	RA	A 8071
RCOUNT	A 3035	REPEAT	A 82FC	RFAST	A 83C0	RFCON	A 83CA	RSCON	A 83EB	RSETUP	A 82AC	RSLOW	A 83E1
S	A 3091	SETEC	A 879E	SIN	A 8EE8	SLOPE	A 861C	SNMAX	A 30D8	SNOF	A 30D7	SPMAX	A 30D6
SPOF	A 30D5	SQRT	A 8F24	STATUS	A 3090	TEN	A 804D	TFLAG	A 3037	TPULL	A 81BA	TPUSH	A 81D0
TWO	A 8051	V1	A 3095	V2	A 3099	VB	A 30BC	VL	A 30BA	VLIN	A 8DBA	VR	A 30BB
VS	A 30B9	VVALFA	A 30AD	VVBETA	A 30B1	VVBKT	A 30B5	VVBLEW	A 30A9	XA1A	A 800C	XA1B	A 8010
XAMAX	A 8040	XAMIN	A 803C	XANMAX	A 8003	XANDF	A 8002	XAPMAX	A 8001	XAPOF	A 8000	XBMAX	A 8048
XBMIN	A 8044	XBNMAX	A 8007	XBNOF	A 8006	XBPMAX	A 8005	XBPOF	A 8004	XCHF	A 8F18	XCST10	A 8028
XCST11	A 802C	XDCRIT	A 8030	XDELAY	A 803A	XDPCRT	A 8034	XEACRT	A 8020	XEBCRT	A 8024	XEMIN	A 801C
XFFAST	A 8038	XFSLDW	A 8039	XI	A 3058	XNCRIT	A 8018	XO	A 3064	XOF	A 3015	XP	A 3020
XPCRIT	A 8014	XPXD	A 81A9	XSNMAX	A 800B	XSNOF	A 800A	XSPMAX	A 8009	XSPOF	A 8008	XY	A 8190
YI	A 305C	YD	A 3068	YOF	A 3019	YP	A 3024	ZERO	A 807D	ZETA	A 8091		

ASSEMBLY COMPLETE, NO ERRORS