

Hybrid uncertainty propagation based on multi-fidelity surrogate model

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Abstract

There always exist multiple uncertainties including random uncertainty, interval uncertainty, and fuzzy uncertainty in engineering structures. In the presence of hybrid uncertainties, the hybrid uncertainty propagation analysis can be a challenging problem, which suffers from the computational burden of double-loop procedure when numerical simulation techniques are employed. In this work, a novel method for efficient hybrid uncertainty propagation analysis with the three types of uncertainties is proposed. Generally, multi-fidelity surrogate models, such as Co-Kriging, can greatly improve the computational efficiency by leveraging information from a low-fidelity model to build a high-fidelity approximate model. However, the traditional multi-fidelity surrogate model methods always calculate the hybrid uncertainty propagation result by combining with several numerical simulation techniques. This process can introduce post-processing errors unless unlimited number of samples are used, which is impossible in engineering application. In order to address this issue, the analytical solutions of the output mean and output variance are derived based on the Co-Kriging, and the resulting mean and variance are both random variables. Moreover, a new adaptive framework is established to strengthen the estimation accuracy of the hybrid uncertainty propagation result, by combining the augmented expected improvement function and the derived mean random variable. Several applications are introduced to demonstrate the effectiveness of the proposed method for solving hybrid uncertainty propagation problems.

Keywords: Hybrid uncertainties; Uncertainty propagation; Multi-fidelity surrogate model; Analytical solution; Adaptive framework

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Preprint submitted to Elsevier

27 1. Introduction

28 Uncertainty is pervasive in engineering practice due to the inevitable variability of structures. These
29 uncertainties in inputs can have a significant impact on responses of interest. Thus, uncertainty propaga-
30 tion analysis, which aims to quantify the uncertainties in the output that propagate from the input, has
31 become a crucial foundation of uncertainty quantification, such as reliability-based design optimization
32 (RBDO) [1, 2] and robust design optimization (RDO) [3, 4]. However, how to assess this propagation of
33 uncertainty remains a challenge due to the increasing complexity of engineering structures. To this end,
34 many uncertainty propagation approaches have been investigated, including simulation-based methods
35 [5, 6], Taylor series expansion-based methods [7, 8], numerical integration-based method [9, 10], and
36 surrogate model-based methods [11, 12], etc.

37 Generally, the notion of uncertainty can be divided into two distinct classes: aleatory and epistemic
38 uncertainties [13, 14]. Aleatory uncertainty, also termed as inherent uncertainty, describes the natural
39 randomness of structural system. This type of uncertainty is irreducible and it is usually handled by
40 probabilistic methods. Epistemic uncertainty, on the other hand, stems from scarce experimental data
41 or insufficient information. As more knowledge or samples become available, this type of uncertainty
42 can be reduced. For aleatory uncertainty, random variables with precise probability distributions are
43 used to characterize input uncertainties. For epistemic uncertainty, because available information is
44 imprecise, evidence theory (also known as Dempster–Shafer theory), fuzzy set theory, interval theory,
45 etc., are usually adopted to represent input parameters.

46 Monte Carlo simulation (MCS) [15] is a traditional simulation-based method, the results of which are
47 widely used as a reference to verify the accuracy of other methods due to its simplicity and robustness.
48 However, for MCS, as well as some improved simulation-based methods (e.g., subset simulation (SS),
49 importance sampling (IS), directional simulation (DS), line sampling (LS), etc.), the prohibitive com-
50 putational cost is still a limitation, especially when a single simulation is time-consuming and multiple
51 uncertainties coexist. Over the past few decades, some research has been done on uncertainty propaga-
52 tion problems involving only one type of uncertainty. For example, Rao and Berke [16] applied interval

53 analysis to uncertain structures. Lee and Chen [17] performed a comparative study on the performances
54 of some uncertainty propagation methods. In the work of Wei et al. [18], polynomial chaos expansion
55 constructed with points of monomial cubature rules is proposed for uncertainty propagation. Long et
56 al. [19] presented an interval analysis method for the fatigue crack growth life prediction. Liu et al.
57 [20] provided a non-probabilistic uncertainty propagation method, where the uncertain parameters are
58 modeled using the ellipsoidal convex set. Wang and Matthies [21] proposed a modified parallelepiped
59 model for the non-probabilistic uncertainty propagation. Remarkably, one of the most common sce-
60 narios in engineering is where the two uncertainties mentioned above exist simultaneously. Therefore,
61 the development of practical methods for hybrid uncertainty propagation analysis needs to be focused.
62 Jiang et al. [22] reviewed four main research directions in probability-interval hybrid uncertainty anal-
63 ysis. Pedroni et al. [23] applied the joint hierarchical propagation of hybrid uncertainty to a model
64 for the risk-based design of a flood protection dike. In the work of Wang and Matthies [24–26], some
65 uncertain models and numerical computing methods were presented for hybrid uncertainty propagation
66 analysis. Dang et al. [27] developed a Bayesian framework for propagating hybrid uncertainties. Long
67 et al. [28] presented a unified framework to address the hybrid uncertainty problems under four types
68 of uncertainties, i.e., probabilistic, evidence, fuzzy and interval uncertainties. Despite the significant
69 progress mentioned above, research on hybrid uncertainty analysis methods is still at a preliminary
70 stage, and most research considers only two types of uncertainties. Due to the increasing complexity
71 of structures, efficient methods that can accommodate more than two types of uncertainties for hybrid
72 uncertainty analysis are desirable.

73 Although the surrogate model is widely used in uncertainty analysis, the computational burden of
74 constructing a surrogate model can still be heavy when a single simulation is extremely time-consuming.
75 Furthermore, even resorting to surrogate model, hybrid uncertainty propagation is still generally per-
76 formed using numerical methods, which inevitably introduce post-processing errors. To avoid the post-
77 processing errors, Shi et al. [29] derived the analytical solutions of the output mean and variance based
78 on the Kriging model for RDO. Chen et al. [30] proposed an adaptive method for uncertainty analy-

79 sis based on the Kriging model associated with analytical solutions of the output mean and variance.
80 However, the above methods are not applicable to uncertainty propagation for multi-fidelity models,
81 and the above methods cannot deal with hybrid uncertainty problems. Co-Kriging [31, 32], as a typical
82 multi-fidelity surrogate model, can make a good trade-off between accuracy and efficiency. Based on the
83 Co-Kriging model, this paper aims to develop a fully decoupled adaptive method for hybrid uncertainty
84 propagation analysis involving three types of uncertainties, i.e., random, interval and fuzzy variables.
85 The novelty of this study can be summarized as follows. First, based on the Co-Kriging model, the
86 analytical solutions for the output mean and the output variance are derived, which can be computed
87 efficiently without additional simulation. These analytical solutions are still random variables, and are
88 explicit functions with respect to epistemic variables. Second, a new adaptive framework for hybrid
89 uncertainty propagation is established in which the variance of the output mean is also analytically
90 derived to measure the modeling uncertainty and enable active learning. In this framework, update
91 samples are determined sequentially for high-fidelity (HF) and low-fidelity (LF) simulation. Third,
92 two new convergence criteria are designed to terminate the adaptive process when a desired level of
93 accuracy for the bounds on the output mean and the output variance is achieved. To the best of our
94 knowledge, these analytical solutions have not been derived before. The proposed method requires only
95 a few samples to compute the analytical solutions of the output mean and output variance, and can
96 avoid the post-processing errors in hybrid uncertainty propagation analysis.

97 The outline of this paper is as follows. Section 2 provides a detailed formulation of the problem
98 considered in this paper. Then, a fully decoupled adaptive method for hybrid uncertainty propagation
99 analysis is presented in Section 3. Four case studies are investigated in Section 4 to demonstrate the
100 effectiveness and efficiency of the proposed method. Finally, the conclusions are given in Section 5.

101 **2. Formulation of the problem**

102 In traditional uncertainty propagation analysis, only random variables are employed to measure
103 the input uncertainty of structures. Nonetheless, when hybrid uncertainties are present in structures,

104 the uncertainty analysis becomes more complicated. In this study, we address the hybrid uncertainty
 105 propagation with the coexistence of three distinct types of input uncertainties, namely, random, interval,
 106 and fuzzy variables.

107 *2.1. Interval and fuzzy variables*

108 Generally, a large number of samples is required to obtain the exact probability distribution of the
 109 input parameter, but in practice this is difficult to achieve due to the huge computational or economic
 110 burden. In fact, closed intervals (i.e., the range of variation), which are easier to obtain, are often used
 111 to represent uncertain parameters in many cases. Remarkably, there is no assumption of probability
 112 distribution for interval variables, of which the bounds are determined based on engineering experience.
 113 The interval variable Y is defined as follows [33]:

$$Y \in [Y^L, Y^U], \quad Y^m = \frac{Y^L + Y^U}{2}, \quad Y^r = \frac{Y^U - Y^L}{2} \quad (1)$$

114 where Y^L , Y^U , Y^m and Y^r denote the lower bound, the upper bound, the midpoint, and the radius of
 115 Y , respectively.

116 Fuzzy variables are related to fuzzy sets which are first introduced by Zadeh [34]. Let Z be a fuzzy
 117 variable, which is a set mathematically defined by the following pair:

$$Z = \{\langle z, m(z) \rangle | z \in \Omega, m(z) \in [0, 1]\} \quad (2)$$

118 where z is the general elements of the fuzzy set, Ω is the definition domain of the fuzzy set, and
 119 $m(z) : \Omega \rightarrow [0, 1]$ is the membership function. It should be noted that the value of $m(z)$ represents the
 120 membership degree of z in the fuzzy set. In other words, it represents the degree of possibility that the
 121 fuzzy variable takes the value of z . $m(z) = 0$ means that element z is not included in the fuzzy set,
 122 while $m(z) = 1$ means that element z is fully included in the fuzzy set. $m(z)$ between 0 and 1 means
 123 that element z is partially included in the fuzzy set.

124 The α -cut approach plays an important role in the implementation of fuzzy arithmetic. Given a cut

125 level α , the α -cut of a fuzzy set can be denoted as [35]:

$$Z_\alpha = \{z \mid m(z) \geq \alpha, z \in \Omega, 0 \leq \alpha \leq 1\} \quad (3)$$

126 which is a set consisting of the elements z whose membership values $m(z)$ are equal to or greater than
 127 the cut level α . For a certain cut level α , the corresponding set Z_α can be regarded as an interval
 128 variable Z_α^I :

$$Z_\alpha^I = [Z_\alpha^L, Z_\alpha^U] = \{z \in \Omega \mid Z_\alpha^L \leq z \leq Z_\alpha^U\} \quad (4)$$

129 where Z_α^L and Z_α^U represent the lower and upper bounds of Z_α^I , respectively. There are various types
 130 of membership functions that define distinct forms of fuzzy variables, and the triangular membership
 131 function is used in this paper. The triangular membership function is described by piecewise linear
 132 segments:

$$m(z) = \begin{cases} \frac{z-a}{b-a} & \text{if } a \leq z \leq b \\ \frac{c-z}{c-b} & \text{if } b \leq z \leq c \\ 0 & \text{otherwise} \end{cases} \quad (5)$$

133 Intuitively, Fig. 1 shows a triangular membership function and the α -cut interval Z_α^I . In this context,
 134 fuzzy sets can be seen as a generalization of interval variables, and both of them are usually used to
 describe epistemic uncertainty.

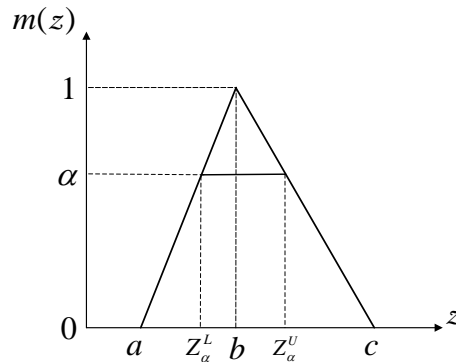


Figure 1: Diagram of the triangular membership function of fuzzy variable Z

137 For a hybrid uncertainty problem, there are multiple types of variables, and the relationship between
 138 the input parameters and the response of interest can be described by the performance function g :

$$G = g(\mathbf{X}, \mathbf{Y}, \mathbf{Z}) \quad (6)$$

139 where G denotes the response of interest, $\mathbf{X} = [X_1, X_2, \dots, X_{n_{\mathbf{X}}}]^T$ is the $n_{\mathbf{X}}$ -dimensional input vector of
 140 random variables, $\mathbf{Y} = [Y_1, Y_2, \dots, Y_{n_{\mathbf{Y}}}]^T$ denotes the $n_{\mathbf{Y}}$ -dimensional input vector of interval variables,
 141 and $\mathbf{Z} = [Z_1, Z_2, \dots, Z_{n_{\mathbf{Z}}}]^T$ denotes the $n_{\mathbf{Z}}$ -dimensional input vector of fuzzy variables. In this setting,
 142 the uncertainties in the inputs are propagated to the response G , which is also a random variable under
 143 arbitrary values of interval and fuzzy variables. In engineering practice, it is usually difficult to obtain
 144 the exact probability density function (PDF) of the response because the input random variables may
 145 follow different types of distributions and the performance function is often nonlinear.

146 In this study, the primary objective is to assess the effect of uncertainties in the inputs on the
 147 response G through the analytical expressions of the output mean $u_g(\mathbf{y}, \mathbf{z})$ and the output variance
 148 $\sigma_g^2(\mathbf{y}, \mathbf{z})$, which are functions of the values of interval and fuzzy variables:

$$u_g(\mathbf{y}, \mathbf{z}) = \int_{\Omega_{\mathbf{X}}} g(\mathbf{x}, \mathbf{y}, \mathbf{z}) f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x} \quad (7)$$

$$149 \quad \sigma_g^2(\mathbf{y}, \mathbf{z}) = \int_{\Omega_{\mathbf{X}}} [g(\mathbf{x}, \mathbf{y}, \mathbf{z}) - u_g(\mathbf{y}, \mathbf{z})]^2 f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x} \quad (8)$$

150 where $f_{\mathbf{X}}(\mathbf{x})$ is the joint PDF, $\Omega_{\mathbf{X}}$ denotes the value domain of \mathbf{X} , and $\mathbf{x}, \mathbf{y}, \mathbf{z}$ are the realization of
 151 $\mathbf{X}, \mathbf{Y}, \mathbf{Z}$, respectively. Furthermore, due to the presence of interval and fuzzy variables, the output
 152 mean $u_g(\mathbf{y}, \mathbf{z})$ and the output variance $\sigma_g^2(\mathbf{y}, \mathbf{z})$ are no longer crisp values, but intervals at each cut
 153 level α .

154 3. The proposed method

155 3.1. Performance approximation with Co-Kriging

156 As an extension of Kriging, Co-Kriging has attracted a great deal of attention in the field of engi-
 157 neering [36, 37]. It is a multi-fidelity surrogate model that combines the HF and LF models to provide
 158 a trade-off between accuracy and efficiency. The conventional single-fidelity Kriging model requires
 159 that all samples are from the HF model, where computational burden is still a limitation when the
 160 simulation is extremely time-consuming. In this regard, Co-Kriging uses a limited number of expensive
 161 HF samples and more relatively cheap LF samples to construct a multi-fidelity model. Denote the
 162 model input as $\boldsymbol{\xi}$, and the Co-Kriging prediction can be expressed as [38]:

$$S_e(\boldsymbol{\xi}) = \rho S_c(\boldsymbol{\xi}) + S_d(\boldsymbol{\xi}) \quad (9)$$

163 where $S_c(\boldsymbol{\xi})$ denotes the LF Kriging prediction, $S_d(\boldsymbol{x})$ denotes Kriging model of the difference between
 164 HF and LF model predictions, and ρ is a scaling factor. Let $\mathbf{D}_c = (\boldsymbol{\xi}_c^{(1)}, \boldsymbol{\xi}_c^{(2)}, \dots, \boldsymbol{\xi}_c^{(n_c)})^T$ denote an
 165 n_c -by- n matrix consisting of n_c LF samples whose responses are $\mathbf{y}_c = (y_c^{(1)}, y_c^{(2)}, \dots, y_c^{(n_c)})^T$, $\mathbf{D}_e =$
 166 $(\boldsymbol{\xi}_e^{(1)}, \boldsymbol{\xi}_e^{(2)}, \dots, \boldsymbol{\xi}_e^{(n_e)})^T$ denote an n_e -by- n matrix consisting of n_e HF samples whose responses are $\mathbf{y}_e =$
 167 $(y_e^{(1)}, y_e^{(2)}, \dots, y_e^{(n_e)})^T$, and n is the dimension of the sample points. The covariance matrix of Co-Kriging
 168 is expressed in block form as:

$$\mathbf{C} = \begin{bmatrix} \sigma_c^2 \boldsymbol{\Psi}_c(\mathbf{D}_c, \mathbf{D}_c) & \rho \sigma_c^2 \boldsymbol{\Psi}_c(\mathbf{D}_c, \mathbf{D}_e) \\ \rho \sigma_c^2 \boldsymbol{\Psi}_c(\mathbf{D}_e, \mathbf{D}_c) & \rho^2 \sigma_c^2 \boldsymbol{\Psi}_c(\mathbf{D}_e, \mathbf{D}_e) + \sigma_d^2 \boldsymbol{\Psi}_d(\mathbf{D}_e, \mathbf{D}_e) \end{bmatrix} \quad (10)$$

169 where σ_c^2 and σ_d^2 are the process variances of the LF and HF Kriging models, respectively, $\boldsymbol{\Psi}_c$ and $\boldsymbol{\Psi}_d$
 170 are the correlation matrix of LF and HF Kriging models, respectively. Based on the LF Kriging model
 171 constructed from \mathbf{D}_c and \mathbf{y}_c , σ_c^2 and $\boldsymbol{\Psi}_c$ can be obtained by the maximum likelihood estimation (MLE),
 172 while σ_d^2 and $\boldsymbol{\Psi}_d$ are obtained based on the difference Kriging model. To this end, the difference \mathbf{d} is
 173 defined as:

$$\mathbf{d} = \mathbf{y}_e - \rho \mathbf{y}_c(\mathbf{D}_e) \quad (11)$$

174 where $\mathbf{y}_c(\mathbf{D}_e)$ denotes the responses of LF model at samples \mathbf{D}_e . Then, σ_d^2 and Ψ_d can be determined
 175 based on the difference Kriging model constructed from \mathbf{D}_e and \mathbf{d} .

176 After all parameters are estimated, at an arbitrary unknown point $\boldsymbol{\xi}$, the prediction of Co-Kriging
 177 is available, which is a random variable. The mean value can be expressed as follows:

$$\hat{y}_e(\boldsymbol{\xi}) = \hat{\mu} + \mathbf{c}_{(\boldsymbol{\xi})}^T \mathbf{C}^{-1} (\mathbf{y}^* - \mathbf{1}\hat{\mu}) \quad (12)$$

178 where

$$\hat{\mu} = \frac{\mathbf{1}^T \mathbf{C}^{-1} \mathbf{y}^*}{\mathbf{1}^T \mathbf{C}^{-1} \mathbf{1}} \quad (13)$$

179

$$\mathbf{c}_{(\boldsymbol{\xi})} = \begin{bmatrix} \rho\sigma_c^2\psi_c(\mathbf{D}_c, \boldsymbol{\xi}) \\ \rho^2\sigma_c^2\psi_c(\mathbf{D}_e, \boldsymbol{\xi}) + \sigma_d^2\psi_d(\mathbf{D}_e, \boldsymbol{\xi}) \end{bmatrix} \quad (14)$$

180 $\mathbf{y}^* = [\mathbf{y}_c^T, \mathbf{y}_e^T]^T$ is the response vector of LF and HF samples, and ψ refers to a column vector of
 181 correlations between samples and $\boldsymbol{\xi}$. Note that the subscripts $\langle c \rangle$, $\langle e \rangle$ and $\langle d \rangle$ in this paper indicate
 182 whether the parameters used are from the LF, HF, or difference Kriging models, respectively. The
 183 variance of the prediction is expressed as:

$$s_e^2(\boldsymbol{\xi}) = \rho^2\sigma_c^2 + \sigma_d^2 - \mathbf{c}_{(\boldsymbol{\xi})}^T \mathbf{C}^{-1} \mathbf{c}_{(\boldsymbol{\xi})} \quad (15)$$

184 The reader can refer to [31] for more details about the derivation. In this study, the Gaussian correlation
 185 function shown below is used:

$$\psi_\theta(\boldsymbol{\xi}, \boldsymbol{\xi}') = \exp \left\{ - \sum_{k=1}^n \theta^{(k)} \left(\xi^{(k)} - \xi'^{(k)} \right)^2 \right\} \quad (16)$$

186 where $\theta^{(k)}$ ($k = 1, 2, \dots, n$) are the correlation parameters.

187 3.2. Uncertainty Propagation Solution of Output Mean

188 In this method, if the input random variables do not follow normal distributions, an isoprobabilistic
 189 transformation should first be applied to transform the original input variables into independent ones
 190 in standardized normal space, i.e., $\mathbf{U} = T(\mathbf{X})$, where $\mathbf{U} = [U_1, U_2, \dots, U_{n_x}]^T$ is the vector of standard

191 normal variables. Then, Eq. (6) can be rewritten as follows:

$$G = g(T^{-1}(\mathbf{U}), \mathbf{Y}, \mathbf{Z}) = \mathcal{G}(\mathbf{U}, \mathbf{Y}, \mathbf{Z}) \quad (17)$$

192 Two types of transformations can be used, the Rosenblatt and Nataf transformations [39, 40]. For
 193 convenience of expression, let $\mathbf{W} = [\mathbf{U}^T, \mathbf{Y}^T, \mathbf{Z}^T]$ and $\mathbf{P} = [\mathbf{Y}^T, \mathbf{Z}^T]$. Because the output mean and
 194 the output variance are functions of \mathbf{y} and \mathbf{z} , the Gaussian correlation function (as shown in Eq. (16))
 195 of LF Kriging model can be rewritten as follows:

$$\begin{aligned} \psi_c(\mathbf{w}, \mathbf{w}') &= \exp \left\{ - \sum_{k=1}^{n_{\mathbf{X}}} \theta_c^{(k)} \left(u^{(k)}, u'^{(k)} \right)^2 - \sum_{k=1}^{n_{\mathbf{Y}}+n_{\mathbf{Z}}} \theta_c^{(n_{\mathbf{X}}+k)} \left(p^{(k)}, p'^{(k)} \right)^2 \right\} \\ &= \exp \left\{ - \sum_{k=1}^{n_{\mathbf{X}}} \theta_c^{(k)} \left(u^{(k)}, u'^{(k)} \right)^2 \right\} \exp \left\{ - \sum_{k=1}^{n_{\mathbf{Y}}+n_{\mathbf{Z}}} \theta_c^{(n_{\mathbf{X}}+k)} \left(p^{(k)}, p'^{(k)} \right)^2 \right\} \\ &= \gamma_{uc}(\mathbf{u}, \mathbf{u}') \gamma_{pc}(\mathbf{p}, \mathbf{p}') \end{aligned} \quad (18)$$

196 where \mathbf{w} and \mathbf{w}' are two arbitrary realizations of \mathbf{W} , \mathbf{u} and \mathbf{u}' are two arbitrary realizations of \mathbf{U} , \mathbf{p}
 197 and \mathbf{p}' are two arbitrary realizations of \mathbf{P} . Similarly, the correlation function of the difference Kriging
 198 model can be expressed as follows:

$$\begin{aligned} \psi_d(\mathbf{w}, \mathbf{w}') &= \exp \left\{ - \sum_{k=1}^{n_{\mathbf{X}}} \theta_d^{(k)} \left(u^{(k)}, u'^{(k)} \right)^2 \right\} \exp \left\{ - \sum_{k=1}^{n_{\mathbf{Y}}+n_{\mathbf{Z}}} \theta_d^{(n_{\mathbf{X}}+k)} \left(p^{(k)}, p'^{(k)} \right)^2 \right\} \\ &= \gamma_{ud}(\mathbf{u}, \mathbf{u}') \gamma_{pd}(\mathbf{p}, \mathbf{p}') \end{aligned} \quad (19)$$

199 In this setting, the matrices of LF and HF training samples are $\mathbf{D}_c = (\mathbf{w}_c^{(1)}, \mathbf{w}_c^{(2)}, \dots, \mathbf{w}_c^{(n_c)})^T$ and
 200 $\mathbf{D}_e = (\mathbf{w}_e^{(1)}, \mathbf{w}_e^{(2)}, \dots, \mathbf{w}_e^{(n_e)})^T$, respectively. Then, we employ the mean of Co-Kriging prediction $\hat{y}_e(\mathbf{w})$
 201 to replace the real response G to obtain the analytical expression of the output mean $u_g(\mathbf{y}, \mathbf{z})$. It should
 202 be noted that $u_g(\mathbf{y}, \mathbf{z})$ is also a random variable after the replacement, whose mean $m_{\hat{g}}(\mathbf{y}, \mathbf{z})$ can be
 203 estimated by substituting Eqs. (12), (18) and (19) into Eq. (7):

$$\begin{aligned} m_{\hat{g}}(\mathbf{y}, \mathbf{z}) &= \int_{\Omega_U} [\hat{\mu} + \mathbf{c}_{(w)}^T \mathbf{C}^{-1} (\mathbf{y}^* - \mathbf{1}\hat{\mu})] f_U(\mathbf{u}) d\mathbf{u} \\ &= \hat{\mu} + \left\{ \int_{\Omega_U} \mathbf{c}_{(w)}^T f_U(\mathbf{u}) d\mathbf{u} \right\} \mathbf{F}_c \end{aligned} \quad (20)$$

204 where

$$\mathbf{F}_c = [\mathbf{C}^{-1} (\mathbf{y}^* - \mathbf{1}\hat{\mu})] \quad (21)$$

205

$$\begin{aligned} \mathbf{c}_{(\mathbf{w})} &= \begin{bmatrix} \rho\sigma_c^2\psi_c(\mathbf{D}_c, \mathbf{w}) \\ \rho^2\sigma_c^2\psi_c(\mathbf{D}_e, \mathbf{w}) + \sigma_d^2\psi_d(\mathbf{D}_e, \mathbf{w}) \end{bmatrix} \\ &= \begin{bmatrix} \rho\sigma_c^2\gamma_{uc}(\mathbf{u}_c^{(1)}, \mathbf{u})\gamma_{pc}(\mathbf{p}_c^{(1)}, \mathbf{p}) \\ \rho\sigma_c^2\gamma_{uc}(\mathbf{u}_c^{(2)}, \mathbf{u})\gamma_{pc}(\mathbf{p}_c^{(2)}, \mathbf{p}) \\ \vdots \\ \rho\sigma_c^2\gamma_{uc}(\mathbf{u}_c^{(n_c)}, \mathbf{u})\gamma_{pc}(\mathbf{p}_c^{(n_c)}, \mathbf{p}) \\ \rho^2\sigma_c^2\gamma_{uc}(\mathbf{u}_e^{(1)}, \mathbf{u})\gamma_{pc}(\mathbf{p}_e^{(1)}, \mathbf{p}) + \sigma_d^2\gamma_{ud}(\mathbf{u}_e^{(1)}, \mathbf{u})\gamma_{pd}(\mathbf{p}_e^{(1)}, \mathbf{p}) \\ \vdots \\ \rho^2\sigma_c^2\gamma_{uc}(\mathbf{u}_e^{(n_e)}, \mathbf{u})\gamma_{pc}(\mathbf{p}_e^{(n_e)}, \mathbf{p}) + \sigma_d^2\gamma_{ud}(\mathbf{u}_e^{(n_e)}, \mathbf{u})\gamma_{pd}(\mathbf{p}_e^{(n_e)}, \mathbf{p}) \end{bmatrix} \end{aligned} \quad (22)$$

206 Ω_U denotes the value domain of \mathbf{U} , and $f_U(\mathbf{u})$ is the joint PDF of \mathbf{U} with the corresponding mean
207 vector and covariance matrix being \mathbf{b} and \mathbf{B} , respectively.

208 To calculate the integral in Eq. (20), rewrite the vector $\mathbf{c}_{(\mathbf{w})}$ into two parts, where $\gamma_c^{(i)}$ ($i = 1, 2, \dots, n_c$)
209 are the first n_c elements in $\mathbf{c}_{(\mathbf{w})}$, and $\gamma_e^{(j)}$ ($j = 1, 2, \dots, n_e$) are the last n_e elements in $\mathbf{c}_{(\mathbf{w})}$. Then,
210 $\gamma_c^{(i)} f_U(\mathbf{u})$ ($i = 1, 2, \dots, n_c$) can be expressed as follows:

$$\gamma_c^{(i)} f_U(\mathbf{u}) = \rho\sigma_c^2 (2\pi)^{\frac{n}{2}} |\mathbf{A}_c|^{\frac{1}{2}} f_{cc}^{(i)}(\mathbf{u}) f_U(\mathbf{u}) \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \quad (23)$$

211 where

$$f_{cc}^{(i)}(\mathbf{u}) = (2\pi)^{-\frac{n}{2}} |\mathbf{A}_c|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_c^{(i)} - \mathbf{u})^\top \mathbf{A}_c^{-1} (\mathbf{u}_c^{(i)} - \mathbf{u}) \right\} \quad (24)$$

212 and $\mathbf{A}_c = \text{diag} \left(\frac{1}{2\theta_c^{(1)}}, \frac{1}{2\theta_c^{(2)}}, \dots, \frac{1}{2\theta_c^{(n_x)}} \right)$. Similarly, $\gamma_e^{(j)} f_U(\mathbf{u})$ ($j = 1, 2, \dots, n_e$) can be expressed as follows:

$$\gamma_e^{(j)} f_U(\mathbf{u}) = (2\pi)^{\frac{n}{2}} \left(\rho^2\sigma_c^2 |\mathbf{A}_c|^{\frac{1}{2}} f_{ce}^{(j)}(\mathbf{u}) \gamma_{pc}(\mathbf{p}_e^{(j)}, \mathbf{p}) + \sigma_d^2 |\mathbf{A}_d|^{\frac{1}{2}} f_{de}^{(j)}(\mathbf{u}) \gamma_{pd}(\mathbf{p}_e^{(j)}, \mathbf{p}) \right) f_U(\mathbf{u}) \quad (25)$$

213 where

$$f_{ce}^{(j)}(\mathbf{u}) = (2\pi)^{-\frac{n}{2}} |\mathbf{A}_c|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_e^{(j)} - \mathbf{u})^\top \mathbf{A}_c^{-1} (\mathbf{u}_e^{(j)} - \mathbf{u}) \right\} \quad (26)$$

214

$$f_{de}^{(j)}(\mathbf{u}) = (2\pi)^{-\frac{n}{2}} |\mathbf{A}_d|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_e^{(j)} - \mathbf{u})^\top \mathbf{A}_d^{-1} (\mathbf{u}_e^{(j)} - \mathbf{u}) \right\} \quad (27)$$

215 and $\mathbf{A}_d = \text{diag} \left(\frac{1}{2\theta_d^{(1)}}, \frac{1}{2\theta_d^{(2)}}, \dots, \frac{1}{2\theta_d^{(n_x)}} \right)$, respectively. $f_{cc}^{(i)}(\mathbf{u})$, $f_{ce}^{(j)}(\mathbf{u})$, $f_{de}^{(j)}(\mathbf{u})$ and $f_U(\mathbf{u})$ are four

216 joint Gaussian PDFs about the n_x -dimension random variable \mathbf{U} , and the product of two Gaus-

217 sian PDFs generates another un-normalized Gaussian PDF [41]. Accordingly, the three products, i.e.,

218 $f_{cc}^{(i)}(\mathbf{u}) f_U(\mathbf{u})$, $f_{ce}^{(j)}(\mathbf{u}) f_U(\mathbf{u})$, and $f_{de}^{(j)}(\mathbf{u}) f_U(\mathbf{u})$ can be derived as follows [41]:

$$f_{cc}^{(i)}(\mathbf{u}) f_U(\mathbf{u}) = (2\pi)^{-\frac{n}{2}} |\mathbf{A}_c + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_c^{(i)} - \mathbf{b})^\top (\mathbf{A}_c + \mathbf{B})^{-1} (\mathbf{u}_c^{(i)} - \mathbf{b}) \right\} f'_U(\mathbf{u}) \quad (28)$$

219

$$f_{ce}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) = (2\pi)^{-\frac{n}{2}} |\mathbf{A}_c + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_e^{(j)} - \mathbf{b})^\top (\mathbf{A}_c + \mathbf{B})^{-1} (\mathbf{u}_e^{(j)} - \mathbf{b}) \right\} f''_U(\mathbf{u}) \quad (29)$$

220

$$f_{de}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) = (2\pi)^{-\frac{n}{2}} |\mathbf{A}_d + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_e^{(j)} - \mathbf{b})^\top (\mathbf{A}_d + \mathbf{B})^{-1} (\mathbf{u}_e^{(j)} - \mathbf{b}) \right\} f'''_U(\mathbf{u}) \quad (30)$$

221 where $f'_U(\mathbf{u})$, $f''_U(\mathbf{u})$ and $f'''_U(\mathbf{u})$ are also joint Gaussian PDFs with the mean vectors $\bar{\mathbf{u}}'$, $\bar{\mathbf{u}}''$, $\bar{\mathbf{u}}'''$ and

222 covariance matrices \mathbf{Q}' , \mathbf{Q}'' , \mathbf{Q}''' , in which $\mathbf{Q}' = \mathbf{Q}'' = (\mathbf{A}_c^{-1} + \mathbf{B}^{-1})^{-1}$, $\mathbf{Q}''' = (\mathbf{A}_d^{-1} + \mathbf{B}^{-1})^{-1}$, $\bar{\mathbf{u}}' =$

223 $\mathbf{Q}' (\mathbf{A}_c^{-1} \mathbf{u}_c^{(i)} + \mathbf{B}^{-1} \mathbf{b})$, $\bar{\mathbf{u}}'' = \mathbf{Q}'' (\mathbf{A}_c^{-1} \mathbf{u}_e^{(j)} + \mathbf{B}^{-1} \mathbf{b})$, and $\bar{\mathbf{u}}''' = \mathbf{Q}''' (\mathbf{A}_d^{-1} \mathbf{u}_e^{(j)} + \mathbf{B}^{-1} \mathbf{b})$, respectively.

224 Substituting Eq. (28) into Eq. (23), Eq. (29) and (30) into Eq. (25), the integral in Eq. (20) can

225 be obtained by:

$$\begin{aligned} \int_{\Omega_U} \mathbf{c}_{(w)}^\top f_U(\mathbf{u}) d\mathbf{u} &= [\beta_c^{(1)}, \beta_c^{(2)}, \dots, \beta_c^{(n_c)}, \beta_e^{(1)}, \beta_e^{(2)}, \dots, \beta_e^{(n_e)}] \\ &= [\beta_c^{(i)}, \beta_e^{(j)}] \quad (i = 1, 2, \dots, n_c; j = 1, 2, \dots, n_e) \\ &= \boldsymbol{\beta} \end{aligned} \quad (31)$$

226 where

$$\beta_c^{(i)} = \rho \sigma_c^2 |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_c + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_c^{(i)} - \mathbf{b})^\top (\mathbf{A}_c + \mathbf{B})^{-1} (\mathbf{u}_c^{(i)} - \mathbf{b}) \right\} \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \quad (32)$$

$$\begin{aligned} \boldsymbol{\beta}_e^{(j)} = & \rho^2 \sigma_c^2 |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_c + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_e^{(j)} - \mathbf{b})^\top (\mathbf{A}_c + \mathbf{B})^{-1} (\mathbf{u}_e^{(j)} - \mathbf{b}) \right\} \gamma_{pc} (\mathbf{p}_e^{(j)}, \mathbf{p}) \\ & + \sigma_d^2 |\mathbf{A}_d|^{\frac{1}{2}} |\mathbf{A}_d + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_e^{(j)} - \mathbf{b})^\top (\mathbf{A}_d + \mathbf{B})^{-1} (\mathbf{u}_e^{(j)} - \mathbf{b}) \right\} \gamma_{pd} (\mathbf{p}_e^{(j)}, \mathbf{p}) \end{aligned} \quad (33)$$

Substituting Eq. (31) into Eq. (20), the analytical solution of $m_{\hat{g}}(\mathbf{y}, \mathbf{z})$ can be estimated as follows:

$$m_{\hat{g}}(\mathbf{y}, \mathbf{z}) = \hat{\mu} + \boldsymbol{\beta} \mathbf{F}_c \quad (34)$$

It should be pointed out that all parameters in Eq. (34) are available based on the constructed Co-Kriging model. Given a value of \mathbf{p} (i.e., (\mathbf{y}, \mathbf{z})), the mean of the performance function can be estimated analytically.

In the above derivation, the mean of $u_g(\mathbf{y}, \mathbf{z})$ is derived by replacing the real response G with the mean of the Co-Kriging prediction $\hat{g}_e(\mathbf{w})$, where epistemic uncertainty is introduced. In the following text, we will also derive the analytical solution of the variance of $u_g(\mathbf{y}, \mathbf{z})$, which is adopted to measure the epistemic uncertainty in $u_g(\mathbf{y}, \mathbf{z})$.

The variance of $u_g(\mathbf{y}, \mathbf{z})$ is defined as follows:

$$\begin{aligned} s_{\hat{g}}^2(\mathbf{y}, \mathbf{z}) &= \int_{\Omega_{\hat{g}}} \left[\int_{\Omega_U} \hat{g}(\mathbf{u}, \mathbf{y}, \mathbf{z}) f_U(\mathbf{u}) d\mathbf{u} - m_{\hat{g}}(\mathbf{y}, \mathbf{z}) \right]^2 f(\hat{g}) d\hat{g} \\ &= \int_{\Omega_{\hat{g}}} \left[\int_{\Omega_U} [\hat{g}(\mathbf{u}, \mathbf{y}, \mathbf{z}) - m_{\hat{g}}(\mathbf{y}, \mathbf{z})] f_U(\mathbf{u}) d\mathbf{u} \right. \\ &\quad \left. \int_{\Omega_{U'}} [\hat{g}(\mathbf{u}', \mathbf{y}, \mathbf{z}) - m_{\hat{g}}(\mathbf{y}, \mathbf{z})] f_{U'}(\mathbf{u}') d\mathbf{u}' \right] f(\hat{g}) d\hat{g} \\ &= \int_{\Omega_U} \int_{\Omega_{U'}} \text{cov}((\mathbf{u}, \mathbf{y}, \mathbf{z}), (\mathbf{u}', \mathbf{y}, \mathbf{z})) f_U(\mathbf{u}) f_{U'}(\mathbf{u}') d\mathbf{u} d\mathbf{u}' \end{aligned} \quad (35)$$

where $\hat{g}(\mathbf{u}, \mathbf{y}, \mathbf{z})$ is the Co-Kriging model approximation of G , $\Omega_{\hat{g}}$ and $f(\hat{g})$ denote the value domain and the PDF of \hat{g} . Based on Eq. (15), the prediction covariance $\text{cov}(\mathbf{w}, \mathbf{w}')$ is expressed below:

$$\text{cov}(\mathbf{w}, \mathbf{w}') = \rho^2 \sigma_c^2 \psi_c(\mathbf{w}, \mathbf{w}') + \sigma_d^2 \psi_d(\mathbf{w}, \mathbf{w}') - \mathbf{c}_{(\mathbf{w})}^\top \mathbf{C}^{-1} \mathbf{c}_{(\mathbf{w}')} \quad (36)$$

239 Substituting Eqs. (18), (19), (31) and (36) into Eq. (35), $s_g^2(\mathbf{y}, \mathbf{z})$ can be rewritten as follows:

$$s_g^2(\mathbf{y}, \mathbf{z}) = \rho^2 \sigma_c^2 \int_{\Omega_U} \int_{\Omega_{U'}} \gamma_{uc}(\mathbf{u}, \mathbf{u}') f_U(\mathbf{u}) f_{U'}(\mathbf{u}') d\mathbf{u} d\mathbf{u}' + \sigma_d^2 \int_{\Omega_U} \int_{\Omega_{U'}} \gamma_{ud}(\mathbf{u}, \mathbf{u}') f_U(\mathbf{u}) f_{U'}(\mathbf{u}') d\mathbf{u} d\mathbf{u}' - \boldsymbol{\beta} \mathbf{C}^{-1} \boldsymbol{\beta}^T \quad (37)$$

240 in which $\int_{\Omega_U} \int_{\Omega_{U'}} \gamma_{uc}(\mathbf{u}, \mathbf{u}') f_U(\mathbf{u}) f_{U'}(\mathbf{u}') d\mathbf{u} d\mathbf{u}'$ and $\int_{\Omega_U} \int_{\Omega_{U'}} \gamma_{ud}(\mathbf{u}, \mathbf{u}') f_U(\mathbf{u}) f_{U'}(\mathbf{u}') d\mathbf{u} d\mathbf{u}'$ are given
241 as [42, 43]:

$$\int_{\Omega_U} \int_{\Omega_{U'}} \gamma_{uc}(\mathbf{u}, \mathbf{u}') f_U(\mathbf{u}) f_{U'}(\mathbf{u}') d\mathbf{u} d\mathbf{u}' = |2\mathbf{A}_c^{-1} \mathbf{B} + \mathbf{I}|^{-\frac{1}{2}} \quad (38)$$

$$\int_{\Omega_U} \int_{\Omega_{U'}} \gamma_{ud}(\mathbf{u}, \mathbf{u}') f_U(\mathbf{u}) f_{U'}(\mathbf{u}') d\mathbf{u} d\mathbf{u}' = |2\mathbf{A}_d^{-1} \mathbf{B} + \mathbf{I}|^{-\frac{1}{2}} \quad (39)$$

242 Finally, the analytical solution of $s_g^2(\mathbf{y}, \mathbf{z})$ is obtained as follows:

$$s_g^2(\mathbf{y}, \mathbf{z}) = \rho^2 \sigma_c^2 |2\mathbf{A}_c^{-1} \mathbf{B} + \mathbf{I}|^{-\frac{1}{2}} + \sigma_d^2 |2\mathbf{A}_d^{-1} \mathbf{B} + \mathbf{I}|^{-\frac{1}{2}} - \boldsymbol{\beta} \mathbf{C}^{-1} \boldsymbol{\beta}^T \quad (40)$$

244 3.3. Uncertainty Propagation Solution of Output Variance

245 In order to obtain the analytical solution of the output variance $\sigma_g^2(\mathbf{y}, \mathbf{z})$ defined in Eq. (8), we still
246 resort to the mean of Co-Kriging prediction, and Eq. (8) can be rewritten as follows:

$$\begin{aligned} \sigma_g^2(\mathbf{y}, \mathbf{z}) &= \int_{\Omega_U} [g(\mathbf{u}, \mathbf{y}, \mathbf{z}) - u_g(\mathbf{y}, \mathbf{z})]^2 f_U(\mathbf{u}) d\mathbf{u} \\ &= \int_{\Omega_U} [g^2(\mathbf{u}, \mathbf{y}, \mathbf{z}) + u_g^2(\mathbf{y}, \mathbf{z}) - 2g(\mathbf{u}, \mathbf{y}, \mathbf{z})u_g(\mathbf{y}, \mathbf{z})] f_U(\mathbf{u}) d\mathbf{u} \\ &= \int_{\Omega_U} [g^2(\mathbf{u}, \mathbf{y}, \mathbf{z}) - u_g^2(\mathbf{y}, \mathbf{z})] f_U(\mathbf{u}) d\mathbf{u} \\ &= \int_{\Omega_U} [\hat{y}_e^2(\mathbf{u}, \mathbf{y}, \mathbf{z}) - u_g^2(\mathbf{y}, \mathbf{z})] f_U(\mathbf{u}) d\mathbf{u} \\ &= \hat{\mu}^2 + 2\hat{\mu} \boldsymbol{\beta} \mathbf{C}^{-1} \boldsymbol{\beta}^T \mathbf{F}_c - u_g^2(\mathbf{y}, \mathbf{z}) + \mathbf{F}_c^T \left[\int_{\Omega_U} \mathbf{c}_{(w)} \mathbf{c}_{(w)}^T f_U(\mathbf{u}) d\mathbf{u} \right] \mathbf{F}_c \end{aligned} \quad (41)$$

247 where $u_g^2(\mathbf{y}, \mathbf{z})$ can be estimated by Eq. (34), $\mathbf{c}_{(w)} \mathbf{c}_{(w)}^T$ is a block matrix expressed as follows:

$$\mathbf{c}_{(w)} \mathbf{c}_{(w)}^T = \begin{bmatrix} \gamma_{cc} & \gamma_{ce} \\ \gamma_{ec} & \gamma_{ee} \end{bmatrix} \quad (42)$$

248 in which γ_{cc} is an n_c -by- n_c matrix with the (i, j) -th entry $[\gamma_{cc}]_{ij} = \gamma_c^{(i)} \gamma_c^{(j)}$, γ_{ce} is an n_c -by- n_e matrix
 249 with the (i, j) -th entry $[\gamma_{ce}]_{ij} = \gamma_c^{(i)} \gamma_e^{(j)}$, γ_{ec} is the transpose matrix of γ_{ce} , and γ_{ee} is an n_e -by- n_e matrix
 250 with the (i, j) -th entry $[\gamma_{ee}]_{ij} = \gamma_e^{(i)} \gamma_e^{(j)}$.

251 Take the (i, j) -th entry of matrix γ_{cc} as an example, the resulting integral is calculated as follows:

$$\begin{aligned} \int_{\Omega_U} \gamma_c^{(i)} \gamma_c^{(j)} f_U(\mathbf{u}) d\mathbf{u} &= \left(\rho \sigma_c^2 (2\pi)^{\frac{n}{2}} |\mathbf{A}_c|^{\frac{1}{2}} \right)^2 \left[\int_{\Omega_U} f_{cc}^{(i)}(\mathbf{u}) f_{cc}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) d\mathbf{u} \right] \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \gamma_{pc}(\mathbf{p}_c^{(j)}, \mathbf{p}) \\ &= \rho^2 \sigma_c^4 |\mathbf{A}_c| H_1(\mathbf{u}_c^{(i)}) H_2(\mathbf{u}_c^{(j)}) \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \gamma_{pc}(\mathbf{p}_c^{(j)}, \mathbf{p}) \end{aligned} \quad (43)$$

252 where

$$H_1(\mathbf{u}_c^{(i)}) = |\mathbf{A}_c + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_c^{(i)} - \mathbf{b})^T (\mathbf{A}_c + \mathbf{B})^{-1} (\mathbf{u}_c^{(i)} - \mathbf{b}) \right\} \quad (44)$$

253

$$H_2(\mathbf{u}_c^{(j)}) = |\mathbf{Q}' + \mathbf{A}_c|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\bar{\mathbf{u}}' - \mathbf{u}_c^{(j)})^T (\mathbf{Q}' + \mathbf{A}_c)^{-1} (\bar{\mathbf{u}}' - \mathbf{u}_c^{(j)}) \right\} \quad (45)$$

254 Similarly, the integral of the (i, j) -th entry of matrix γ_{ce} can be obtained as follows:

$$\begin{aligned} &\int_{\Omega_U} \gamma_c^{(i)} \gamma_e^{(j)} f_U(\mathbf{u}) d\mathbf{u} \\ &= \rho^3 \sigma_c^4 (2\pi)^n |\mathbf{A}_c| \left[\int_{\Omega_U} f_{cc}^{(i)}(\mathbf{u}) f_{ce}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) d\mathbf{u} \right] \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \gamma_{pe}(\mathbf{p}_e^{(j)}, \mathbf{p}) \\ &\quad + \rho \sigma_c^2 \sigma_d^2 (2\pi)^n |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_d|^{\frac{1}{2}} \left[\int_{\Omega_U} f_{cc}^{(i)}(\mathbf{u}) f_{de}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) d\mathbf{u} \right] \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(j)}, \mathbf{p}) \quad (46) \\ &= \rho^3 \sigma_c^4 |\mathbf{A}_c| H_1(\mathbf{u}_c^{(i)}) H_2(\mathbf{u}_e^{(j)}) \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \gamma_{pe}(\mathbf{p}_e^{(j)}, \mathbf{p}) \\ &\quad + \rho \sigma_c^2 \sigma_d^2 |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_d|^{\frac{1}{2}} H_1(\mathbf{u}_c^{(i)}) H_3(\mathbf{u}_e^{(j)}) \gamma_{pc}(\mathbf{p}_c^{(i)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(j)}, \mathbf{p}) \end{aligned}$$

255 where

$$H_3(\mathbf{u}_e^{(j)}) = |\mathbf{Q}' + \mathbf{A}_d|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\bar{\mathbf{u}}' - \mathbf{u}_e^{(j)})^T (\mathbf{Q}' + \mathbf{A}_d)^{-1} (\bar{\mathbf{u}}' - \mathbf{u}_e^{(j)}) \right\} \quad (47)$$

256 Once again, the integral of the (i, j) -th entry of matrix γ_{ee} is given as follows:

$$\begin{aligned}
& \int_{\Omega_U} \gamma_e^{(i)} \gamma_e^{(j)} f_U(\mathbf{u}) d\mathbf{u} \\
&= \rho^4 \sigma_c^4 (2\pi)^n |\mathbf{A}_c| \left[\int_{\Omega_U} f_{ce}^{(i)}(\mathbf{u}) f_{ce}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) d\mathbf{u} \right] \gamma_{pc}(\mathbf{p}_e^{(i)}, \mathbf{p}) \gamma_{pc}(\mathbf{p}_e^{(j)}, \mathbf{p}) \\
&+ \rho^2 \sigma_c^2 \sigma_d^2 (2\pi)^n |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_d|^{\frac{1}{2}} \left[\int_{\Omega_U} f_{ce}^{(i)}(\mathbf{u}) f_{de}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) d\mathbf{u} \right] \gamma_{pc}(\mathbf{p}_e^{(i)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(j)}, \mathbf{p}) \\
&+ \rho^2 \sigma_c^2 \sigma_d^2 (2\pi)^n |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_d|^{\frac{1}{2}} \left[\int_{\Omega_U} f_{ce}^{(j)}(\mathbf{u}) f_{de}^{(i)}(\mathbf{u}) f_U(\mathbf{u}) d\mathbf{u} \right] \gamma_{pc}(\mathbf{p}_e^{(j)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(i)}, \mathbf{p}) \\
&+ \sigma_d^4 (2\pi)^n |\mathbf{A}_d| \left[\int_{\Omega_U} f_{de}^{(i)}(\mathbf{u}) f_{de}^{(j)}(\mathbf{u}) f_U(\mathbf{u}) d\mathbf{u} \right] \gamma_{pd}(\mathbf{p}_e^{(i)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(j)}, \mathbf{p}) \\
&= \rho^4 \sigma_c^4 |\mathbf{A}_c| H_1(\mathbf{u}_e^{(i)}) H_4(\mathbf{u}_e^{(j)}) \gamma_{pc}(\mathbf{p}_e^{(i)}, \mathbf{p}) \gamma_{pc}(\mathbf{p}_e^{(j)}, \mathbf{p}) \\
&+ \rho^2 \sigma_c^2 \sigma_d^2 |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_d|^{\frac{1}{2}} H_1(\mathbf{u}_e^{(i)}) H_5(\mathbf{u}_e^{(j)}) \gamma_{pc}(\mathbf{p}_e^{(i)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(j)}, \mathbf{p}) \\
&+ \rho^2 \sigma_c^2 \sigma_d^2 |\mathbf{A}_c|^{\frac{1}{2}} |\mathbf{A}_d|^{\frac{1}{2}} H_1(\mathbf{u}_e^{(j)}) H_5(\mathbf{u}_e^{(i)}) \gamma_{pc}(\mathbf{p}_e^{(j)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(i)}, \mathbf{p}) \\
&+ \sigma_d^4 |\mathbf{A}_d| H_6(\mathbf{u}_e^{(i)}) H_7(\mathbf{u}_e^{(j)}) \gamma_{pd}(\mathbf{p}_e^{(i)}, \mathbf{p}) \gamma_{pd}(\mathbf{p}_e^{(j)}, \mathbf{p})
\end{aligned} \tag{48}$$

257 where

$$H_4(\mathbf{u}_e^{(j)}) = |\mathbf{Q}'' + \mathbf{A}_c|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\bar{\mathbf{u}}'' - \mathbf{u}_e^{(j)})^\top (\mathbf{Q}'' + \mathbf{A}_c)^{-1} (\bar{\mathbf{u}}'' - \mathbf{u}_e^{(j)}) \right\} \tag{49}$$

258

$$H_5(\mathbf{u}_e^{(j)}) = |\mathbf{Q}'' + \mathbf{A}_d|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\bar{\mathbf{u}}'' - \mathbf{u}_e^{(j)})^\top (\mathbf{Q}'' + \mathbf{A}_d)^{-1} (\bar{\mathbf{u}}'' - \mathbf{u}_e^{(j)}) \right\} \tag{50}$$

259

$$H_6(\mathbf{u}_e^{(i)}) = |\mathbf{A}_d + \mathbf{B}|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\mathbf{u}_e^{(i)} - \mathbf{b})^\top (\mathbf{A}_d + \mathbf{B})^{-1} (\mathbf{u}_e^{(i)} - \mathbf{b}) \right\} \tag{51}$$

260

$$H_7(\mathbf{u}_e^{(j)}) = |\mathbf{Q}''' + \mathbf{A}_d|^{-\frac{1}{2}} \exp \left\{ -\frac{1}{2} (\bar{\mathbf{u}}''' - \mathbf{u}_e^{(j)})^\top (\mathbf{Q}''' + \mathbf{A}_d)^{-1} (\bar{\mathbf{u}}''' - \mathbf{u}_e^{(j)}) \right\} \tag{52}$$

261 Substituting Eqs. (43), (46) and (48) into Eq. (41) gives the analytical solution of the output variance
262 $\sigma_g^2(\mathbf{y}, \mathbf{z})$, which is an explicit function of \mathbf{p} (i.e., (\mathbf{y}, \mathbf{z})).

263 3.4. Adaptive hybrid uncertainty propagation

264 Recall that the primary goal is to estimate the output mean $u_g(\mathbf{y}, \mathbf{z})$ and the output variance
265 $\sigma_g^2(\mathbf{y}, \mathbf{z})$, where epistemic uncertainty is introduced by the Co-Kriging model prediction. Hence, the
266 active learning strategy should focus on reducing the epistemic uncertainty in $u_g(\mathbf{y}, \mathbf{z})$ and $\sigma_g^2(\mathbf{y}, \mathbf{z})$.

Based on the augmented expected improvement (AEI) function [44], an adaptive framework is established, where two stopping criteria are proposed for the single loop active learning. The analytical solutions for the mean and variance of $u_g(\mathbf{y}, \mathbf{z})$ given in Eqs. (34) and (40) are employed to facilitate the identification of new points:

$$\text{AEI}(\mathbf{p}) = (m_{\hat{g}}(\mathbf{p}^{**}) - m_{\hat{g}}(\mathbf{p})) \Phi\left(\frac{m_{\hat{g}}(\mathbf{p}^{**}) - m_{\hat{g}}(\mathbf{p})}{s_{\hat{g}}(\mathbf{p})}\right) + s_{\hat{g}}(\mathbf{p}) \varphi\left(\frac{m_{\hat{g}}(\mathbf{p}^{**}) - m_{\hat{g}}(\mathbf{p})}{s_{\hat{g}}(\mathbf{p})}\right) \quad (53)$$

where \mathbf{p}^{**} is determined by:

$$\mathbf{p}^{**} = \arg \max [-m_{\hat{g}}(\mathbf{p}) - cs_{\hat{g}}(\mathbf{p})] \quad (54)$$

with $c = 1$; $\Phi(\cdot)$ and $\varphi(\cdot)$ are the cumulative distribution function (CDF) and the PDF of the standard normal distribution, respectively.

The computational steps of active learning are elaborated as below:

Step 1: Generation of candidate sample set Ω for random variables. In this paper, the Sobol's quasi-random sequence [45] is employed to generate low-discrepancy candidate samples of size N_Ω in standard normal space.

Step 2: Construction of the Co-Kriging model based on training samples \mathbf{D}_c and \mathbf{D}_e for LF and HF models. To ensure the uniformity of the initial samples and to capture the global approximation behavior of Co-Kriging, Latin Hypercube Sampling (LHS) is performed to generate initial training samples, where the cut level α of the fuzzy variables is set to 0 for sampling. Then, the real responses \mathbf{y}_c and \mathbf{y}_e of the LF and HF models at training samples are obtained.

Step 3: Calculation of the upper and lower bounds for the output mean $u_g(\mathbf{y}, \mathbf{z})$ and the output variance $\sigma_g^2(\mathbf{y}, \mathbf{z})$ at each cut level. Based on Eqs. (34) and (41), the bounds of $u_g(\mathbf{y}, \mathbf{z})$ and $\sigma_g^2(\mathbf{y}, \mathbf{z})$ at each cut level α can be collected by discretizing interval and fuzzy variables.

Step 4: Stopping criterion. In this paper, two efficient convergence criteria are established to stop the iteration. The first stopping criterion is defined as the maximum coefficient of variation (Cov) of $u_g(\mathbf{y}, \mathbf{z})$ at the lower and upper bounds:

$$[Cov^{(1)}, Cov^{(2)}, \dots, Cov^{(n)}]_{\max} \leq e_1 \quad (55)$$

where $Cov^{(i)}$ ($i = 1, 2, \dots, n$) denote all the Cov of $u_g(\mathbf{y}, \mathbf{z})$ at the lower and upper bounds, and e_1 is the error threshold. The first criterion can measure the accuracy of the lower and upper bounds of the output mean. In addition, the second criterion considers the maximum value of the AEI function:

$$\max(\text{AEI}(\mathbf{p})) \leq m_{\hat{g}}(\mathbf{p}^{**}) \cdot e_2 \quad (56)$$

where e_2 is a user-specified value. The left term in the second stopping criterion indicates by how much the maximum improvement is expected to be greater than $m_{\hat{g}}(\mathbf{p}^{**})$ and reflects the level of epistemic uncertainty in the Co-Kriging model. If both of the stopping criteria are consecutively satisfied for 2 iterations, stop the Co-Kriging update and return the bounds of $u_g(\mathbf{y}, \mathbf{z})$ and $\sigma_g^2(\mathbf{y}, \mathbf{z})$. Otherwise, go to step 5.

Step 5: Identification of the update point. The values of the interval and fuzzy variables for the new point (denoted as $(\mathbf{y}^*, \mathbf{z}^*)$) are adaptively determined by maximizing the learning function AEI shown in Eq. (53). The values of the interval and fuzzy variables are then fixed, and determine the values of the random variables from Ω by maximizing the expected improvement (EI) function based on LF and HF predictions:

$$\text{EI}_c(\mathbf{x}) = (y_c^{\min} - y_c(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)) \Phi \left(\frac{y_c^{\min} - y_c(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)}{s_c(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)} \right) + s_c(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*) \varphi \left(\frac{y_c^{\min} - y_c(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)}{s_c(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)} \right) \quad (57)$$

$$\text{EI}_e(\mathbf{x}) = (y_e^{\min} - y_e(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)) \Phi \left(\frac{y_e^{\min} - y_e(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)}{s_e(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)} \right) + s_e(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*) \varphi \left(\frac{y_e^{\min} - y_e(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)}{s_e(\mathbf{x}, \mathbf{y}^*, \mathbf{z}^*)} \right) \quad (58)$$

where y_c^{\min} and y_e^{\min} are the minimum values of the responses \mathbf{y}_c and \mathbf{y}_e , respectively, s_c and s_e are the standard deviation of LF and HF predictions, respectively. If the maximum value of $\text{EI}_c(\mathbf{x})$ is larger than that of $\text{EI}_e(\mathbf{x})$, the values of the random variables is determined as the point \mathbf{x}^* corresponding to the maximum of $\text{EI}_c(\mathbf{x})$, and add the new point $(\mathbf{x}^*, \mathbf{y}^*, \mathbf{z}^*)$ to the LF samples. Otherwise, the point \mathbf{x}^* corresponding to the maximum of $\text{EI}_e(\mathbf{x})$ is selected and add the new point $(\mathbf{x}^*, \mathbf{y}^*, \mathbf{z}^*)$ to HF samples.

The flowchart of the proposed approach is shown in Fig. 2.

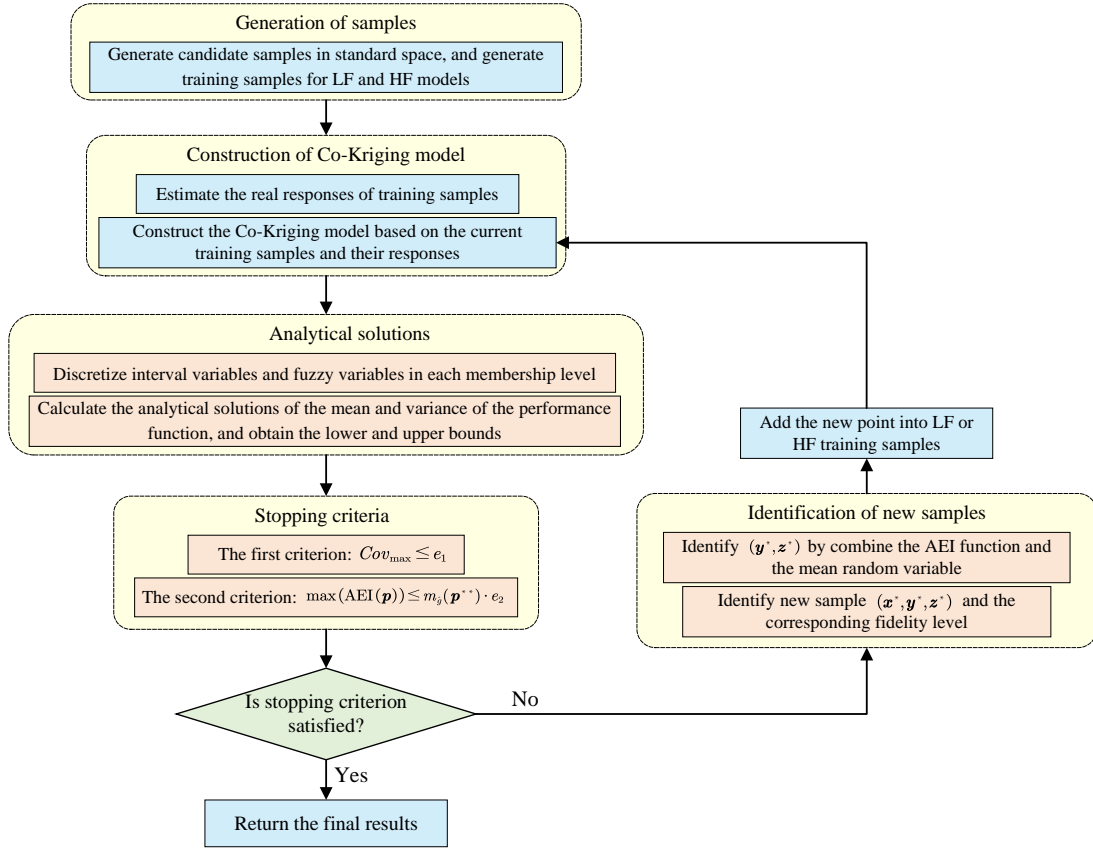


Figure 2: Flowchart of the proposed method

308

309 4. Illustrative Examples

310 In this section, four examples are investigated to validate the efficiency and accuracy of the proposed
 311 method, including a mathematical example, a roof truss structure, a planetary transmission gear and a
 312 frame structure. In each example, the scaling factor ρ is set to 1, and the candidate sample size N_Ω is set
 313 to 10^5 . For interval and fuzzy variables, 11 α -cut levels are assigned uniformly to fuzzy variables, and
 314 300 discrete points are generated between the bounds of interval and fuzzy variables at each cut level.
 315 The results of the proposed active learning method are obtained over 30 independent runs, and the
 316 average results are compared with the reference results obtained by MCS and with the results obtained
 317 without active learning (i.e., construct a Co-Kriging model using all the training samples required by
 318 the proposed method, and directly estimate the bounds of $u_g(\mathbf{y}, \mathbf{z})$ and $\sigma_g^2(\mathbf{y}, \mathbf{z})$).

319 *4.1. Example 1: A mathematical example*

320 The first example is a mathematical problem which is modified from [46]. In this example:

$$\begin{aligned}
 g^h(\mathbf{X}, Y, Z) &= \sin\left(\frac{5X_1}{2}\right) - \frac{(X_1Z + 4)(X_2 - 1)}{20} + Y \\
 g^l(\mathbf{X}, Y, Z) &= \sin\left(\frac{5X_1}{2}\right) - \frac{(0.9X_1Z + 4)(0.9X_2 - 1)}{20} + 0.9Y
 \end{aligned}
 \tag{59}$$

321 where $g^h(\cdot)$ and $g^l(\cdot)$ denote the HF and LF models, respectively. In this example, two independent
 322 random variables, one interval variable and one fuzzy variable are included. The details of these
 323 uncertain variables are listed in Table 1.

324 In this example, 20 HF samples and 20 LF samples are generated to construct the initial Co-Kriging
 325 model. The error threshold e_1 and e_2 are set to 0.005. Fig. 3 shows the lower and upper bounds of the
 326 output mean u_g and the output variance σ_g^2 at each membership level. It is observed that the proposed
 327 method has a very good performance in estimating the intervals of the output mean u_g and the output
 328 variance σ_g^2 , while the results without active learning are not accurate enough. In particular, the bounds
 329 of σ_g^2 obtained without active learning deviate significantly from the reference. Table 2 summarizes the
 330 comparative results obtained by different methods, where $\underline{\varepsilon}(u_g)$ and $\bar{\varepsilon}(u_g)$ are the maximum relative
 331 errors of the lower and upper bounds of u_g , $\underline{\varepsilon}(\sigma_g^2)$ and $\bar{\varepsilon}(\sigma_g^2)$ are the maximum relative errors of the
 332 lower and upper bounds of σ_g^2 . It can be seen that the results obtained without active learning have
 333 the largest error for the upper bound of σ_g^2 , which is 7.90% corresponding to the membership level 0.
 334 The maximum relative error of u_g obtained by the proposed method is 0.36% corresponding to the
 335 membership level 1, while the maximum relative error of σ_g^2 is 0.44% corresponding to the membership
 336 level 1. Compared to MCS, the function calls of the proposed method are greatly reduced, requiring
 337 only 32 evaluations of the HF model and 58 evaluations of the LF model. In addition, through kernel
 338 density estimation, the PDFs of the output obtained by the three methods at two different points of
 339 interval and fuzzy variables are plotted in Fig. 4. It can be seen that the estimated PDFs of the
 340 proposed method are almost identical to the reference PDFs, while the PDFs obtained without active
 341 learning are less accurate. Thus, the proposed method has prominent performance in terms of efficiency

Table 1: Uncertain variables in Example 1.

Uncertain variables	Distribution types	Parameter 1	Parameter 2
X_1	Normal	1.5	1
X_2	Normal	2.5	1
Y	Interval	2	2.5
Z	Fuzzy	Triangular	(1.5, 2, 2.5)

For the random variable, parameter 1 and 2 are the mean and standard deviation, respectively; for the interval variable, parameter 1 and 2 are the lower and upper bounds, respectively; for the fuzzy variable, parameter 1 and parameter 2 are the type of membership function and the function parameters

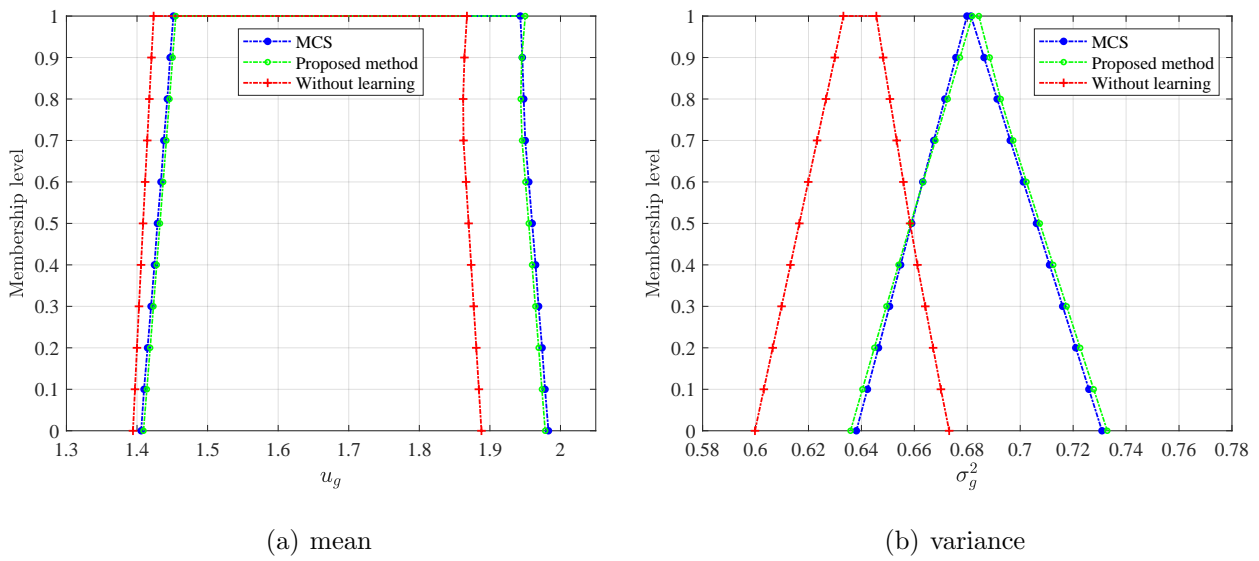
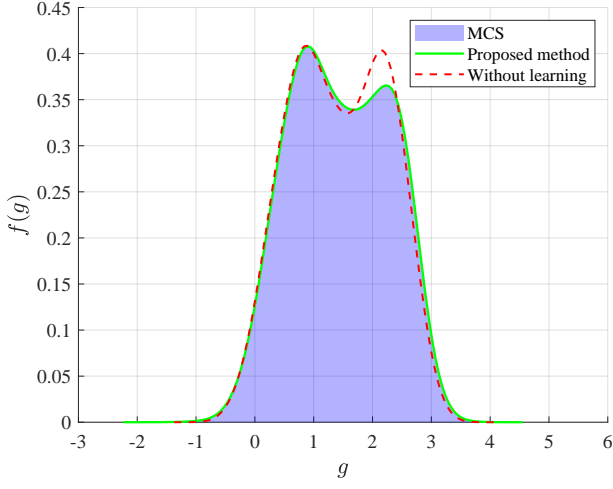
Figure 3: The bounds of the mean u_g and variance σ_g^2 in Example 1

Table 2: Comparative results in Example 1.

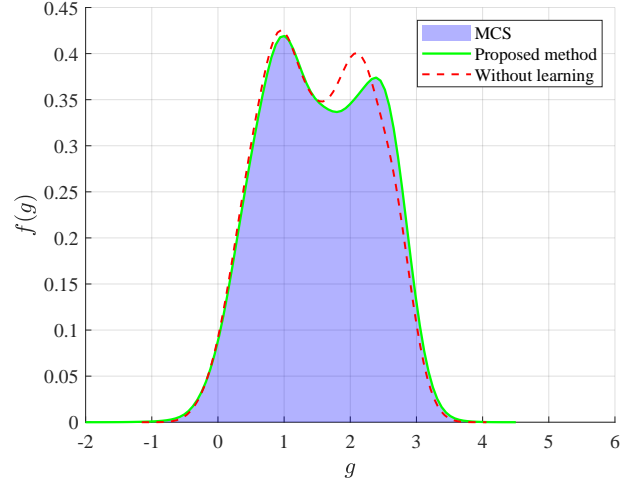
Methods	$\underline{\varepsilon}(u_g)$	$\bar{\varepsilon}(u_g)$	$\underline{\varepsilon}(\sigma_g^2)$	$\bar{\varepsilon}(\sigma_g^2)$	Function costs
MCS	-	-	-	-	$10^5 \times 300 \times 11$
Proposed method	0.28% ($\alpha = 0.1$)	0.36% ($\alpha = 1$)	0.35% ($\alpha = 0$)	0.44% ($\alpha = 1$)	32HF+58LF
Without learning	1.93% ($\alpha = 1$)	4.79% ($\alpha = 0$)	6.87% ($\alpha = 1$)	7.90% ($\alpha = 0$)	32HF+58LF

343 4.2. Example 2: A roof truss

344 As shown in Fig. 5, this example investigates a roof truss structure, which is modified from [47]. For
 345 this structure, the bottom boom and the tension bars are steel, while the top boom and the compression
 346 bars are reinforced by concrete. Assume that this roof structure is subjected to the uniformly distributed



(a) PDFs ($Y = 2$ and $Z = 2$)



(b) PDFs ($Y = 2.5$ and $Z = 2$)

Figure 4: The PDFs of the output in Example 1

347 load q , which can be equivalently transformed to the nodal load $P = ql/4$. We focus on the vertical
 348 deflection Δ_C at the node C , where the HF and LF models are expressed as follows:

$$\Delta_C^h = \frac{ql^2}{2} \left(\frac{3.81}{A_c E_c} + \frac{1.13}{A_s E_s} \right) \quad (60)$$

$$\Delta_C^l = \frac{q(l+1)^2}{2} \left(\frac{3.81}{A_c (E_c + 1e7)} + \frac{1.13}{A_s (E_s + 1e7)} \right) \quad (61)$$

349 where A_s and A_c denote the cross-sectional area of the steel and concrete bars, respectively, E_s and
 350 E_c denote their Young's modulus, respectively. Table 3 gives the information of uncertain variables.
 351 For the truncated Gaussian distribution, the range values is between positive and negative 3 sigma
 352 intervals.
 353 intervals.

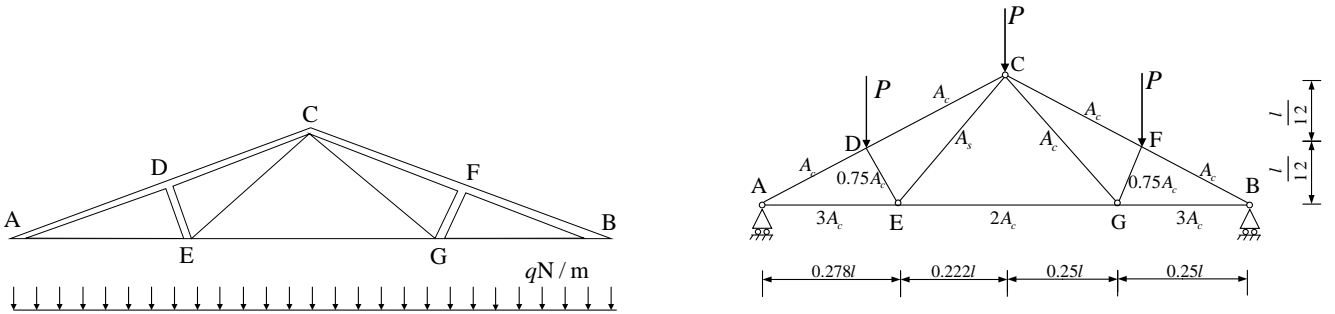


Figure 5: Schematic structural view of the roof truss

354 Initially, the number of training samples for the HF and LF models is set to 28 and 28, respectively.
 355 The error thresholds e_1 and e_2 are set to 0.005 and 0.0001 in this example. Three methods are applied

Table 3: Uncertain variables of the roof truss structure.

Uncertain variables	Distribution types	Parameter 1	Parameter 2
q (N/m)	Truncated Gaussian	20000	1600
l (m)	Truncated Gaussian	12	0.24
E_s (N/m ²)	Truncated Gaussian	1.2×10^{11}	8.4×10^9
E_c (N/m ²)	Truncated Gaussian	3×10^{10}	2.4×10^9
A_s (m ²)	Interval	9.2×10^{-4}	9.6×10^{-4}
A_c (m ²)	Fuzzy	Triangular	(0.032, 0.034, 0.036)

Parameters 1 and 2 are the same as those in Table 1

356 to obtain the intervals of the output mean u_g and the output variance σ_g^2 of the vertical deflection Δ_C .
357 The bounds of u_g and σ_g^2 are drawn in Fig. 6, Table 4 lists the maximum relative error and the function
358 calls of different methods, and the PDFs estimated by the three methods are also plotted in Fig. 7. It
359 can be seen in Fig. 6 that the lower and upper bounds of u_g and σ_g^2 obtained by the proposed method
360 are almost identical to the reference solutions, while the bounds of σ_g^2 estimated directly without active
361 learning do not agree so well with the reference bounds obtained by MCS. From Table 4, the maximum
362 relative error of the lower and upper bounds of u_g caused by the proposed method are 0.10% and 0.12%,
363 when the membership level is 0.4 and 0.7, respectively. Moreover, the maximum relative error of the
364 bounds of σ_g^2 caused by the proposed method is 0.19%, which is smaller than that caused by the direct
365 estimation without active learning. The function calls of the proposed method are 49 evaluations of
366 HF models and 78 evaluations of LF models, while the function calls of MCS is $10^5 \times 300 \times 11$. In Fig.
367 7, it is observed that the PDF shapes obtained by the proposed method agree well with the reference.
368 Accordingly, the proposed method can produce more accurate results than direct estimation without
369 active learning, and can obtain the lower and upper bounds of u_g and σ_g^2 with only a few HF samples.

Table 4: Comparative results for the roof truss structure.

Methods	$\underline{\varepsilon}(u_g)$	$\bar{\varepsilon}(u_g)$	$\underline{\varepsilon}(\sigma_g^2)$	$\bar{\varepsilon}(\sigma_g^2)$	Function costs
MCS	-	-	-	-	$10^5 \times 300 \times 11$
Proposed method	0.10% ($\alpha = 0.4$)	0.12% ($\alpha = 0.7$)	0.19% ($\alpha = 0$)	0.19% ($\alpha = 0$)	49HF+78LF
Without learning	0.15% ($\alpha = 1$)	0.15% ($\alpha = 0.7$)	1.61% ($\alpha = 1$)	1.50% ($\alpha = 0$)	49HF+78LF

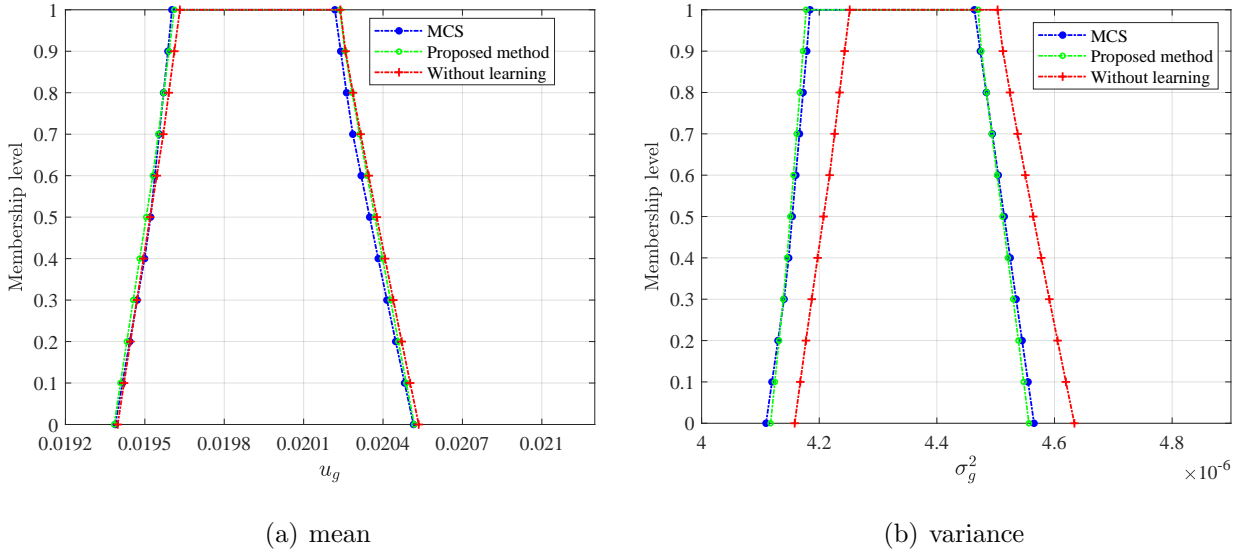


Figure 6: The bounds of the mean and variance of the vertical deflection Δ_C

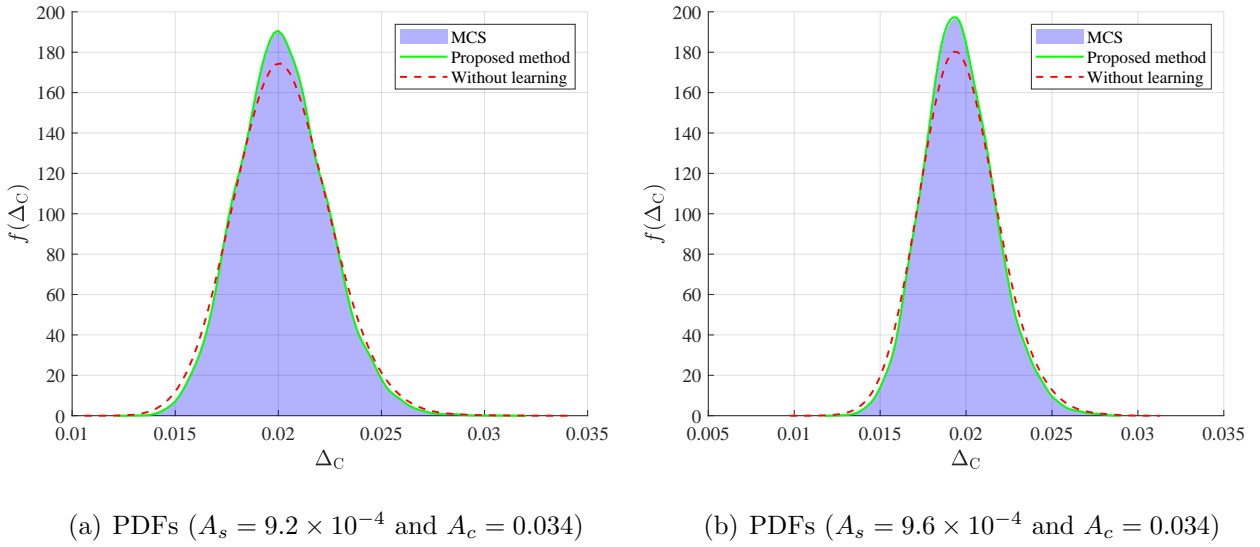


Figure 7: The PDFs of the vertical deflection Δ_C

370 *4.3. Example 3: A planetary transmission gear*

371 A planetary transmission gear system, as shown in Fig. 8, is studied to demonstrate the proposed
 372 method when dealing with a practical engineering problem. This gear system consists of a ring gear,
 373 three planet gears, and a sun gear that serves as the input gear. The pressure angle α_k , module m
 374 and tooth width b for all gears are 20 degrees, 1.5mm and 30mm, respectively. The numbers of teeth
 375 for the sun gear, the planet gear and the ring gear are 36, 21 and 78, respectively. All gears are made
 376 of the same material. The Young's modulus E , the Poisson's ratio ν and the coefficient of friction f
 377 are random variables, while the transmitted torque T is a fuzzy variable. Table 5 lists the statistical

378 information of the uncertain variables. For the truncated Gaussian distribution, the range values is
 379 between positive and negative 3 sigma intervals. As shown in Fig. 9, the maximum contact stress
 380 σ_H on the planet gear is the response of interest, which is calculated by the finite element software
 381 ABAQUS. For the HF model, the initial and maximum increment sizes are 0.01. For the LF model,
 382 the initial and maximum increment sizes are set to 0.05 and 0.1, respectively. The simulation time for
 383 each run of the HF model is about 2 hours, while the simulation time for each run of the LF model is
 384 about 30 minutes.

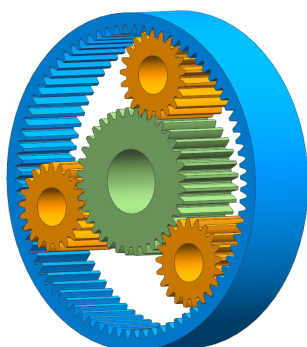


Figure 8: The planetary transmission gear

Table 5: Uncertain variables of the planetary transmission gear.

Uncertain variables	Distribution types	Parameter 1	Parameter 2
E (MPa)	Lognormal	210000	10500
ν	Truncated Gaussian	0.3	0.015
f	Truncated Gaussian	0.05	0.0025
T (N · mm)	Fuzzy	Triangular	$(2.95 \times 10^5, 3.0 \times 10^5, 3.05 \times 10^5)$

Parameters 1 and 2 are the same as those in Table 1

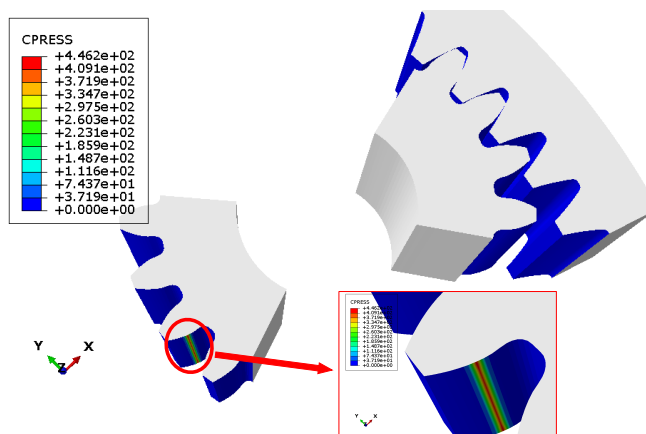


Figure 9: The stress result of planetary transmission gear

385 To perform MCS as the reference results, 100 HF samples are generated to construct a sparse
386 polynomial chaos expansions (PCE) model with the maximum degree 4 to approximate the true finite
387 element model. 10 HF samples are used as the test set, and the root mean square error (RMSE) is 0.003.
388 In addition, the construction and update of Co-Kriging model are based on the sparse PCE model. In
389 this example, 18 LF and 18 HF samples are chosen to construct the initial Co-Kriging model. The
390 error threshold e_1 and e_2 are 0.002 and 0.0001. The lower and upper bounds of u_g and σ_g^2 of maximum
391 contact stress are shown in Fig. 10. The comparative results of this example are presented in Table
392 6. The maximum relative errors of u_g and σ_g^2 bounds introduced by the proposed method are 0.01%
393 and 3.44%, respectively, both occurring at the membership level $\alpha = 0$. Without active learning, the
394 maximum relative errors of u_g and σ_g^2 bounds are 0.03% and 40.19%, respectively. In terms of accuracy,
395 the average results of σ_g^2 have larger relative errors than the average results of u_g . 84 evaluations of
396 the HF model and 46 evaluations of the LF model are required by the proposed method, which is
397 fewer than that by MCS. In this example, there are more HF points than LF points, which may be
398 due to the lack of accuracy of the LF finite element model. In Fig. 11, the PDF shapes obtained by
399 different methods are provided. It can be found that compared to the direct estimation without active
400 learning, the proposed method can produce more accurate results of the output variance and the shape
401 of the PDF. Thus, it is demonstrated the efficiency and accuracy of the proposed method for the hybrid
402 uncertainty analysis of structures.

Table 6: Comparative results for the planetary transmission gear.

Methods	$\underline{\varepsilon}(u_g)$	$\bar{\varepsilon}(u_g)$	$\underline{\varepsilon}(\sigma_g^2)$	$\bar{\varepsilon}(\sigma_g^2)$	Function costs
MCS	-	-	-	-	$10^5 \times 300 \times 11$
Proposed method	0.01% ($\alpha = 0$)	0.01% ($\alpha = 0$)	3.44% ($\alpha = 0$)	1.16% ($\alpha = 0$)	84HF+46LF
Without learning	0.03% ($\alpha = 1$)	0.03% ($\alpha = 0.6$)	33.04% ($\alpha = 1$)	40.19% ($\alpha = 0$)	84HF+46LF

403 4.4. Example 4: A two-bay ten-story frame structure

404 A two-bay ten-story spatial steel frame structure is considered in this example, which requires the
405 finite element analysis, as shown in Fig. 12. The OpenSees software is employed to model and analyze

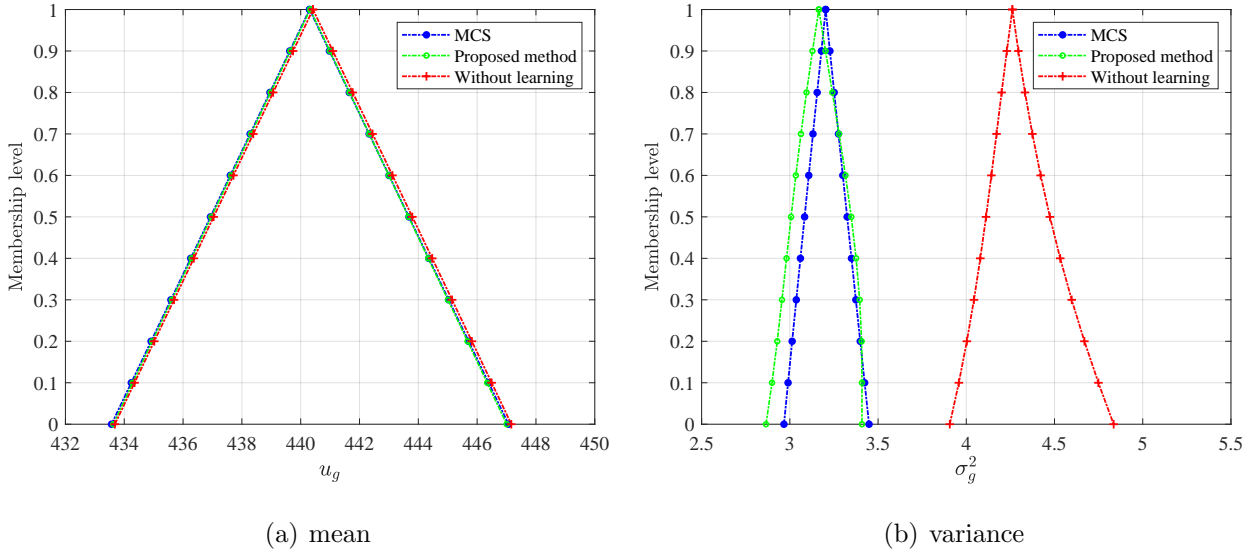


Figure 10: The bounds of the mean and variance of the maximum contact stress σ_H

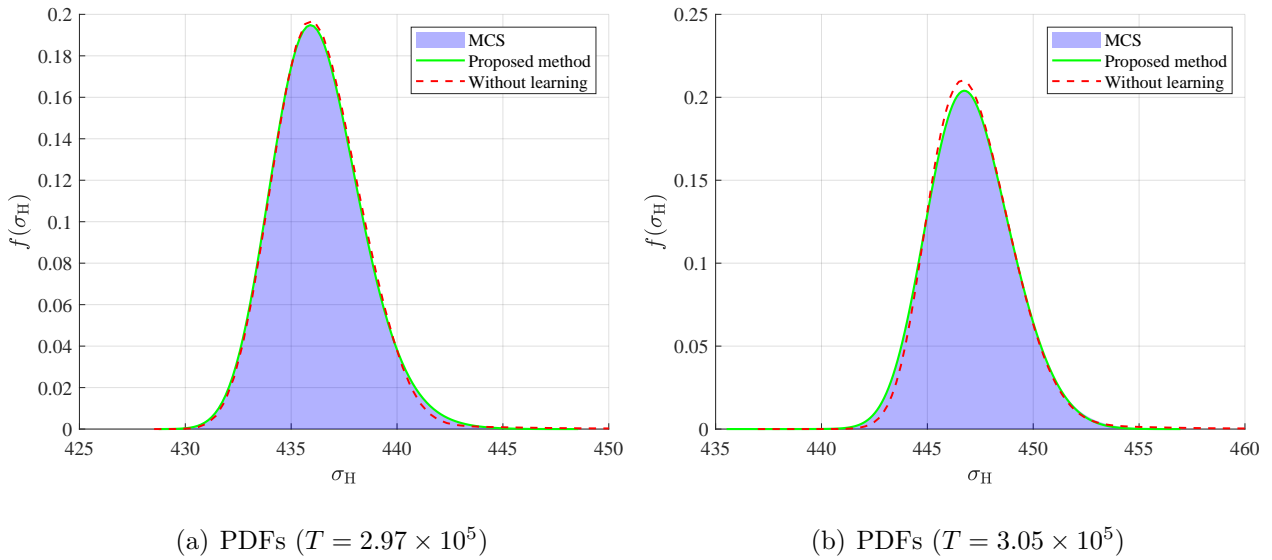


Figure 11: The PDFs of the maximum contact stress σ_H

406 this frame structure, and the roof drift is adopted as the response of interest, which is symbolized as D_r .

407 In this example, the slab of each floor is supposed to be rigid. The random variables include the Young's

408 modulus of the beams and columns (denoted as E_b and E_c , respectively), the cross-sectional area of the

409 bottom column (denoted as A_{c1}), the cross-sectional area of the remaining columns (denoted as A_{c2}),

410 and seven concentrated loads F_i ($i = 1, 2, \dots, 7$). The interval variables consist of two concentrated loads

411 F_8 and F_9 . The load F_{10} and the cross-sectional area of the beam are fuzzy variables. Table 7 lists the

412 statistical information of the uncertain variables. For the truncated Gaussian distribution, the range

413 values is between positive and negative 3 sigma intervals. For the LF model, the load F_{10} is discarded.

414 To save computational time, the reference solution of MCS is performed using the Kriging model, with
415 270 HF samples used as the training set and 30 HF samples used as the test set. The RMSE of the
416 Kriging model is 0.049.

417 68 LF and 68 HF training samples are generated to construct the initial Co-Kriging model. The
418 error thresholds e_1 and e_2 are set to 0.005 and 0.0005, respectively. The lower and upper bounds of
419 u_g and σ_g^2 of D_r are shown in Fig. 13. It can be observed that as the membership level increases,
420 the bounds of u_g and σ_g^2 become narrower. Moreover, although the bounds of u_g obtained by the
421 proposed method and the direct estimation without active learning both agree well with the reference
422 bounds, the bounds of σ_g^2 obtained by the proposed method are much more accurate than that obtained
423 without active learning. The maximum relative error of the lower and upper bounds of u_g and σ_g^2 are
424 summarized in Table 8. The maximum relative error of the bounds of u_g caused by the proposed method
425 is 0.48% with the membership level $\alpha = 0$, while the maximum relative error without active learning
426 is 3.83%. The maximum relative error of σ_g^2 of the proposed method is 0.76% when the membership
427 level is 0, while the maximum relative error without active learning is 17.07%. The total number of
428 function calls is 115 evaluations of the HF model and 147 evaluations of the LF model, which is fewer
429 than those required by MCS. When the fuzzy variable takes the value of the membership level of 1,
430 the PDFs of D_r at two different values of the interval variable are drawn in Fig. 14. The results
431 indicate that the proposed method can more accurately estimate the output mean and the output
432 variance, as well as the output PDF. In summary, the proposed method demonstrates a high efficiency
433 in hybrid uncertainty propagation analysis and is also applicable to the engineering problems with
434 multiple epistemic uncertainties.

435 5. Conclusions

436 A novel decoupled method based on multi-fidelity active learning is proposed to deal with hybrid
437 uncertainty propagation analysis under random, interval and fuzzy variables. The analytical solutions
438 of the output mean and the output variance are derived based on the Co-Kriging model, where the

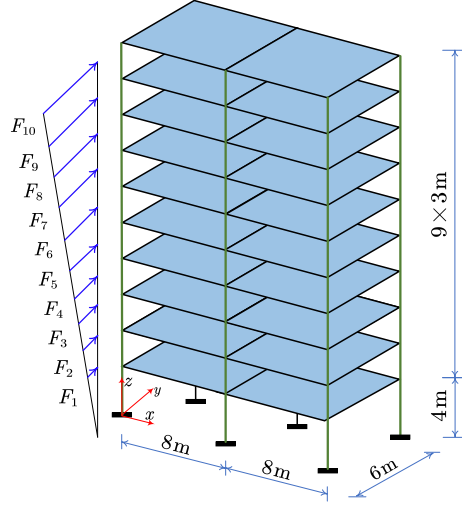


Figure 12: The two-bay ten-story frame structure

Table 7: The statistical information of uncertain variables for the frame structure.

Uncertain variables	Distribution types	Parameter 1	Parameter 2
E_b (MPa)	Truncated Gaussian	3.25×10^4	1.625×10^3
E_c (MPa)	Truncated Gaussian	3.25×10^4	1.625×10^3
A_{c1} (m ²)	Truncated Gaussian	3.6×10^{-1}	1.8×10^{-2}
A_{c2} (m ²)	Truncated Gaussian	1.6×10^{-1}	8×10^{-3}
F_1 (N)	Truncated Gaussian	2.5×10^4	1.25×10^3
F_2 (N)	Truncated Gaussian	2.7×10^4	1.35×10^3
F_3 (N)	Truncated Gaussian	2.9×10^4	1.45×10^3
F_4 (N)	Truncated Gaussian	3.1×10^4	1.55×10^3
F_5 (N)	Truncated Gaussian	3.3×10^4	1.65×10^3
F_6 (N)	Truncated Gaussian	3.5×10^4	1.75×10^3
F_7 (N)	Truncated Gaussian	3.7×10^4	1.85×10^3
F_8 (N)	Interval	3.5×10^4	4.5×10^4
F_9 (N)	Interval	4.0×10^4	5.0×10^4
F_{10} (N)	Fuzzy	Triangular	$(4.5 \times 10^4, 5.0 \times 10^4, 5.5 \times 10^4)$
A_b (m ²)	Fuzzy	Triangular	$(2.0 \times 10^{-1}, 2.4 \times 10^{-1}, 2.8 \times 10^{-1})$

Parameters 1 and 2 are the same as those in Table 1

Table 8: Comparative results for the spatial frame structure.

Methods	$\underline{\varepsilon}(u_g)$	$\bar{\varepsilon}(u_g)$	$\underline{\varepsilon}(\sigma_g^2)$	$\bar{\varepsilon}(\sigma_g^2)$	Function costs
MCS	-	-	-	-	$10^5 \times 300 \times 11$
Proposed method	0.48% ($\alpha = 0$)	0.40% ($\alpha = 0.1$)	0.76% ($\alpha = 0$)	0.37% ($\alpha = 0$)	115HF+147LF
Without learning	3.83% ($\alpha = 0$)	1.44% ($\alpha = 1$)	7.89% ($\alpha = 0$)	17.07% ($\alpha = 0$)	115HF+147LF

439 variance of the output mean is also derived to measure the uncertainty of the Co-Kriging model. Then,
440 the analytical solutions for the mean and variance of the output mean are employed to enable an active

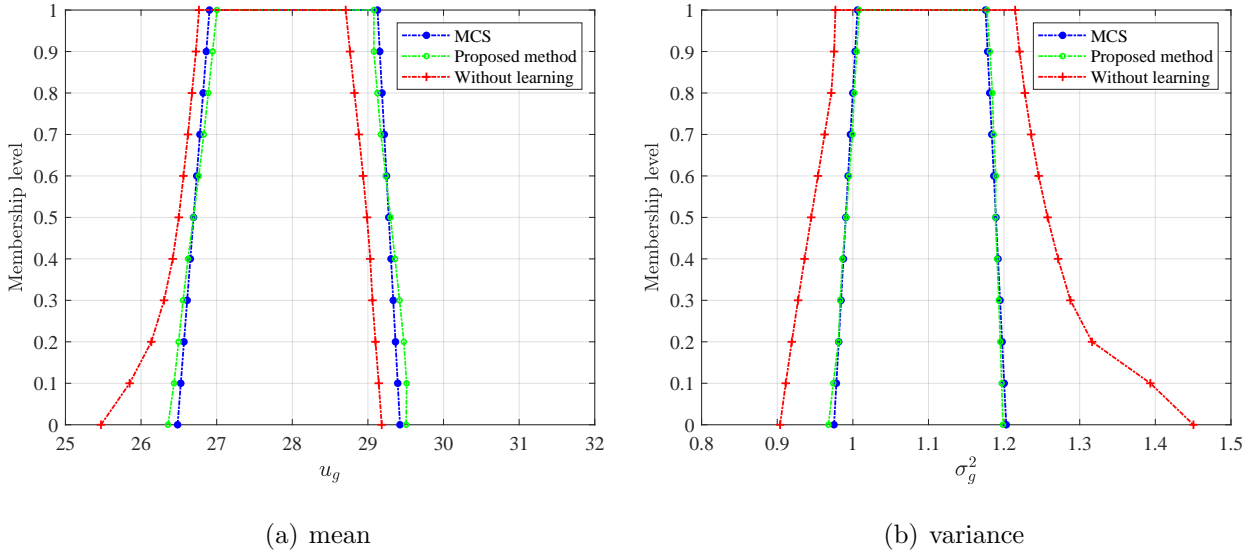


Figure 13: The bounds of the mean and variance of the roof drift D_r .

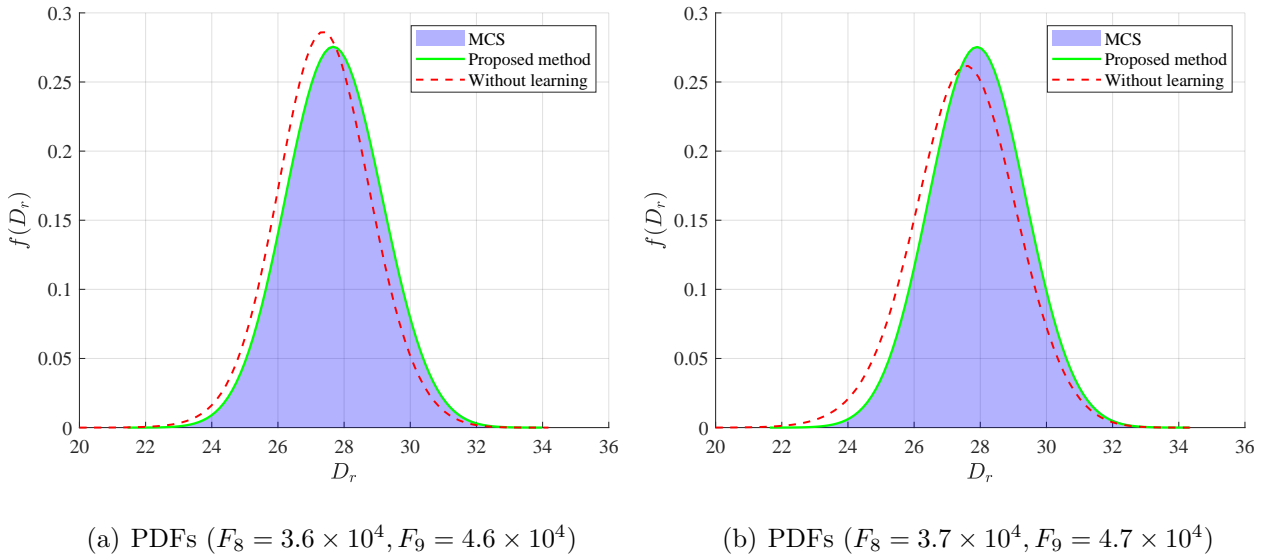


Figure 14: The PDFs of the roof drift D_r .

441 learning framework. Finally, the Co-Kriging model update is terminated by considering the coefficient
 442 of variation of the output mean and the value of the learning function.

443 Four examples are used to test the performance of the proposed method. From the comparative
 444 results of the four examples, the relative error of the output mean obtained by the proposed method is
 445 very small, while the relative error of the output variance is larger but still acceptable, and the proposed
 446 method produces more accurate results than the direct estimation without active learning. It is worth
 447 noting that this method can avoid the post-processing errors, and can be degraded to handle hybrid
 448 uncertainty propagation problems with only two types of uncertain variables. In addition, since the

analytical solutions of the output mean and output variance are derived based on Co-Kriging model, this method can deal with efficient hybrid uncertainty propagation for multi-fidelity problems, and the constructed framework can be further incorporated into the sensitivity analysis, RBDO and RDO. For example, in materials science, randomness is present in all materials at some level of resolution [48]. To achieve robust materials design, uncertainty has to be considered, and uncertainty propagation is one of the most important elements. While epistemic uncertainty in model parameters is usually ignored in conventional deterministic approaches [49], the proposed method can deal with hybrid uncertainty propagation for multi-fidelity models.

In the construction of Co-Kriging model, hyper-parameters need to be estimated, where optimization is required. As the dimensionality increases, so does the number of parameters to be estimated, and high-dimensional optimization remains a challenge. It should be noted that our approach is based on Co-Kriging and is not exempt from this limitation. To deal with high-dimensional problems, dimension reduction methods [47, 50] can be incorporated into Co-Kriging to improve efficiency. This is the focus of our future work.

Acknowledgment

This work is supported by the National Natural Science Foundation of China (Grant 52205252), the National Natural Science Foundation of Sichuan Province (Grant 2023NSFSC0876), the Alexander von Humboldt Foundation of Germany, and the China Scholarship Council (CSC).

Conflict of interest statement

The authors declare that they have no conflict of interest.

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