# Multi-spot ultrafast laser ablation at ambient pressure – a new window on coalescing shock wave interactions

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## 15 Abstract

During ultrafast laser ablation at ambient pressure, redeposition of nano-particulates occurs through 16 backwards flux towards the end of the ablation process and is often viewed as undesirable. Here, 17 on the contrary, we report on unique, highly symmetric redeposition patterns observed during 18 19 ultrafast laser ablation of metals with closely spaced multi-spots in ambient gases. Spot symmetries were altered with a Spatial Light Modulator or beam splitting optics. At low fluence (relative to 20 21 material ablation threshold), debris is highly confined within the spot patterns, while at higher fluence, jets of debris emanate along axes of symmetry reaching distances far exceeding the spot 22 23 separations. These phenomena appear universal but depend on the spot proximity, substrate, ambient gas density and pulse energy. The jets, formed at the collision planes between plasma 24 plumes, consist of agglomerated nanoparticle debris, lifted and accelerated by colliding supersonic 25 Mach shocks whose early interactions are imprinted on the debris fields. Numerical simulation 26 using computational fluid dynamics (CFD) of multi-spot ablation in ambient gas supports this view 27 of the phenomena. These observations are relevant to an improved understanding of coalescing 28 shock waves, induced air flows and re-deposition at ambient pressure. 29

# 30 1. Introduction

Ultrafast laser ablation at ambient pressure is complex, involving processes over a remarkably wide 31 timescale from femtoseconds to microseconds. In metals, light absorption heats electrons rapidly 32 so creating a high nonequilibrium state with transient electron temperature  $T_e > 10^4 \text{ K}$ [1]. Electron-33 phonon coupling then heats the lattice well above the critical temperature on a picosecond timescale 34 resulting in a fast solid-vapour/plasma transition with superheated material in a metastable state, 35 36 leading to phase explosion[2]. On a nanosecond timescale, the expanding high-temperature plasma  $(T_e \sim 1 \text{ eV})$  with a longitudinal velocity exceeding a few km/sec creates a supersonic shock (blast) 37 wave through energetic collisions with background gas molecules accompanied by intense plasma 38 spectral emission[3]. 39

While the plasma expansion in vacuo can be described as free, increasing ambient pressure alters plume geometry from spherical to cylindrical as the ambient fluid drag affects both longitudinal and radial plasma expansion[1]. Increasing pressure spatially confines the plume expansion, "aiding molecular and cluster generation with aerosols and nanoclusters generated through a nucleationcondensation process"[4] occurring towards the end of the ablation event with a vortex structure 45 developing at the plume edge[5-7]. Nanoparticles (NPs) may also be generated directly from phase 46 explosion or spallation during ablation[8]. On stainless steel, 90% of NPs generated by ps and fs 47 laser pulses have diameters  $\varphi \le 100 \text{ nm}[9]$ .

During the collision of laser-produced plasmas in vacuo, interpenetration or plasma stagnation can 48 occur depending on atomic number Z, relative plasma velocity and plasma density[10, 11]. 49 Significant momentum transfer takes place between the atoms/ions during stagnation. For elements 50 with high Z (W, Mo) plasma ions tend to interpenetrate, while low Z elements (Al, C) plasma ions 51 can stagnate. Plasma collisions in ambient air have recently been studied using Aluminium V-52 shaped targets where the seed plasmas collided at the mid-plane[12]. Spectrally resolved fast 53 imaging of Al atoms along with Al<sup>+</sup> and Al<sup>2+</sup> ions demonstrate that "ions travel much further than 54 neutral atoms, which are detected closer to the surface". Two high-energy, ns laser-produced Al 55 plasmas and their shock wave interactions in ambient air demonstrated a stagnation layer behind 56 the shock fronts at microsecond delays with gas density behind the shock front n ~  $4.3.10^{20}$  cm<sup>-3</sup> 57 almost 20 times that of air at 1 bar pressure[13]. Even at low mBar ambient pressure, a numerical 58 59 study of lateral colliding plasmas demonstrates stagnation and evidence of shock waves[14].

60 Debris redeposition after single spot laser ablation is a dynamic gas effect[6, 15, 16]. Backward flux redeposition during double spot, multi-pulse ultrafast laser ablation on stainless steel was 61 recently reported by us with the appearance of aligned debris or "filaments" along the spot axis and 62 symmetric jets emanating normal to the spot axis, fluence dependent[17]. Only a tentative 63 explanation of the phenomena could be advanced there, connected with colliding plasmas and 64 coalescing shock waves. In this paper, we present the first observations of debris fields during multi-65 spot ultrafast ablation on different metals in ambient air and Helium atmospheres with spot number 66 67  $N \ge 2$ . The impressive symmetry observed on various materials suggests a universal behaviour and common physical explanation which has been investigated here thoroughly and supported by 68 simulations of coalescing shocks. 69

# 70 2. Materials and Methods

71 Experiments were performed in the Laserinstitut Hochschule Mittweida laboratory (Fig 1.): 600 fs 72 exposure: polished samples were supported on a micro-positioning x,y,z system. The Laser beam was expanded and directed to a 50:50 beam splitter and then variable delay line (mirrors M2,M3) 73 74 with tilt mirror M8 to spatially separate and temporally synchronize double spots on target. A half wave plate (HWP3) was used to bring pulse polarisations parallel. Time zero was detected through 75 plasmonic structures when the beams were focused and overlapped spatially and temporally. The 76 77 spatial distance between the pulses is monitored with a CCD camera in the focal plane. The laser system (0.6 ps/1030 nm) is a FX200-Series model, Edgewave GmbH (Wurselen, Germany) with a 78 maximum pulse energy  $E_P > 40 \mu J$ . The average power could be measured with a thermal detector 79 (Gentec EO Inc., Ouebec, Canada). The experiments were performed under normal conditions in 80 air. SEM images were captured with a microscope from JOEL Ltd. (Tokyo, Japan). 81

Experiments were performed in the Department of Engineering, University of Liverpool (Fig 2.): 82 83 10 ps exposure: all samples were optically polished prior to laser exposure and supported on x,y,z stages (Aerotech). Laser beams were attenuated, expanded (×3) and directed to a Scanning Galvo 84 85 with an f-theta lens (f = 100 mm, spot size  $2\omega_0 = 22.2 \,\mu$ m) after reflection from a phase-only Spatial 86 Light Modulator (SLM, Hamamatsu, X-10468-03). The SLM was addressed with appropriate 87 Computer-Generated Holograms (CGHs) which are generated and programmed in Labview software. A 4f optical system relayed the reflected complex optical field to the input aperture of the 88 89 scanning Galvo. The laser system (10 ps/1064 nm) is a High-Q model IC355-800 with maximum pulse energy  $E_P > 120 \mu J$ . Spot patterns and relative spot energies could be checked prior to material 90 exposure using a pick-off mirror and focused with a long focal length lens to a Spyricon CCD 91 camera (SP 620U). Pulse energies could be measured with a power meter/pyro-electric detector. 92

The pulse number is controlled by using a fast-mechanical shutter (Thorlabs SH05) which is 93 synchronised to the SCAPS GmbH scanning software. For ablation in He, substrates were mounted 94 in a special 3-way vacuum tight cell which is mounted on the x,y,x stage. A vacuum pump first 95 reduced the air pressure to < 0.01 Bar after which the cell was backfilled with Helium to required 96 97 pressure. Laser beams were focused on the substrate through an AR-coated window on top. A 2 lens imaging system (M ~  $\times$ 8) aligned outside the vacuum cell side window imaged the expanding 98 plasma plumes onto the ICCD camera (Andor, iStar 734) which was synchronised by the TTL 99 output from the Pockels Cell driver of the laser system. Scanning electron microscopy (SEM) and 100 accompanying energy dispersive X-ray spectroscopy (EDX) was performed using a Zeiss Gemini 101 450 FEG-SEM equipped with an Oxford Instruments X-Max 50 mm<sup>2</sup> EDX detector. This was 102 operated using an accelerating voltage between 1 - 10 kV and probe current between 500 - 1000103 pA. Ansys Fluent software was used for multi-spot ablation simulations in ambient gas with the 104 continuity equations based on the Rankine-Hugoniot equations [18]. The surface dimension was 105 set to 2000 µm x 2000 µm with grid dimension 4 µm x 4 µm which allowed the simulations to 106 converge. 107

## 108 **3. Results**

## 109 3.1 Femtosecond ablation

110 The terms "low pulse energy", "intermediate pulse energy" and "high pulse energy" are used 111 throughout the paper, represented by acronyms,  $LE_p$ ,  $IE_p$ , and  $HE_p$  respectively. They represent  $LE_p$ 112 = 2  $\mu$ J,  $IE_p = 5 \mu$ J and  $HE_p \ge 8 \mu$ J. while pulse exposure number lay in the range 600  $\le N \le 1000$ . 113 Various materials (ANSI 304 Stainless Steel = SS, Copper, Silicon) were investigated using 600 fs 114 laser two spot ablation at 1030 nm wavelength. The pulse repetition rate was kept constant at f = 5 115 kHz while incident spot energy Ep, fluence F, separation d and pulse number/spot N were varied.



#### 116

Fig. 1 SEM images of 600 fs (N = 1000) two spot ablation on SS, Cu and Si. A schematic diagram of the optical 117 118 set-up for fs ablation is shown, middle top. **a** SS,  $IE_p = 5 \mu J$ ,  $d = 100 \mu m$ . Strong jets appear out to 0.5 mm from the spot centre. **b** Cu,  $HE_p = 20 \mu J$ ,  $d = 100 \mu m$ , jets here are much weaker, consistent with higher ablation 119 120 threshold of Cu. c Cu,  $HE_p = 20 \mu J$ , centre of ablation region at higher magnification of Fig. 1b, showing debris 121 removal between spots during plume collisions. **d** Si,  $HE_p = 20 \mu J$ ,  $d = 50 \mu m$ , highly diverging debris jets are 122 evident. e Si, HE<sub>p</sub> = 20  $\mu$ J, d = 100  $\mu$ m, lower divergence jets appear. f Si, IE<sub>p</sub> = 5 $\mu$ J, d = 150  $\mu$ m, debris is now concentrated in a "filament" between the spots. g schematic summary of two spots stainless steel ablation with 123 pulse energy, pulse number and spot separation (pulse distance d), demonstrating that filaments and jets are a 124 125 universal feature.

Fig. 1a-f show SEM images of simultaneous two spot ablation and redeposition patterns observed 126 in ambient air with stainless steel, Copper and Silicon. For these images, we use red edged 127 rectangles for s. steel, blue for Cu and green for Si substrate. Spot separation d was varied in the 128 range  $50 \le d \le 150 \ \mu\text{m}$  with pulse exposure N = 1000. In Fig. 1a, on stainless steel with IE<sub>P</sub> = 5  $\mu$ J 129  $(d = 100 \,\mu\text{m}, F = 1.5 \,\text{Jcm}^{-2})$ , strong jets appear perpendicularly aligned with respect to the spot axis 130 reaching almost 0.5 mm from the spot axis. On Copper, with HE<sub>P</sub> = 20  $\mu$ J (d = 100  $\mu$ m, F = 5.7 131 Jcm<sup>-2</sup>), Fig. 1b, jets also appear but are now significantly weaker compared to stainless steel. This 132 is likely due to the fact that the ablation threshold of Copper,  $F_{0th}(Cu) = 0.28 \text{ Jcm}^{-2}$  is much higher 133 than  $F_{0th}(SS) = 0.09 \text{ Jcm}^{-2}$  for stainless steel[19]. Fig. 1c shows an expanded image of the central 134 region of Fig. 1b, exhibiting material removal at the collision plane between the ablation spots. Fig. 135 1d-f illustrate simultaneous double spot HE<sub>P</sub>/IE<sub>P</sub> ablation on Si while varying spot separation. In 136 Fig. 1d (HE<sub>P</sub>,  $d = 50 \mu m$ ), highly diverging debris jets appear, while in Fig. 1e, (HE<sub>P</sub>,  $d = 100 \mu m$ ), 137 the effect of increasing spot separation results in lower jet divergence with clear debris removal 138 between spots. At  $d = 150 \mu m$  combined with lower energy IE<sub>P</sub>, Fig. 1f, the debris is primarily 139 concentrated in a filament between the spots. The schematic in Fig. 1g summarises the observations 140 on two spot fs ablation of stainless steel when altering pulse energy/fluence, pulse exposure and 141 spot separations. These results suggest that the appearance of filaments and jets is a universal 142 143 feature, fluence and material dependent.

#### 144 **3.2 Picosecond laser ablation**

With longer pulse length  $\tau = 10$  ps, multi-beam (N  $\ge 2$ ) ablation of ANSI 304 Stainless steel was 145 studied in ambient air and Helium with the aid of a Spatial Light Modulator (SLM) addressed with 146 appropriate CGHs based on Inverse Fourier Transforms (IFTs)[20]. Fig. 2 (centre) illustrates the 147 148 laser and optical set-up used for more complex multi-beam ablation with the SLM. After attenuation, beam expansion (BE) and beam modulation with appropriate CGH, a 4f optical system 149 re-images the complex field to the Galvo input aperture and focused by an f-theta lens to the 150 substrate. For ablation under Helium, a gas cell with fused silica input and side windows was first 151 evacuated then backfilled with He. The observed plasma emission is imaged to a fast ICCD camera. 152 Fig. 2a-i show optical images of redeposition patterns at LE<sub>p</sub> (E<sub>p</sub> = 2  $\mu$ J, F = 0.9 Jcm<sup>-2</sup>) and HE<sub>p</sub> (E<sub>p</sub> 153 = 10  $\mu$ J, F = 4.5 Jcm<sup>-2</sup>) exposure with N = 800 pulses and spot separation d = 100  $\mu$ m. We use red 154 dash boxes for ablation in air and green for ablation under He. 155

In Fig. 2a-c, the effect of altering spot geometry at  $LE_p$  results in clear debris confinement within 156 the spot patterns. Fig. 2a, with 3 spots in an equilateral triangle, debris is also confined in this 157 triangular geometry. In Fig. 2b with 4 spots in a square the confined debris field reflects this 158 geometry closely. In Fig. 2c, with 5 spots, the centre spot now acts to further direct the backward 159 flux to yield clear linear multiple narrow filaments. The effect of HE<sub>p</sub> multi-beam ablation in air is 160 shown in Fig. 2d-f, exhibiting strong debris removal (jets) along axes of symmetry. In Fig. 2d, three 161 jets are observed, while in Fig. 2e, four jets appear, two emanating along each axis of symmetry. A 162 rotated cross appears at the centre. In Fig. 2f, the 5 spots pattern again shows 4 diverging jets with 163 clear debris removal in a well-defined diamond shape around the central spot. The small spots in 164 Fig. 2d-f are ablation spots due to low-intensity ghost beams and the remaining zero order when 165 their fluence exceeds the multi-pulse ablation threshold on stainless steel. These are expected since 166 the CGHs are rarely perfect in modulation but full phase maps used here ( $\Delta \phi = 0 - 2\pi$ ) are more 167 efficient than binary holograms[21]. However, the debris around these small spots indicates the 168 local gas flow direction behind the shockwaves. The effect of using ambient He gas is shown in 169 Fig. 2g-h. Fig. 2g shows 2 spot HE<sub>p</sub> ablation under 1 Bar He where redeposition is almost absent 170 with weak debris confinement and filaments between ghost beams and the main ablation spots. This 171 172 contrasts with 2 spot ablation femtosecond in air, Fig. 1a where strong jets appear, even with intermediate energy IE<sub>P</sub>. Fig. 2h shows 5 spot HE<sub>P</sub> ablation in He at 2.5 Bar pressure, yielding 173

174 symmetric debris confinement within the spot pattern with little redeposition. Ablation under

175 Helium is more akin to free plasma expansion under vacuum.



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177 **Fig. 2** Optical images of multi-spot, 10 ps laser ablation of s. steel with  $LE_p$  and  $HE_p$  under air (dashed red boxes), 178 He (dash green boxes). Pulse exposure N = 800 pulses. A schematic of the optical set-up is shown in the centre. **a** air,  $LE_p = 2 \mu J$ , 3 spot ablation in triangular pattern, debris also shows confinement in triangular geometry. **b** 179 air,  $LE_p = 2 \mu J$ , 4 spot square pattern with clear debris field, confined in this geometry. c air,  $LE_p = 2 \mu J$ , 5 spot 180 181 ablation, now resulting in linear filaments between spots. **d** air,  $HE_p = 10 \mu J$ , 3 spot ablation with symmetric jets observed along axes of symmetry. e air,  $HE_P = 10 \mu J$ , 4 spot square ablation with 2 opposing jets emanating 182 along each axis of symmetry. **f** air,  $HE_p = 10 \mu J$ , 5 spot ablation showing 4 jets with clear debris removal in a 183 184 diamond shape around the central spot and high divergence shock debris removal. g He, 1 Bar, HE<sub>p</sub> = 10  $\mu$ J, 2 spot ablation: redeposition is almost absent with weak debris confinement and filaments between ghost beams 185 and the main ablation spots. **h** He, 2.5 Bar,  $HE_p = 10 \mu J$ , 5 spot ablation, yielding symmetric debris confinement 186 within the spot pattern but little redeposition. 187

188 SEM images and EDX spectra of debris from  $LE_P$  and  $HE_P$  5 spot ablation in air at atmospheric pressure are shown in Fig. 3. In Fig. 3a, at  $LE_p$ , debris concentration between spots is clear. Fig. 3b 189 shows the expanded region within the dotted circle of Fig. 3a and a darker region appears between 190 the spots. The EDX elemental map of this region (right) shows a higher Oxygen Ka signal around 191 the spot rims and between spots, inferring that the darker region is due to oxidation. At HE<sub>P</sub> ( $E_p =$ 192 15  $\mu$ J, F = 6.8 Jcm<sup>-2</sup>), Fig. 3c, clear jets appear along the symmetry axes while the debris field 193 within the jet in the small, dotted circle (Fig. 3c) which is shown in Fig. 3d at higher magnification. 194 This agglomerated nano-particulate material, with um size dimension shows elongation along the 195

196 jet axis. An enhanced Oxygen K $\alpha$  signal is also detected in the EDX map of the jet material (right).

197 Fig. 3e shows the detailed EDX elemental spectrum intensities of the region indicated in Fig. 3d,

198 confirming a higher oxygen concentration detected in the agglomerated jet debris (spectrum 2)

199 when compared to the underlying metal surface (spectrum 1).



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201 Fig. 3 SEM images and EDX spectra of debris from  $LE_P$  and  $HE_P$  5 spot ablation in air at atmospheric pressure. 202 **a**  $LE_p = 2 \mu J$  ablation, where debris field is concentrated between and within spots. **b**  $LE_P = 2 \mu J$ , expanded region within the dotted circle of Fig. 3a with a darker region directed between the spots. The EDX elemental map (right) 203 of this region shows a higher Oxygen K $\alpha$  signal around the spot rims and between spots. **c** HE<sub>P</sub> = 15  $\mu$ J ablation, 204 205 with 4 jets appearing along the symmetry axes. **d** HE<sub>P</sub> = 15  $\mu$ J, high magnification image of jet debris within the dotted circle (Fig. 3d). This agglomerated nano-particulate material, with µm size dimension shows elongation 206 207 along the jet axis. An enhanced Oxygen K $\alpha$  signal is also detected in the jet material, shown in the EDX map of this region (right). e detailed EDX elemental spectrum intensities of the regions indicated in Fig. 3d. A higher 208 Oxygen concentration is detected in the um size jet nano-particle agglomerate (spectrum 2) when compared to 209 210 the underlying metal surface (spectrum 1).

#### 211 **3.3 Plasma emission**

Using a fast ICCD camera, time-resolved plasma plume emissions from  $HE_p = 15 \mu J$ , picosecond 212 multi-spot stainless steel ablation in ambient air and in He were observed, Fig. 4. Red and green 213 dotted boxes relate to plasma expansion in air and He respectively. The Gate width was 5 ns, spot 214 separation  $d = 95 \mu m$ . All images were normalized to the peak intensity. In Fig. 4a, three triangular 215 spot plasma plume collisions from stainless steel in 1 bar air occur at delay time  $t \ge 15$  ns while 216 demonstrating longitudinal plasma deceleration and rapid transverse plasma plume expansion. The 217 corresponding ablation and redeposition pattern are shown in Fig. 2d. Initial longitudinal expansion 218 velocity can be estimated to be  $v \sim 3$  km/s. In Fig. 4b, with 2 spot ablation under air, the plumes 219 again show collisions after 25ns, decelerate and expand transversely. In Fig. 4c, under low density 220 He at ambient pressure ( $\rho_0 = 0.16 \text{ kg/m}^3$ ), fast longitudinal plasma expansion at speed v ~ 6 km/s 221 222 is observed with plumes colliding within 15 ns. They leave the surface, reminiscent of free plasma expansion in a vacuum. 223



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Fig. 4 Time-resolved plume emission on ICCD with  $HE_p = 15\mu J$ , multi-spot (d = 95  $\mu$ m) ablation of stainless steel in air and He at 1Bar pressure. **a** air, 3 triangular spots, plasma plume collisions occur at delay time t  $\geq$  15 ns while demonstrating longitudinal plasma deceleration and rapid transverse plasma plume expansion. Initial longitudinal expansion velocity can be estimated to be v ~ 3 km/s. **b** Two spot in air: seed plasmas collide by 25ns delay, decelerate and show radial plume expansion. **c** He, two spot, where, due to its low density ( $\rho_0 = 0.16$ kg/m<sup>3</sup>), fast longitudinal plasma expansion at speed v ~ 6 km/s is observed with plumes colliding within 15 ns. They leave the surface, reminiscent of free plasma expansion in a vacuum.

#### 232 4. Theory: Simulation of coalescing shock waves in air

233 To investigate whether laser-induced shockwave interactions influence the debris patterns, the temporal pressure evolution following multi-spot ablation in the ambient atmosphere was simulated 234 using Ansys Fluent (CFD) software. The 2D pressure field changes are solved by Euler equations 235 of gas dynamics (conservation of mass, energy and momentum) using the implicit method. The 236 237 details of plasma physics are neglected in the simulation with initial condition of the laser-induced micro-blasts considered as point sources[22]. The air environment is assumed to be a perfect gas, 238 and the boundary conditions are set as non-reflecting. The resulting pressure change could be 239 calculated by setting the initial conditions following the Sedov-Taylor model[22-24] where the 240 position of the shock wave propagation in air R(t), the maximum pressure P(R), speed U and 241 temperature T behind the shock front is given by, 242

243 
$$R(t) = \left(\frac{E_s}{\rho_0 K}\right)^{\frac{1}{5}} t^{\frac{2}{5}}$$
(1)

$$P(R) = 0.155 \frac{Es}{R^3}$$
(2)

(3)

245 
$$U = 0.360 R^{-\frac{3}{2}} \left(\frac{Es}{\rho_0}\right)^{\frac{1}{2}}$$

246 
$$T = \frac{2\gamma}{(\gamma+1)} \left[ \frac{(\gamma-1)}{(\gamma+1)} M^2 + 1 \right] T_0$$
(4)

where  $E_s$  is the energy released,  $\rho_0$  is the density of the air, K is a dimensionless constant which depends on the heat capacity ratio  $\gamma$ , and M is the shock Mach number,  $M = \frac{U}{v_{sound}}$ . For air at atmospheric pressure and room temperature,  $\rho_0 = 1.274 \text{ kg/m}^3$ ,  $\gamma = 1.4$ ,  $v_{sound} = 344 \text{ m/s}$  and

250 K = 0.856.



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252 Fig. 5 Simulation of multi-spot HE ablation on stainless steel in air,  $E_P = 15 \mu J$ , delay times 1- 60 ns. a 2 spot, d  $= 100 \ \mu m$ : coalescing shocks appears between the two spots after a 20ns delay with a pressure gradient directed 253 254 along the jet axis, evident after 30 ns. By 60ns delay, a diverging Mach shock appears with the central region now 255 back to ambient pressure. **b** 3 spot triangular,  $d = 86.6 \mu m$ : shocks appear by 9 ns delay and the coalescence of the three shocks is apparent at the geometric centre by 20 ns. Expansion continues along the symmetry axes with 256 maximum pressures at the interacting shock fronts which diverge by 60 ns delay. c 4 spot,  $d = 70.7 \mu m$ : the 257 pressure field maxima display a square symmetry along the axes at 8 ns delay and coalescing shocks again produce 258 a pressure maximum at the geometrical centre by 20 ns delay with shock fields expanding along the two symmetry 259 260 axes. By 40 ns delay, the interacting and diverging shock fronts are apparent.

During ablation, the energy released in the plume is significantly lower than the incident pulse energy  $E_p[25]$ . We have estimated the conversion efficiency by measuring the ablation rate/pulse and the plume kinetic energy (KE). From the plasma temperature  $T_e \sim 1 \text{ eV} [17]$ , we estimate that all Fe atoms are initially ionized to Fe<sup>+1</sup> ions, requiring IP = 7.9 eV/atom. The major contributions to the energy balance are the evaporation enthalpy, plasma temperature and plume KE and consequently, we estimate  $E_s/E_p \sim 0.21$ . This value appears reasonable in view of the fact that plasma absorption with ultrafast pulses is almost negligible. Setting HE<sub>P</sub> = 15 µJ (E<sub>s</sub>/E<sub>p</sub> ~ 0.21), 268 plume energy with the shock wave pressure, radius and temperature at delay time  $\Delta t = 1$  ns was 269 estimated to be P = 684.4 bar at R = 19.6  $\mu$ m and T<sub>0</sub> = 22000 K, respectively.

Results of these HE<sub>P</sub> simulations with, 2 spot, 3 triangular spot and 4 spot in a square geometry are 270 271 shown in Fig. 5a-c. In each case, the distance from spots to the geometrical centre (collision point) 272 equals 50 µm. A symmetric temporal development of shock wave interactions on the nanosecond timescale with linear shock regions appearing between spots. In Fig. 5a, a coalescing shock appears 273 after 10ns with overpressure ( $P_{max} \sim 160$  Bar), a linear shock region between spots after a 20ns 274 delay and a clear pressure gradient along the jet axis evident after 30 ns. The interaction of the two 275 expanding shock waves creates a diverging Mach shock at a time delay of 60 ns with the central 276 region now back to ambient pressure. In Fig. 5b, simulating three spot ablation, a triangular 277 overpressure region appears by 10 ns delay and the coalescence of the three shocks is apparent at 278 279 the geometric centre by 20 ns with 160 Bar overpressure. Expansion continues along the symmetry axes with maximum pressures at the interacting shock fronts which diverge by 40 ns delay. In Fig. 280 5c with four simultaneously irradiating laser spots, the pressure field displays a square symmetry 281 at 10 ns and coalescing shocks again produce a pressure maximum at the geometrical centre by 20 282 ns delay with shock fields expanding along the two symmetry axes. By 30 ns delay, the interacting 283 and diverging shock fronts are apparent. The simulations of transient pressure fields reflect the spot 284 geometries, and observed debris removal patterns from HE<sub>P</sub> two, three and 4 spot ablation (Fig. 1 285 and Fig. 2). 286



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Fig. 6 SEM images of the multi-spot  $HE_p = 15\mu J$ , debris field observed during ablation on stainless steel in air and corresponding CFD simulations. **a** 3+1 spot ablation showing debris removal. **b** simulation of corresponding HE<sub>P</sub>, 3+1 pressure field at delay time  $\Delta t = 10$  ns highlighting the triangular pressure field symmetry around the centre with similar dimensions. **c** HE<sub>P</sub>, 5 spot pattern with debris field removal in a square pattern round the centre spot. **d** simulation of HE<sub>P</sub> 5 spot pressure field at delay time  $\Delta t = 10$ ns which replicates this well-defined square symmetry.

Fig. 6 shows SEM images of more complex multi-spot HE<sub>p</sub> (N = 1000) ablation of stainless steel in air and corresponding CFD simulations. Fig. 6a shows the (3+1) debris field with shockwave removal of debris in triangular geometry around the central spot. The simulation of corresponding 3+1 pressure field at delay time  $\Delta t = 10$  ns is shown in Fig. 6b on the same scale with a triangular high pressure shocked region matching that in Fig. 6a. In Fig. 6c, the 5 spot ablation pattern shows 299 debris removal in a square pattern around the centre, while in Fig. 6d, the simulation of this pressure 300 field at delay time  $\Delta t = 10$  ns replicates this well-defined square symmetry in the coalescing shocks.

Fig. 7 presents data from simulations of LE<sub>P</sub> two spot ablation of stainless steel in ambient air. Fig. 301 7a shows the calculated pressure with time at the midpoint with spot separations from 50  $\mu$ m  $\leq$  d  $\leq$ 302 250 µm. The time to reach maximum pressure increases with d as expected while peak overpressure 303 falls rapidly. The insert shows an expanded scale for delay time  $\Delta t \ge 80$  ns and demonstrates that 304 rarefaction occurs with pressure falling below 1 Bar. Fig. 7b shows the simulated 2D pressure field 305 306 from LE<sub>P</sub>, 2 spot (d =100  $\mu$ m) ablation at time delay  $\Delta t = 140$  ns. The two white dots mark the spot positions. There is evidence here of secondary shocks moving towards the centre. In Fig. 7c, the 307 simulated pressure along the axes parallel (X-axis) and normal (Y-axis) to the spots (Fig. 7b) at 308 delay time t = 140 ns is shown, where negative pressure gradients are evident along both axes. The 309 310 Y-axis peak pressure is significantly higher than that parallel to the spots.



**Fig. 7 a** Simulated pressure with time at the centre of  $LE_P = 2\mu J$ , spot ablation when varying spot separation, 50 µm  $\leq d \leq 250 \mu m$ . The insert shows an expanded scale for delay time  $t \geq 80 ns$ . **b** simulated 2D pressure field of LE<sub>P</sub> 2 spot ablation at time delay t = 140 ns with evidence of inward moving secondary shocks **c** simulated pressure along the axes parallel (X) and perpendicular (Y) to spot axis for Fig. 6b at delay time t = 140 ns. Note the negative pressure gradient in both directions towards the centre and rarefaction near centre. The spot positions are shown by the dotted lines.

#### 319 5. Discussion

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When a pulsed laser beam ablates a metal surface in an ambient atmosphere, the expanding plasma plume can be likened to a micro-detonation[24, 26]. As the plume expands supersonically, this results in a Mach shockwave and plume pressure gradient. The debris field around a circular laser spot is then spherical from symmetry. The effect of adding simultaneously generated ablation plumes alters this symmetry accordingly when the spots are in close proximity.

The study of shock waves through detonation goes back to the 1950's[24, 27] while laser-generated plume expansion into background gases indicates that the compressed background gas layer temperature behind the shock front depends on the Mach number[25]. The study of spherical and cylindrical converging shock waves and their stability has been researched extensively[27-29].

The effect of multiple ablation plumes in close proximity, creating coalescing shock waves, would 329 be expected to increase the transient peak overpressures in certain regions. The interaction and 330 coalescence of simultaneous, multiple blast waves from explosive detonations were studied recently 331 through Schlieren simulations with symmetric geometries similar to those used here with multi-332 spot ablation[30]. The predicted pressure fields show high symmetry and pressure gradients along 333 the axes of symmetry. Our simulations of multi-beam ablation also predict the symmetry of 334 interacting shocks observed experimentally, strongly suggesting that supersonic shocks are 335 involved, even though the pulse energies used here are relatively small. There is evidence in our 336 experimental results that Mach Stems[31] also appear, Fig. 5a&c. 337

The interaction of quasi-stationary shockwaves during fs laser of multiple excitation spots at a 338 339 water/air interface was observed by transient reflection due to supersonic colliding airflows normal to the spot axes, with shock symmetry reflecting spot geometries [32, 33]. In particular, their 4 spot 340 reflection image (with geometry due to refractive index changes during shock wave coalescence) 341 342 showed the precise shock wave pattern with a cross at centre, remarkably similar to our 4 spot redeposition pattern, Fig.2e. In He, however, the shocks disappeared due to the low gas density, and 343 our observations of high energy multi-spot ablation in He, also showing the absence of jets, are 344 consistent with references [32, 33]. As the speed of sound in He,  $v_s \sim 1000$  m/s, the Mach number 345 is reduced by a factor of 3 compared to air, while the low density allows nearly free plasma 346 expansion with speed v > 6 km/s, (Fig. 4). Our elemental analysis of the debris from stainless steel 347 during LE<sub>P</sub> and HE<sub>P</sub> multi-spot ablation, investigated using EDX (Fig. 3) confirmed significantly 348 increased levels of oxygen (O Ka signal) around spot rims, between spots and in the agglomerated 349 nano-particulate material in the jets (Fig.3b,d). Combustion occurs during single and multi-spot 350 ablation due to the exothermic reaction of Fe with Oxygen likely resulting in  $Fe_2O_3$  and  $Fe_3O_4$ 351 debris where reaction enthalpies are 824 kJ/mol and 1118 kJ/mol respectively[34]. However, the 352 shock wave acts as a barrier to combustion, so molecular formation probably occurs towards the 353 end of the ablation process after shock wave collapse[4]. We estimate that oxidation adds only 10 354 % to the energy balance. 355

During surface ablation with ultrafast laser pulses (as opposed to nanosecond pulse irradiations), 356 more stable plasma plumes are generated by avoiding melt and plasma absorption. Ablation 357 thresholds are also much lower. This results in very fine nanoparticles and agglomerated 358 nanoparticle debris, created in the plasma collisions with the ambient gas along with phase 359 explosion. At low energy in ambient air, LE<sub>p</sub> ablation rate and debris are minimised while shock 360 wave pressures are significantly reduced, hence unable to remove surface debris. CFD simulations 361 carried out at LE<sub>p</sub> and HE<sub>p</sub> demonstrated self-similar pressure field geometries but at different times 362 scales due to the differences in the rate of shock wave expansion. We infer that long after shock 363 364 waves have decayed, the following air flows due to the negative pressure gradients and rarefactions can drive NPs in the air towards the centre to create directed redeposition by backword flux. If we 365 look at the simulations of LE<sub>p</sub> 2, 3 and 4 spot exposure at later times, Fig. 5a-c where  $\Delta t = 60$  ns, 366 the pressure fields exhibit linear, triangular and square shaped central low pressure regions 367 respectively. The plume NPs for 2 spot would then be directed towards the spot axis while for N > N368 2 these geometries experience radial negative pressure gradients, confining debris within spot 369 geometry. 370

The plasma lifetimes observed here,  $\tau_{pl} \leq 100$  ns << interpulse period  $\tau = 200$  µs at 5 kHz pulse 371 repetition rate, so that plasma absorption from following pulses is negligible. High energy multi-372 spot, multi-pulse ablation allows the build-up of sufficient debris on the substrate surface by 373 backward flux, which, due to the agglomerated low-density nano-particulate nature, becomes a 374 surface layer sensitive to the coalescing shock waves and gas flow fields (rarefactions) behind 375 shocks, ejecting surface debris along axes of symmetry. The early high-pressure shock interactions 376 imprint the shock symmetry on the debris fields, and our experimental results are supported by the 377 simulations. A universal behaviour, independent of material has been observed with filaments and 378 jets when allowing for the varying material ablation thresholds and ambient gas density. The 379 380 observations at high energies can be regarded as a form of laser shock cleaning which is more generally accomplished with plasma breakdown in the air above a surface [35]. Dust removal from 381 a surface has been observed behind a propagating shock wave [36]. Shock wave generated cavities 382 at an air/water interface with fs pulses at an ultrahigh intensity  $I > 10^{15} \text{ W cm}^{-2}$  have also been 383 observed[32] while within fused silica, material densification was recently reported due to the high 384 pressure shocked regions ( $P_{max} > 10^5$  Bar) between spots[37]. 385

Coalescing blast waves, which have been shown to obey common scaling laws [18], allow for direct 386 read-across with larger scale high explosive and nuclear blast data. There is a potential application, 387 therefore, for using smaller-scale, well-controlled laser ablation techniques to study the interaction 388 of blast waves from multiple sources to mitigate the damage to complex structural forms, replicable 389 390 by treating a reflecting surface as a symmetry plane and designing the experiment accordingly [38].

CFD simulations were related to multi-pulse exposure on s. steel where we estimated the conversion 391 392 efficiency from incident pulse energy to expanding plasma plume to be  $E_S/E_P = 0.21$ . On other materials, this ratio will be different - and needs to be determined, but the experimental 393 observations of a universal multi-spot ablation behaviour on Stainless Steel, Cu and Si with jets and 394 filaments, material dependent, encourages us to suggest that CFD modelling may also be applied 395 to other materials when allowing for material reflectivity, ablation threshold, and pulse to plume 396 conversion efficiency. 397

#### **6.** Conclusions 398

Due to the capabilities of a Spatial Light Modulator, able to produce arbitrary spot patterns with 399 uniform and non-uniform laser spot energies, the observations here open up a potentially useful 400 new diagnostic technique for the study of coalescing shock waves and supersonic air flows using 401 relatively low energy ultrafast laser pulses. During multi-spot ablation in ambient air at low pulse 402 energies, debris is highly confined within the spot patterns due to converging air flows towards the 403 404 end of the ablation process. On the contrary, at higher fluence, jets of debris, lifted and accelerated by colliding supersonic Mach shocks on the nanosecond timescale, emanate along every axis of 405 406 symmetry. These phenomena appear universal but depend on the spot proximity, substrate and ambient gas density. This approach opens up a new window on coalescing shock waves based on 407 408 observed debris re-deposition patterns which complement techniques using transient reflection[32] or fast transient absorption[19]. However, a major advantage here is that at low shock wave 409 intensities, where refractive index changes in the air may not be visible anymore, the debris field 410 around spots and confined within spot patterns now highlight the air flows following weak shocks. 411

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